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RADC-TR-67-17 Final Report



AMR DIGITAL TROPOSCATTER TEST RESULTS

Environmental Science Services Administration
Staff of ESSA/ITSA

TECHNICAL REPORT NO. RADC-TR-67-17
March 1967

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FOREWORD

This final technical report was prepared by the Institute for Tele-communications Sciences and Aeronomy of the Environmental Science Services Administration (ESSA/TISA), Boulder, Colorado 80302 for the Rome Air Development Center under Contract AF 30(602)-3446, Project 6523, Task 652304. Secondary report number is 3446 04.

The report has been coordinated with each digital technique manufacturer upon the receipt of the draft and their comments have been included.

Reference is made to RADC-TR-65-427 which covers the results of the Sunde Tropo Channel Model used to predict error probabilities on this test. The Signal Processing Section (EMCRS) undertook the theoretical and mathematical analysis of the communication techniques tested.

RADC Project Engineer is Frank Chiffy (EMCTW-3).

This technical report has been reviewed and is approved.

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ABSTRACT

This report describes the work performed under Contract AF30(602)3446. Its purpose was to evaluate the performance of three types of contractor furnished digital modulation equipment, using simultaneous data from an FM-FDM system as a standard.

The tests covering a period from November 1964 through May 1965 were conducted on an over-water path between East Island, Puerto Rico and Grand Turk Island, BWI.

The standard FM-FDM system technique referenced was the Radio Set AN/MRC-98 a transportable tropospheric scatter radio set operating in the 755-985 MHz range with an output r.f. power capability of 10 K.W.

The digital techniques were variations of Pulse Code Modulation, Pulse Position Modulation, and Delta Modulation schemes.

A description of test instrumentation configurations and data collection procedures is presented. Test results are discussed and presented in tabular and graphical form.

EVALUATION

This report confirms the need to run 200 and 100 mile tropo tests that are presently being conducted in upstate New York. The contractor experienced difficulties during his data analysis and some data was removed for such reasons as, power failures, noisy tapes, errors in time code and for conditions during which the data was outside the range of calibration.

A limited amount of looping and quad-diversity data has not been reduced by ESSA due to a lack of time but is available on magnetic tape for reduction should the need arise.

This report was coordinated with each technique manufacturer upon receipt of the rough draft and their comments have been included.

FRANK P. CHIFFY

Project Engineer

EMCTW-3

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I. Introduction

Tests were conducted over an over-water path between East Island, Puerto Rico, and Grand Turk Island in order to obtain data for the purpose of evaluating the performance of three types of contractor furnished digital modulation equipment, using simultaneous data from an FM-FDM system as a control. The tests were divided into three time periods, one for each contractor, covering a period from November 25, 1964 through May 13, 1965. The purpose of this report is to describe the tests and to present the data obtained from them.

Some of the data were recorded on 14 channel magnetic tape for later reduction (see Section IV). An attempt was made to record simultaneously for both systems as many of the following parameters as possible:

- (1) time code
- (2) carrier levels (possibility of four receivers on the digital system and four on FDM when quad diversity used)
- (3) digital data, out-of-sync information
- (4) digital data, errors
- (5) combined signal levels (when using diversity)
- (6) signal-to-noise ratio (see Section IV. 2)
- (7) idle channel noise.

Priority was assigned to parameters (1), (2) and (4).

Voice data were recorded on a separate magnetic tape recorder.

Because of the wide variety of conditions encountered and the large number of variations of the type of data obtained, it is difficult to derive definite conclusions from the data. However, the information from these tests should be valuable when evaluating the results from later tests. Two additional paths, (1) an over-land path approximately 200 miles long between

Verona, N. Y. and Model City, N. Y. and (2) an over-land path between Verona, N. Y. and a point approximately 100 miles distant along the Verona-Model City path, are proposed for these later tests.

II. Path Description

The path extends over water from Grand Turk Island to East Island, Puerto Rico as shown in figure 1. The antennas are located at 21° , 25° , 32.25° north by 71° , 8° , 43.00° west and 18° , 28° , 34.93° north by 66° , 10° , 48° west. The distance d indicated in the lower portion of figure 1 is 613.7 km. The angle θ (see figure 1) for a surface refractivity value, $N_{s} = 347$, corresponding to the average value for February is .0596 radians, and for $N_{s} = 380$, corresponding to the average for August. $\theta = .0551$ radians, where the bending was calculated using Bean and Thayer [1959]. The scattering volume lies above approximately 9 km above sea level. Two 18.3 meter parabolic section reflectors fed by offset horns are located at each end of the path. The heights of the center of the reflectors above sea level are 14 meters at Grand Turk and 25.9 meters at East Island. The antennas at East Island are shown in figure 2, and one feed horn with a section of wave guide are shown in figure 3.

The AN/MRC-98 communications system consists basically of two (2) transmitters, four (4) receivers with necessary combiners for dual or quadruple diversity, a twenty-four (24) channel multiplex-demultiplex system, a mobile diesel generator, and test equipment, waveguide, etc., necessary for independent operation as a communications terminal. One complete AN/MRC-98 system was installed at each end of the path. In addition, a third system was divided between the terminals to provide three (3) transmitters and six (6) receivers at each end of the path. This provides the combinations of equipment configurations shown in figure 4. Generally throughout the tests, the FM-FDM system was operated in the dual diversity mode using horizontal polarization.

The path area is near the tropical hurricane region of the Eastern Carribean. The climate is tropical marine, slightly modified by insular influence when land breezes blow. A preliminary examination of seven years of radiosonde data taken at San Juan, Puerto Rico, was made to determine, to some extent, the radio climatology. At the San Juan end, radio ducts are believed to exist about 25% of the time. However, two years of radio data, [RCA, 1964] do not contain field strengths as large as would be expected if the ducts extended the length of the path.

Ducting gradients were found to exist 35% of the time for the winter months of December through February, 28% of the time for the March-April-May period, 20% of the time for the summer months of June through August, and 19% for the autumn period of September through November. Fifty (50) percent of these ducting layers showed a range from 157-200 N units/kilometer, decreasing to a 0.6% occurrence for a gradient of 588 N units/kilometer. Twenty-three (23) percent of the total number of ducting gradients were surface ducts and about twice as many of these occurred at 1500 GCT (1000 local time) as were found to occur at 0300 GCT (2200 of the previous day).

Predictions of transmission loss [Rice, et. al., 1965] were made and compared with the available data [RCA, 1964], using the maritime temperate overseas classification to obtain the distributions shown in figures 5, 6, 7, 8. Pertinent values of the parameters used for these calculations are: Transmitter power, $P_t = 7.5$ kw, line losses, .5 dB, antenna gain, $G_t = G_r = 41$ dB, and frequencies, f = 779.5 MHz and f = 879.5 MHz.

III. Test Facility Equipment Descriptions

The basic RF system used in these tests is discussed briefly in Section II, Path Description. These equipments were used in various combinations as required by the test being performed. For example, it was

possible to operate both the FM-FDM system and a digital modulation system dual diversity by transmitting both from one end of the path and receiving at the other. When quad diversity was used, the FM-FDM was transmitted from one end of the path and the digital modulation was transmitted from the other. All receiving was then done at the opposite end of the path.

The exciter and power amplifier of the transmitters and the RF section of the receivers were used with each of the digital modulation systems. Each contractor was required to properly interface their digital modulation system to the AN/MRC-98 transmitting and receiving systems. The point in the system for making the interface connections was at the discretion of the contractor. Details of the interface connections are discussed in the description of each digital modulation system.

Each system was basically a 24 channel communications system.

During most of the tests all systems were fully loaded with four channels used for data and the other 20 channels noise loaded. Periods when less than 24 channels were loaded are noted in Section VII. The methods of noise loading each system are discussed in the descriptions of each system.

III. 1. FM-FDM Equipment Description

As was mentioned in the introduction, the purpose of this test was to obtain data to evaluate the performance of three types of contractor furnished digital modulation equipment using simultaneous data from an FM-FDM system as a control. The FM-FDM system used was an AN/MRC-98 tropospheric scatter communications system. This is a diversity system with flexibility so that it can be operated using a single transmitter and a single receiver (no diversity); dual diversity with one transmitter, spaced receiving antennas and two receivers; or quad diversity using two transmitters on spaced antennas, spaced receiving antennas and four receivers. The combiner is a post detection combiner.

The AN/MRC-98 is a 24 channel system. At the transmitter the 24 channels are combined into a baseband by a frequency division multiplexer. The baseband is then used to frequency modulate the RF carrier in the exciter stage of the transmitter. The multiplexer has sufficient output to drive two exciters for quad diversity operation. At the receiving end, the baseband output of the combiner is separated by the demultiplexer system into the 24 individual channels.

For these tests four channels were used for data measurement and the other 20 channels were noise loaded. The purpose of the noise loading was to simulate a fully loaded system. The noise loading was accomplished by driving the baseband input of an FDM demultiplexer with a random noise generator. The output of these individual channels were connected into the channels of the FDM multiplexer which were to be noise loaded. This method of loading provides a noise source to each channel which is statistically independent of the noise in the other channels.

III. 2. PCM Equipment Description

Figures 9 and 10 are block diagrams of the interface equipment used between the PCM equipment and the AN/MRC-98 system for transmitting and receiving purposes respectively. The same equipment using different plug-in band shaping networks is used in the transmission of either PCM or FDM information.

The transmitter interface equipment consists of a baseband amplifier and a video shaping network followed by a 70 MHz modulator and an AFC. The baseband amplifier, and the modulator are broadband and are capable of multi-channel operation. The AFC unit is used to stabilize the modulator. The modulator output has sufficient output level to drive either one or two AN/MRC-98 exciters. Thus, both dual diversity and quadruple diversity operations were possible. Video shaping for 12/24

channel FDM or 12/24 channel PCM was achieved by plug-in networks per CCIR recommendations for FDM operation and low pass filters approximating a Gaussian response for PCM operation.

The receiver interface equipment was connected to the AN/MRC-98 receiver at the 70 MHz IF amplifier ahead of the limiter. Thus, no limiting or AGC features of the AN/MRC-98 were used with the PCM equipment. The interface equipment consisted of a five pole Gaussian shaped filter of approximately 2 MHz bandwidth for 24 channel operation and 900 kHz bandwidth for 12 channel operation followed by a heterodyne mixer and IF amplifier-filter configuration and an equal gain predetection combiner. The second local oscillator was voltage controlled to provide coherent combining. The IF filter appeared as a single tuned circuit with a bandwidth of approximately 4 MHz for 24 channel operation. The overall filter configuration preceding the combiner was equivalent to a six pole Gaussian shaped filter with a bandwidth of 1.77 MHz for 24 channel operation and

with a time constant of about 1 millisecond, was derived from the combined output and was fed back to each IF amplifier. The combiners were designed to operate in either dual or quadruple diversity modes by proper connections. In either mode the combiner compares the phase of the IF carrier at its input with the phase of the combined output. The error voltage, which is proportional to the phase difference, is used to adjust the phase of the VCO in that channel and bring the input signal into coherence with the combined output. The time constant of the loop was approximately 30 microseconds. The linear demodulator and the baseband amplifier are broadband to accommodate multi-channel PCM or FDM information. The receiver band shaping is achieved by both predetection and post-detection filtering. Post-detection band shaping for the FDM case consists of de-emphasis networks

designed to produce the inverse of the corresponding pre-emphasis shaping. When PCM type information is to be transmitted, these networks are replaced by filters producing approximately Gaussian attenuation characteristics.

The following is a functional description of the multiplexer equipment based on the PCM multiplexer block diagram of Figure 11.

Each input channel has two parts, the voice input and signalling or address input. The voice input is amplified by the input amplifier and sampled at an 8 kHz rate by the sample switch. During one 125 μ sec. frame, the channels are each sampled once for three bit lengths. The composite of all these samples appears on the PAM bus as a pulse amplitude modulated signal. The signalling input, via an interface buffer, is sampled by a sample switch in the same manner as the voice.

The timing of the internal functions of the multiplexer is determined by the 1, 352 kHz oscillator when 12 to 24 voice channels are used. When 12 voice channels or less are used, the timing is derived from the 676 kHz oscillator. The 12/24 line switching is a manual operation. The clock pulse generator provides the proper pulse width and fan-out for the 1,352/676 kHz clock. The time counter changes state once for each clock pulse and goes through one cycle of seven states for each channel in the frame. A diagram of the PCM format is given in figure 12. The timing decoder produces one pulse for each state of the time counter. These timing pulses are distributed as needed to other parts of the equipment.

The channel counter changes state once for every cycle of the time counter and goes through a cycle of 12 or 24 states (as determined by the 12/24 line switch) for each frame. Each state or code of the channel counter represents a channel. These codes are detected and sampled by the channel selector which sends channel select signals to the sample switches, except for the channel "0" select signal. It is used to activate

the frame synchronization generator. The frame synchronization is a single pulse which assures the "1" state for one frame and then the "0" state for the next frame, etc.

The compressor gain decreases as signal amplitude increases, thereby decreasing the vulnerability to noise. The sample and hold circuit samples the center of each PAM pulse with a one bit wide pulse (1.28/0.74 μ s) thus reducing noise and cross talk. The amplitude sample is held for 5.18 μ sec. (or 10.36 μ sec. for 12 line operation) while it is being converted to a six bit binary code.

The coder control programs the analog-to-digital conversion.

First, it sends code 32 (which corresponds to the middle of the analog signal swing) in binary to the digital to analog converter and the resulting trial voltage is compared with the signal voltage by the comparator.

Second, the trial code (32) is increased or decreased by 16, depending respectively on whether the signal voltage was higher or lower than the trial voltage, and then another comparison is made. Third, the above is repeated, except that eight is added or subtracted from the trial code.

On the fourth time, four is used to increment the trial code. Fifth, two is used, and sixth, one is used. The six high/low decisions made in this any are equivalent to a six bit binary code representing the amplitude of the PAM pulse.

The data format assembler produces the final PCM output. The signalling or addressing is added as a seventh bit to the six bit serial code produced by the coder control. The alternating 1, 0 bit frame synchronization produced by the frame synchronization generator is added to the 24 (or 12) voice channels as though it had originated from a 25th (or 13th) channel.

PCM Demultiplexer: The following is a functional description of the PCM demultiplexer equipment based on the block diagram given in figure 13. The PCM data enters the demultiplexer through a slicer which includes a differential amplifier and internal DC restorer. The slicer

output goes to an extremely high or low value depending on whether the PCM input is above or below a central threshold level. The phase difference integrator integrates the difference between the phase of the slicer output and the phase of the voltage controlled oscillator to adjust the voltage controlling the frequency of the VCO. This frequency-tracking system is arranged to produce a synchronous clock centered halfway between the transitions of the slicer output. The 12/24 line switching is used to accommodate either 1.352 MHz or 676 kHz bit rate. The clock pulse generator provides the proper pulse shape to advance the time counter. The time counter changes state once for every bit and goes through a cycle of seven states for each channel. The timing decoder produces one pulse for each state of the time counter, and these timing pulses are distributed to other parts of the equipment as required.

The input shift register converts the serial binary output of the slicer to a sequence of seven bit, parallel codes, one for each channel. Each six bit code (excluding the signaling bit) is converted by the digital to analog converter to an amplitude modulated pulse (PAM). The expander restores the PAM signal, which had been compressed by the multiplexer, to its original form. The PAM bus connects the central equipment to the individual channel.

The channel counter changes state once for every seven bits going through a cycle of 12 or 24 states (depending on the 12/24 line switching) during each frame. The channel selector detects each state of the channel counter, selecting the 24 (or 12) sample and hold circuits in sequence.

During frame synchronization, no sample-and-hold circuits are selected, and the frame synchronization control examines the sync wave-form to see whether or not the expected frame sync waveform has arrived at the expected time. If the received waveform deviates from the expected waveform beyond a particular limit, the frame sync control will halt the time counter—until the proper sync waveform arrives.

Each sample and hold circuit samples the amplitude of the center of the selected PAM pulse and holds the amplitude until the next sample (in the next frame). The low pass filter smooths out the step-like waveform coming from the sample and hold circuit. The output amplifier drives a 600 ohm telephone line.

The input shift register puts the signaling bit of each seven bit code on the signaling bus. The signaling bit is gated into the appropriate signaling storage device by the channel selector. The signaling storage holds the signaling output constant from one frame to the next.

III. 3. Martin PPM Equipment Description

The essential features of the system supplied by Martin Company are the use of fourth order frequency diversity, and the combination of frequency and time division multiplexing as an integral portion of the equipment.

The digital modulation technique has a bit length of eight microseconds. This is subdivided into six intervals of 1.33 microseconds each. RF pulses, each at a different frequency are transmitted in four of the six sub-intervals. The spacing between the individual frequencies is 2 MHz making the overall bandwidth 8 MHz. From the standpoint of the receiver, which is programmed when to expect the signal on each frequency, a permutation in the order of transmitting the four frequencies can be readily recognized and made the basis for multiplexing several channels on the same basic bandwidth.

The system is basically a 24 channel combination TDM/FDM multiplex system which employs PPM of the quantized data. Only four of the channels were completely implemented. Twenty channels used simulated data during the experiments. A block diagram of the transmitting portion of this equipment is given in figure 14. A bandpass filter with a bandwidth

of 150 to 3500 Hz and a pre-emphasis network of 6 dB/octave which can be optionally switched in or out is supplied at the input to each of the four fully-instrumented voice channels.

The audio AGC operates on the peak of the audio input signal. It has characteristics of fast pull-in and slow drop-out. The pull-in time is approximately equal to 1/2 cycle of the audio present and the drop out time is approximately ten seconds. The squelch circuit has approximately the same pull-in time with a drop-out time of five seconds.

In the compressor an instantaneous compression is obtained using several sections of resistively loaded diodes to achieve an approximate logarithmic response.

A diagram showing the processing that takes place in the voice quantizer is shown in figure 15. The analog waveform is sampled once every $128\,\mu\,\text{sec.}$ The time between such samples is divided into sixteen $8\,\mu\,\text{s}$ frames. The instantaneous amplitude of the voice at the time of sampling is translated into a short pulse whose position in this $128\,\mu\,\text{s}$ period is proportional to the amplitude. This pulse position is continuous and may begin at any time during the sample period. The start of the pulse will fall within one of 16 discrete time frames in the sample period. An $8\,\mu\,\text{s}$ pulse will then be transmitted in this frame. The result may be considered equivalent to a 16 level quantized PPM system. To make the most efficient use of this relatively small number of amplitude levels, the analog voice signal is processed in the compressor and AGC circuits prior to sampling to make all amplitudes within a certain dynamic range nearly equal.

To simulate the output of the other 20 channels there are 20 asymmetric, free-running multivibrators operating close to but not exactly at 7.8125 kHz. All are maintained to within a 5% tolerance. Each multivibrator puts out a 3µs pulse at the 7.8125 kHz rate. Each of the multivibrator outputs is quantized into one of the discrete 16 intervals by a

separate quantizer. These noise quantizers are similar to the voice quantizers. The noise channel programs were keyed on at near random quantum levels at rates of one noise program per two sample periods. This rate made each noise channel approximate a 50% duty factor phone channel.

The data system generator was used to transmit data by "Time Shift Keying" (TSK) between Frames 8 and 9 on Channel 1. Frame 8 represented a one and Frame 9 a zero. Data at 2604 bps was sent using TSK three times redundant.

The synchronization pulse generator sends synchronization once per sample period during Frame 1. The synchronization program was also used for an order wire having 13 levels of QPPM between Frames 3 and 15.

The encoder patch panel and program selector serve the function of ensuring each channel has proper addressing. Each of the 24 channels has its own address which comes from a 4 x 6 matrix (four frequencies and six 1.33μ sec. time slots). Of these 24, some are exclusive (no overlap) in others 2 frequencies or more overlap in a time slot.

The frequency time program used in these tests are given in figure 16. Figure 17 is a diagram in schematic form showing how the programs are selected for transmission over the four frequencies. The program selector selects the frequencies in accordance with the address program and in turn furnishes the gating function which reads the appropriate frequency. The oscillators furnishing the carrier frequencies to the gating circuits are separated by 2 MHz and cover the band between 67 MHz and 73 MHz as shown in figure 14.

The outputs of the four gated oscillators are summed together in a resistive network to assure linearity and low intermodulation. The output of this coupling network is then matched to the AN/MRC-98 exciter.

The Martin receiving equipment is matched to the AN/MRC-98 receiver at the 70 MHz IF. A block diagram of the Martin PPM equipment is given in figure 18. The four frequencies each have separate IF amplifiers with bandwidths of about 750 kHz measured at the 1 dB point.

The AGC, which is fed to the individual IF amplifiers, is controlled by the median signal level from the linear detectors of each of the channels. The time constant of the AGC is on the order of seconds.

The synchronization summer delays the F_1T_1 , F_2T_2 , F_3T_3 information such that it will be time coincident with F_4T_4 . The output is used to synchronize the receiver clock. The synchronization time constant is on the order of seconds.

The output of each of the four intermediate frequency amplifiers is detected by a square-law detector. Figure 19 is a schematic presentation of the gate matrix and decoder patch panel. The squared signal is then synchronously integrated at the time it is expected. This yields a d-c output proportional to the energy of signal plus noise. The integrator outputs are held for the full pulse period (to the end of the eight microsecond frame), and then summed to produce an equal-gain combined output. Each of the 16 frames in a sample period is similarly examined by the detector. At the end of the sample period the frame having the highest d-c level is chosen as having the greatest energy present. The frame is then passed to the balance of the demodulator. A descriptive diagram of the integrator and demodulator process is given in figure 20.

The expander, figure 19, performs the opposite function of the compressor except μ = 10 instead of μ = 50 as in the encoder, figure 14. This reduction of μ aids in the reduction of quantizing noise.

The data TSK demodulates the data from the order wire channel. The data rate is 1/3 the frame rate. Therefore, there is a two out of three majority decision requirement that must be satisfied before the bit is accepted. An internally generated pattern can be used to compare with the incoming data to establish the number of errors.

III. 4. Motorola Deltaplex Terminal Equipment

The delta modulation equipment furnished by Motorola is a 25 channel system which employs a combination of TDM/FDM. Only four data information channels were implemented completely. These channels were 5, 10, 15, and 20. Channel 25 was used for frame synchronization and order wire purposes. The remaining 20 channels consisted of dummy TDM equipment and were fed with a pseudo-random pattern generator. A multiplex transmitter is shown in figure 21.

The four data information channels have bandpass filters which are required for filtering the voice signals before they are applied to the delta modulator. The high frequency cutoff of 3.5 kHz was selected to minimize harmonics of the voice signal that could beat with the sampling frequency and produce audio interference. In addition the high frequency cut-off eliminates false frame synchronization. Two inputs into the delta modulator are provided - one for logically generated audio inputs and one for digital data. The audio input is to the differential amplifier of the delta modulator. For digital data, the input is fed directly into the sampling section of the delta modulator. The four delta modulators are sequentially sampled every $26~\mu$ sec. with a $1.04~\mu$ sec. pulse produced by the clocking mechanism. Figure 22 shows a single channel input and a frequency-time diagram which will further clarify the input to the channels as well as the sequential sampling.

The frame synchronization and order wire channel provides two functions each using one-nalf the channel. The frame synchronization pattern is a repetitive series of a mark followed by three spaces, or 1 0 0 0 1 0 0 0 1 0 0 0, etc. This pattern is directly derived

from the system clock, and has a low probability of being generated by data signals. The frame length is 26μ sec. The order wire signal is delta modulated at a 19.2 kHz sampling rate, one-half the sampling rate of the 24 data transmission channels.

The time division multiplexing groups the 25 channels in five groups of five channels each. To provide maximum spacing within a group, the channels are grouped with constituent channels five sampling periods of 5.2 µ sec. apart.

Since there are five time division multiplexed groups, there are also five FSK frequency pairs. Each time division multiplexed group was used to key one FSK frequency pair. If a "1" (mark) is to be transmitted, one of the frequencies is keyed while the other is constrained to the off state. If a "0" (space) is to be transmitted, the other frequency in the pair is keyed on while the prior one in the pair is constrained to the off position. The ten total frequencies are so chosen that no adjacent time slot has an adjacent frequency element. Each pair is also arranged so that the mark and space frequencies for any time slot are five frequency elements apart. In figure 22, the arrangement of the frequency pairs about the 70 megacycle center frequency is given.

The outputs of the FDM gates consist of ten lines, each line having one 1.04 μ sec. pulse at one of two frequencies every 5.2 μ sec. The outputs of the FDM gates are linearly combined and the output is a succession of pulses, one every 1.04 μ sec. at different frequencies from 65.68 to 74.32 MHz spaced 0.96 MHz apart. The output of the linear combiner is fed to the transmitter exciter. There is no pulse shaping done in the Motorola equipment. The power spectrum at the output of the Motorola equipment may be considered a rectangular pulse.

The Motorola receiving equipment was interfaced with the AN/MRC-98 receiving equipment after the AGC portion, but before the limiting action of the AN/MRC-98 receiver. RADC furnished an IF

amplifier panel with a bandwidth of 10 MHz to accomplish the necessary equipment interface. As shown in figure 23 the two receiver IF sections are fed from separate receivers for diversity operation. The output from one receiver is split into two paths, one path to detect the mark signal (f_3) and the other to detect the space signal (f_8) . The filter provided for each path or channel is a triple section synchronously tuned filter. The overall bandwidth of the filter is approximately 300 kHz.

The outputs of the filters are differentially envelope detected and added to form a bipolar analog pulse train. The integration time at the output of the envelope detectors was about 1 microsecond.

The transmitted signal is processed in a second receiver IF strip identically as described above. The analog pulse trains are passed through individual delay lines to equalize the differential delay between the two pulse trains due to the possibility that the diversity antennas may not be precisely aimed at the same common volume. The time equalized pulse trains are then added in a linear adder to form the composite bit stream. This 192 kHz signal is used to obtain bit synchronization. The clock output is then routed to a divide-by-five commutator. The TDM wave train from the diversity combiner is fed to a threshold amplifier. This amplifier converts the analog bipolar input to a squared binary output. The threshold amplifier is reset prior to each sample by the recovered bit clock. The binary output of the threshold amplifier is in turn sampled by each of the five separate outputs of the commutator to separate the serial train into five parallel digital outputs, each output being 26 microseconds long.

Frame sync is achieved by looking for the 9.6 kHz tone applied to the sync channel. A 9.6 kHz bandpass filter is located at the output of the five digital channel outputs. The energy from the filter having frame sync is used to inhibit the sequential sampling until receiver frame sync is obtained. Normally less than 1 milliseconds are required to obtain frame sync.

The digital output of the channel is fed directly to the delta demodulator. The delta demodulator consists of an integrator circuit with equal charge and discharge time constants. The output is then filtered to obtain 0.3 to 3.5 kHz audio bandwidth.

IV. Data Sources and Recording Techniques

IV. l. Carrier Level

The received carrier levels were recorded on magnetic tape during all test periods. The method of recording the carrier levels varied due to the different types of modulation used. For the FM-FDM system an LEL Model 5264 logarithmic amplifier-detector was connected to the AN/MRC-98 receiver at a point in the 70 MHz IF amplifier ahead of the limiter and the feedback point for the AGC. The detector output of the Model 5264 was recorded on magnetic tape using the FM recording mode. All received carrier levels for the FM-FDM system were recorded, i.e., two for dual diversity and four for quad diversity. The carrier level recording system was calibrated by connecting a signal generator to the antenna input connector of the AN/MRC-98 receiver and reading the output in terms of the frequency of the voltage controlled oscillator of the magnetic tape recording system. This method calibrates all components of the carrier level recording system simultaneously. The system was normally calibrated from -70 dBm to - 115 dBm.

The LEL Model 5264 logarithmic amplifier-detector was also used to record the received carrier levels for the PCM digital modulation system. The connection to the AN/MRC-98 receiver and the recording and calibration techniques were the same as those used for the FM-FDM system.

During the testing of the Martin Company PPM digital modulation system several methods for recording the received carrier levels were tried. As was discussed in Section III. 3. the RF carrier consisted of pulses of RF energy at four frequencies spaced 2 MHz apart and contained in a bandwidth of 8 MHz. A receiving system with an 8 MHz bandwidth was not available.

The receiving system had four IF amplifiers, one for each of the frequencies transmitted. Each IF amplifier had an AGC circuit that was controlled by the median signal level from the linear detector of that channel. However, the time constant of the AGC was on the order of seconds. The time constant was so long that the AGC did not follow the fast fading of the received carrier level. Thus, this recorded AGC is used to determine the magnitude of the received carrier level, but can not be used to study the fading characteristics of the carrier.

During the course of the PPM tests three different methods of calibrating the AGC voltages were used. These were:

- The AN/MRC-98 exciter or power amplifier through a frequency converter to the AN/MRC-98 receiver input at a pulse rate of 7812.5 pps.
- The AN/MRC-98 exciter or power amplifier through a frequency converter to the AN/MRC-98 receiver input at a pulse rate of 125 K pps.
- 3. A signal generator direct into the AN/MRC-98 receiver input at a pulse rate of 7812.5 pps or 125 K pps.

A comparison plot of the three methods of calibration is shown in figure 25. In this graph all curves have been normalized to curve number 2. The wide variation between the various methods has not been satisfactorily explained. The periods when each method was used are noted in Section VIII of this report.

During a portion of the test period on the PPM system a CW signal at 70.0 MHz was inserted with the four gated oscillators, discussed in Section III. 3., into the AN/MRC-98 modulator. The level of the CW signal was 10 dB below the peak power of the gated oscillators. At the receiving end a Communications Electronics, Inc. Model 960 receiver was connected to the AN/MRC-98 receiver at a point in the IF amplifier ahead of the feedback point for the AGC and the limiter. The Model 960 was tuned to 70.0 MHz and its bandwidth was set to 200 kHz. This system was unsatisfactory due to frequency drifts of the system.

During the tests of the Motorola deltaplex digital modulation system the received carrier level was recorded using the LEL Model logarithmic amplifier-detector discussed with the FM-FDM system. Since the LEL amplifier-detector has a bandwidth of 2 MHz, its bandwidth will include only frequencies f_5 and f_6 (see Section III. 4.). For these tests the information was carried on the frequency pair f_3 and f_8 , all other frequencies being driven by a psuedo-random pattern. Thus, f_5 and f_6 should contain one-fifth of the spectrum power, or 7 dB below full power. This system was calibrated using a CW signal generator with its output power level set to -7 dBm. The calibration was then performed using an external attenuator.

IV. 2. Signal-to-Noise

The Philco SNM-2 Signal-to-Noise Meter measures the ratio, in dB, of the signal power plus noise power to noise power in a voice channel of a multiplexed communications system. The signal used is a 2075 Hz tone from an audio signal generator inserted into a voice channel at the transmitting end of the path. The SNM-2 accepts the audio tone from the receiver demultiplex and passes it through a voice band filter. The 2075 Hz signal is then split into two components, noise and signal plus noise,

by a band rejection filter. The two components are put into diode logarithmic shaping networks and their difference taken. This process gives the ratio of signal plus noise to noise in decibels. For large ratios this will approach the true signal to noise ratio. The output of the signal-to-noise meter was a direct reading on a meter on the instrument and a varying d-c voltage for recording on magnetic tape. This system was calibrated using an audio oscillator and a noise source over a range from 15 to 60 dB.

IV. 3. Digital Data

Two sources were used for digital data transmission. The Frederick Electronics Corporation Data Transmission Test Set, Model 600, is a pseudo-random digital test pattern generator consisting of a transmitter and a receiver. The generator produces a repetitive test pattern, 2047 bits in length, at any rate from 10 to 100,000 bits per second. The receiver accepts the transmitted test pattern and synchronizes a locally generated perfect pattern to it. The two patterns are compared and errors in the received pattern are indicated by a voltage pulse output. The error pulses are widened from 2 or 3 microseconds to 200 microseconds by one-shot multivibrators and directly recorded onto magnetic tape. The error pulses are also counted in a Hewlett-Packard 524/560A printing counter. The number of accumulated errors is printed out every minute onto paper tape. The one minute print commands are given by a voltage pulse from an Astrodata Time Code Generator, Model 6140, used for time coding the magnetic tape recordings.

The Model 600 contains a mechanical counter capable of counting errors at speeds up to 20 per second. As errors occur they are stored in a 1520 bit capacity high speed buffer counter. The errors are then read into the mechanical counter at a 20 per second rate. Whenever the capacity of the high speed counter is exceeded a visual and audible out-

of-sync alarm appears. A voltage derived from the sync alarm light is FM recorded on magnetic tape for later use in evaluating the recorded error data.

The Frederick re-syncs on any string of 16 consecutive correct bits and consequently, if errors are occurring in the data at a rate greater than one in sixteen, the Frederick may not re-sync. During periods when the Frederick is giving an out-of-sync indication, it may indicate error rates up to 100% even though the actual error rate is smaller. Thus, the sync-outage as recorded must be used to determine the bounds for the actual error rates.

The AN/GSC-4 Data Modem Modulator/Demodulator, built by Collins Radio Corp. is a system designed for sending digital information over ordinary voice bandwidth channels of radio, wire, microwave, etc. communication circuits. The AN/GSC-4 accepts binary data at 600, 1200, 2400, 3600, 4800, or 5400 bits per second rates. Two or three data channels are encoded by phase shift modulation onto tones spaced 440 Hz apart in the frequency range 935 to 3195 Hz and transmitted through an audio channel. The digital data is detected from the received audio tones at the receiving end by another AN/GSC-4 Modem.

The AN/GSC-4 contains an Integral Test Facility. This consists of a 16 bit test pattern that is transmitted and compared to a locally generated perfect pattern in the receiving Modem. Errors are indicated visually and by a voltage pulse output. The recording of error pulses is the same as explained above for the Frederick. The receiving Modem resets synchronization between the transmitted and locally generated test patterns every minute in case of loss of sync.

The Frederick pattern was usually fed directly into a data channel for the digital modulation system but was always fed through the AN/GSC-4 into a voice channel, for the FM-FDM system.

IV. 4. Idle Channel Noise

The noise from an idle channel of each system, FM-FDM and the digital modulation system under test was recorded on magnetic tape. At the transmitter the channel that was to be used for the noise test was terminated with a 600 ohm resistor. At the receiving end the noise was amplified and recorded on the magnetic tape in a direct record mode.

For calibration purposes, it was assumed that the maximum noise would appear in the idle channel when there was no RF signal into the receivers. The peak-to-peak output of an audio oscillator was matched approximately to the peak-to-peak amplitude of this maximum noise. The audio oscillator output was then used to calibrate the direct recorded channel on the magnetic tape. The output of the audio oscillator was then stepped down in 3 dB steps as the signal was recorded on magnetic tape. Calibration in this manner provided good recording of the noise peaks, but was too compressed to provide a good recording of the average noise.

IV. 5. Teletype

During much of the test period a teletype message was sent over one voice channel of each system, i.e., FM-FDM and digital modulation system being tested. A standard fox teletype test message was used as a data input. These data were generated by a T eletype Corporation TS-2 Fox Generator which produces a 1275 Hz tone that is frequency shift keyed ±42.5 Hz. This tone was inserted into a voice channel of the multiplexer. At the other end of the path the message was taken from the system demultiplexer, fed through a teletype tone converter and printed out on a Teletype Corporation M-28 Printer.

Voice tests were made over the FM-FDM and various digital modulations systems using prerecorded tapes furnished by the U.S. Air Force Electronic Systems Division, Decision Sciences Laboratory, L. G. Hanscom Field.

The articulation test employed was the Modified Rhyme Test, [House, et. al, 1963; Williams, Hecker and Kryter, 1964]. Twelve (12) word lists - fifty (50) words per list - were recorded in an anechoic chamber on an Ampex Model 602 Recorder by six trained male talkers. The words were spoken one every 2-1/2 seconds with pauses at the end of each 50 word list. Thus the voice tape was approximately 35 minutes in length. This tape was played back over an Ampex 602 Recorder and transmitted over the path through a voice channel of both systems under test. The received voice from both systems under test was recorded on the two tracks of the Ampex 602 recorders for later analysis by ESD.

The voice tapes also contained special recorded signals used by the Speech Communication Index Meter (SCIM) discussed in Section V. 6. of this report.

V. Data Reduction Techniques

The data recorded on magnetic tape, as described in Section IV, above, were reduced in the laboratory. The following paragraphs describe briefly the data reduction techniques employed in reducing the data.

V. 1. Cumulative Amplitude Distribution

The cumulative amplitude distribution analysis is performed by a system shown in figure 26. The data are played back from the magnetic

tape at a tape speed of 60 ips (25 times the recording speed). The time track is played into the Time Code Reader and Control unit and is used to select the time periods to be analyzed.

The Distribution Analysis System (shown within the dashed line on figure 26) samples the data 20,000 times per second and compares the amplitude of each sample to ten calibrated signal reference levels. The Level Accumulators accumulate one count each time its associated signal reference level is exceeded by a sample. The Reference Accumulator registers a count for each possible sample within the time period selected. At the end of the time period all accumulators are printed out. From this one can determine percent of time each signal reference level is exceeded.

V. 2. Five Minute Medians

The carrier levels recorded on the magnetic tape were analyzed to determine the median of successive five minute periods. This analysis was performed using techniques the same as those used to determine the cumulative amplitude distribution. However, for the five minute periods all that was desired was the median, no information was required in the small percentage regions of the signal statistics.

To perform this analysis the ten Amplitude Comparators (figure 26) were divided into two groups of five and a separate Sampler used as the input of each group of five comparators. With this arrangement a five point cumulative amplitude distribution was run for two carrier levels simultaneously. The medians for the five minute periods were determined from these cumulative amplitude distributions.

V. 3. Digital Data Error Counting

The digital data errors (Frederick and GSC-4) were recorded on magnetic tape in a direct record mode as described in Section IV. 3. of

this report. The maximum error pulse repetition rate was near the high frequency limit of the direct record system for the tape speed of 2.4 inches per second which was used for data recording. As a result the pulse shape coming directly from the tape was very poor.

To properly recover the digital error data from the magnetic tape, the data from the direct playback amplifier was passed through a band pass filter and a pulse shaping circuit (see figure 27). The shaped pulses were counted by an electronic counter. Each decade of the counter had a staircase output. The first four decade outputs were recorded on separate channels of a strip chart recorder. Also recorded on the strip chart recorder were the recorded time from the magnetic tape and one related carrier level record (i.e., one FM-FDM carrier level when counting errors from the FM-FDM system, etc.). Thus, by referring to the time track it was possible to determine the number of errors made in any specific time period. Errors were counted continuously for each recording run and scaled to determine the number of errors in successive five minute time blocks.

As discussed in Section IV. 3. of this report, when the Frederick Model 600 receiver is out of sync the error information recorded on magnetic tape is not a true representation of the digital errors. The out-of-sync indication which was recorded on one channel of the magnetic tape was used to disable the error counting during out-of-sync periods. This was done by summing an out-of-sync voltage into the input of the pulse shaper to shift the error pulses out of the range of the pulse shaper.

However, total exclusion of errors during the out-of-sync periods does not give a true indication of the total errors committed either. The reason for the system being out-of-sync may be a higher error rate than the system can handle. Thus errors were counted including out-of-sync periods and excluding them as discussed above. These effects are discussed further in Section VIII. 1.

V. 4. Cumulative Amplitude Distribution of Two "Combined" Carrier Levels

The purpose of this analysis system was to determine the percent of time both received carrier levels of a diversity system were below given levels. The system used is shown in the block diagram of figure 28. The received carrier level data, which were recorded on magnetic tape, were played back through No. 1 and No. 2 data discriminators. The discriminators were adjusted to provide equal outputs for inputs representing equal received field strength, e.g., -85 dBm into each receiver would produce the same voltage out of the two discriminators, etc. By selecting the proper polarity for the bias voltage supply and the proper orientation of the two diodes, the output at the junction of the two diodes will follow the higher of the two carrier levels.

This "combined" signal was analyzed by the Distribution Analysis System (shown in figure 26). This is not the same as the distribution of the output of the combiner in the AN/MRC-98 diversity system. However, it should give a good indication of the possible effectiveness of the diversity system.

As indicated in the block diagram, figure 28, the time code on the magnetic tape is used to select specific periods of data for analysis.

V. 5. Crossings of the Five Minute Median

The system used to determine the crossings of the five minute medians does not give a highly accurate count of the median crossing, but does give a very close approximation. Since the distribution of the five minute periods are very nearly Rayleigh the crossings of the median are approximately equal to the crossings of the mean. The system used to obtain the crossings is shown in figure 29. The data from the Data Discriminator are averaged by a circuit made up by the 1 M A resistor, the 10 µf capacitor and A₁. The RC time constant was selected to be equivalent to five minutes in recorded data time. (The data were played back twenty-five times the record speed.) The averaged data and the non-averaged data were then compared by the difference amplifier, A₂. The output of A₂ was then passed through a zener diode clipper and a Schmitt trigger. This provided a squared wave which represented the crossings of the mean. These were then counted by an electronic counter. The staircase outputs of the first two decades were recorded on a strip chart recorder. This produced a continuous count of the crossing for each run. The crossings for successive five minute periods were obtained by referring to the time recorded on the strip chart from the Time Code Reader.

V. 6. Voice Tape Evaluation

The voice tapes recorded over the communications systems were evaluated for the intelligibility of the voice data and the SCIM data by the SCIM equipment.

For the voice analysis the received voice tapes were played back on Ampex 602 Recorders to groups of ten (10) listeners. The listeners were in a quiet listening room and were presented the received voice tapes monaurally to their preferred ear through a set of hi fidelity cushioned ear phones. From this listener response data the average intelligibility of each test run was computed (intelligibility = percent correct response by all listeners to all words) along with the standard deviation.

In 1947 Bell Telephone Laboratories [French, 1947] presented the theory for the articulation index (AI) which relates in a quantitative way the physical characteristics of a speech communication system and the intelligibility of speech as perceived by a crew of trained listeners.

This theory holds that the signal (speech)-to-noise ratio (in 20 narrow frequency bands) of a communication system will, when properly weighted and summed, provide an AI value that is directly related to the intelligibility of speech heard over that system.

The Speech Communication Index Meter (SCIM) [Kryter and Ball, 1964] uses the 9 band method as established by Kryter [1962] rather than the 20 band method of calculating the articulation index. The SCIM, however, accommodates additional factors affecting speech that are not involved in the original procedures for calculating AI. Generally speaking the use of AI and SCIM is predicated upon the assumption that the system is reasonably steady state during both the time the measurements are being made and during general use. This assumption is not met by a tropo system; however, by using conventional sampling statistics, it is probable that AI and SCIM calculations have some degree of validity. These data are presented in Table I.

V. 7. Idle Channel Noise

The idle channel noise of an unloaded channel was recorded on one channel of the magnetic tape in a direct record mode. On playback the noise data was passed through a direct playback amplifier and a bandpass filter having a bandpass equivalent to the normal channel voice band of the MRC-98 system. The noise was then amplitude detected to obtain the envelope of the noise. The envelope was analyzed with the Distribution Analysis System. This analysis yields a plot of the percent of time the idle channel noise exceeds given levels.

V. 8. Correlation Computer

The correlation computer [Johnson, 1961], shown in figure 30, is a special purpose analog computer designed to continuously perform

the multiplication and integration or averaging required in solving the normalized correlation equations [Florman, 1960].

Two random input signals, x' and y', are first applied to the servo controlled signal conditioning amplifiers. The function of these amplifiers is to amplitude condition the incoming signals so as to equate their variances over the averaging time to be used in the computation. The two conditioned signals, x and y, are then applied to a sum and difference circuit and then to squarers followed by averaging circuits. This succession of circuitry produces the variance of the sum of the signals and the variance of their difference as follows:

$$\sigma_{\mathbf{x}+\mathbf{y}}^{2} = \sigma_{\mathbf{x}}^{2} + \sigma_{\mathbf{y}}^{2} + 2\sigma_{\mathbf{xy}} = 2(\sigma_{\mathbf{x}}^{2} + \sigma_{\mathbf{xy}})$$

$$\sigma_{\mathbf{x}-\mathbf{y}}^2 = \sigma_{\mathbf{x}}^2 + \sigma_{\mathbf{y}}^2 - 2\sigma_{\mathbf{x}\mathbf{y}} = 2(\sigma_{\mathbf{x}}^2 - \sigma_{\mathbf{x}\mathbf{y}}).$$

By further taking sums and differences of the above equations the covariance, σ_{xy} , and the sum of the variances, $\sigma_{x}^{2} + \sigma_{y}^{2} = 2\sigma_{x}^{2}$ are computed. The correlation coefficient is obtained through the use of a second servo system which computes the ratio (K) of the covariance to the variance σ_{xy}^{2} .

$$K = \frac{2\sigma_{xy}}{\sigma_x^2 + \sigma_y^2} = \frac{\sigma_{xy}}{\sigma_x^2} = \rho = \frac{\sigma_{x^1y^1}}{\sigma_{x^1}\sigma_{y^1}}.$$

The Correlation Computer was used wherever the cross correlation of two parameters was desired.

VI. Editing and Comparing Data

Some data are not included in the analysis for various reasons, while other data which are included might be considered as valid for some purposes but not for others. This section describes some of the reasons for eliminating data completely and retaining data with limited usefulness.

The philosophy used in the analysis of data for this report was to include as much as possible so that it would be available in a condensed form for use at some later time for possibly some other purpose.

A preliminary editing consisted of removing data, for reasons such as power failures, bad tape, etc. as indicated by the logs kept onsite during the tests. A second editing was performed by visually inspecting the playback from the magnetic tape onto chart rolls. Data were removed again for "obvious" power failures (see Table II), errors in the time code and for conditions during which the data were outside the range of calibrations. What remained, then, is contained in Table III which is explained in Section VII.

Several conditions were observed which might effect the accuracy, or the consistency of the data. During the early parts of the tests, pre and post calibrations were frequently quite different due to unstable power supplies. Also, it was generally true that whenever the 5 minute medians for the two FM (or other) receivers differed by 5 dB or more throughout a run, the calibrations for the two receivers differed by the same amount, and when the medians did not differ, the calibrations did not. The runs for which the calibrations differed by 5 dB or more are listed in Table II.

Also listed in this table are those samples which show apparent aircraft effects, together with miscellaneous remarks which give reasons for omitting data, and observations concerning fading, power levels, etc.

The median signal levels given here are not strictly comparable for each of the systems. Although the medians for runs 1-52 for the FM and PCM show almost the same variation, the medians for the PCM are approximately 3 dB lower due to additional line losses. For runs 61-157, the carrier level was recorded by a different method for the PPM equipment than for any of the other systems, as noted in Section IV. Also, three different methods of calibration were used during these runs as noted previously. Figure 25 gives a rough estimate of the differences obtained by using these different methods, normalized to method 2. Additional differences were noted between successive calibrations using the same method. Moreover, the carrier levels for the digital system which were recorded during runs 61-157 were from the same receiver, at two different frequencies chosen from the four frequencies 67, 69, 71 and 73 MHz, while the two signals recorded for all other systems were from two different receiving systems using the spaced antennas. For runs 158-320, the carrier level for the delta-mod system was recorded by the same method as for the FM. However, the delta-mod used a wider bandwidth than the FM, and the LEL equipment did not have a sufficiently wide bandwidth to include the entire signal. At least part of the variability between the FM system and the digital systems from one run to the next is due to changes in transmitter power.

As with the medians, the error rates are not always comparable, the major difference being that two different systems, the Frederick and the GSC-4 were used to measure errors. However, differences also occurred within each system.

When the Frederick system was used, an out-of-sync pulse could be recorded as discussed in Section IV. Many times when it was recorded however, it could not be recovered from the magnetic tape for various reasons. The following observations were made for those periods for which the pulse could be recovered. Out-of-sync pulses occurred most

frequently for periods of high error rates. When the error rates were determined eliminating out-of-sync periods, they were changed by approximately 10% (i.e., an error rate of 10% would be 9% when out-of-sync periods were removed). Error rates greater than 10% are considered unreliable.

When the GSC-4 was used, an out-of-sync indication was not available for recording. It appeared that when the GSC-4 was out-of-sync, an error rate of 100% was recorded. The GSC-4 appeared to go out-of-sync for periods up to 1 minute. These apparent out-of-sync periods which were longer than a few seconds, are noted in the analysis.

The Frederick error counts taken from the magnetic tape agreed almost exactly with the minute-to-minute tabulations kept on site. However, the GSC-4 counts from the magnetic tape differed from the on-site counts, sometimes by large amounts. A possible explanation for this difference is that different types of pulses were used for recording and counting.

The median crossing rates for the different systems were generally comparable, with the exception of the Martin runs for which the different method of recording carrier level prevented fast fades from being recorded due to a long time constant in the equipment.

VII. Explanation of Table III (List of Data)

Table III contains the data remaining after the editing explained in the last Section. The listing gives the run number, the beginning of the 5 minute period (local time at East Island), the data rate, the number of channels, medians for two receivers (when available), the median crossings for the corresponding tracks, and (possibly) two columns of errors (percentages) together with the columns identifying the types of errors.

The final column contains remarks about the types of diversity used, whether the tests were looping tests, periods of obvious out-of-sync conditions for the Frederick or GSC-4, or periods when pads were put into the receiver.

The percent errors for the run may be obtained by averaging the percents for the 5 minute periods in that run, and a good approximation to the run median can be obtained by averaging the 5 minute medians.

Figures 31-49 show graphically the medians and errors from Table III. Figures 31-39 show both Frederick and GSC-4 errors while Figures 40-49 for the digital systems show only the Frederick errors. The median crossings from Table III are shown in Figures 50-74. Note that these are not always comparable, since some of the runs represented looping data, quad diversity, non diversity, etc.

VIII. System Performance

VIII. 1. Digital Data

Back-to-back tests were run on all of the systems in order to obtain information on the performance under steady signal conditions. The results of these tests for digital data are summarized in Figures 75-82. In these figures, different symbols are used to indicate the number of channels which were noise-loaded.

Figures 83-92 show the average of two recorded medians for a 5 minute period plotted versus the percent errors for that period. The different types of errors (GSC-4 and Frederick) are plotted on different graphs. Different symbols are used to denote the number of channels which were noise-loaded. Also noted on these figures are the data rates for those periods. All points on the lower boundary represent zero

errors. The limit of accuracy of the percentages is at least 10⁻⁴ and probably larger, since this represents an absolute accuracy of 7 counts in a 5 minute period.

These data have been severely edited with data removed for many reasons including the following:

Any data suspect of representing out-of-sync conditions has been removed. If an out-of-sync condition for GSC-4 data occurred during two 5 minute periods, the entire run was removed. If a power outage was noted in the log, the 5 minute periods preceding and following this were removed.

The PCM data shown in figures 86-87 are shown only for the runs after run 28 since equipment changes were made prior to run 28.

The PPM data are shown in 3 different blocks to correspond to the different methods of calibration used for those periods, as discussed in Section IV. 1. For runs 62-97 (figure 88) calibration method 2 (see figure 25) with 7.8 kpps was used. Runs 98-103 using the signal generator direct at 7.8 kpps and runs 104-112 using the signal generator direct at 125 kpps (method 3 in figure 25) are shown in figure 89. Runs 113-120 using the power amplifier through the converter at 125 kpps and runs 121-157 using the exciter through the converter at 125 kpps (method 1 in figure 25) are shown in figure 90.

As expected, the more data available the greater the spread of the data. However, one would expect that a more definite clustering of points would occur than appears in these data. Some of this spread is due to changing propagation conditions which can not be controlled, and some is due to factors which can be controlled. It is clear that every effort should be made to maintain standard operating conditions in the future tests, such as restricting the error measurements to only one type, adopting a standard bit rate for the tests, and obtaining immediate comparisons of calibrations in order to avoid possible uncertainties in the data.

VIII. 2. Idle Channel Noise

The idle channel noise was recorded directly onto the magnetic tape, as discussed in Section IV. The range was set to cover approximately -0 dBm to -25 dBm in order to record the peak noise. This range however, prevents obtaining a distribution of the noise. Only very occasional peaks (above -25 dBm from approximately .001 to .01 percent of the time) were noted. These peaks did not appear to correlate with errors. One possible explanation of this lack of correlation is that the idle channel noise was recorded from a different channel than the errors.

VIII. 3. Signal-to-Noise

The signal-to-noise for the digital systems appears to have an almost discrete character, i.e., it either appears at a high level or a low level. Thus, the distributions have a very sharp transition region between two level regions. As with the idle channel noise, the low regions of S/N did not appear to correspond with errors, or bursts of errors, and many errors occurred during periods of high S/N. Again, a possible explanation is that the S/N was recorded from a different channel than the errors. However, a visual inspection indicated that for 5 minute periods containing a large number of dropouts of S/N, there were also a large number of errors, and for periods with few dropouts, there were few errors. Since, for almost all runs, the median level, S/N, was the same as the high level S/N, the median was not useful for determining errors. However, it appeared that the percentage at which the transition from low to high level on the distribution occurred would correlate well with the errors for the same 5 minute period. A sufficently detailed analysis has not been performed to verify this.

For the FM system, the S/N had characteristics more nearly resembling those of the carrier, and even though the instantaneous correlation of S/N with errors was not good, the median S/N was more indicative than for the digital systems. However, throughout much of the tests, S/N could not be measured below 15 dB, and consequently, meaningful numerical estimates of correlation could not be obtained.

FDM and PCM systems should be compared from the standpoint of idle channel noise and also from the standpoint of signal distortion. It appears more appropriate to consider quantizing noise in the PCM channel to be equivalent to signal distortion of the FDM channel. PCM will have a relatively fixed level of quantizing noise whenever a signal is present in the voice band. However in the absence of signal the idle channel noise in a PCM channel is low due to the absence of quantizing steps.

IX. Propagation

All of the data from these tests appear to exhibit fading characteristics such as would be expected from "scattering". To a first order approximation, the short periods, such as the 5 minute periods used here, are Rayleigh distributed. The 5 minute periods were chosen as a result of preliminary analysis which indicated some variations between successive 5 minute periods of more than 6 dB. The variations between two minute medians within a 5 minute period were small. Because fade rates of 10 per 5 minute period were noted, a shorter period would not have been an adequate sampling interval. An indication that the 5 minute periods were not too short was that the spread of points for the 5 minute medians of figures 83-92 was only slightly larger than that of the comparable 30 minute periods.

The medians given here are not the same as the median transmission loss because these have not been normalized for the proper transmitted power. The transmitter power was varied from about 1kW, to 10 kW during the tests. At least one 40 minute run shows a variation of 6 dB (from 1 kW to 4 kW) during the run. These power variations will be accounted for in a later report. During the tests the medians varied from approximately -70 dBm to -110 dBm with a median value of 88.2, and are in general agreement with the previous data shown in figures 5-8.

The median crossing varied from 10 per 5 minute period to almost 200 per 5 minute period (the latter being somewhat unusual) with a median value of 28.

A number of runs were selected for more detailed analysis. If anything, these runs should be considered as "exceptions" because of the way in which they were chosen, although they do not differ much from what might be considered "typical". The runs were chosen to try to include all possible combinations of high or low median signal levels and high or low fade rates. Distributions for both receivers for these runs are shown in figures 93-103 for the 5 minute periods noted in the figures. The curves labeled 4 and 5, or 2 and 3 in these figures represent the percent of time the signals from both receivers are below the level indicated on the ordinate. This should give a good indication of the improvement that can be obtained by the use of diversity. Also given in these figures is the correlation coefficient between the signals from the two receivers. It is easily seen that the correlation coefficient would not give a good measure of the expected diversity improvement for most of these samples. The median crossing rates for each receiver for these runs are given in Table IV.

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Table I

Word % Correct and SCIM Scores - ITT FDM by Run No.

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
1	96.14	1. 80	. 95	. 06
2	96.02	1.54	. 96	. 03
3	96.36	1.71	. 96	. 06
6	96.96	1.47	. 96	. 07
7	96.36	1.35	. 96	.01
8	96.00	1.79	. 98	. 09
9	97.04	1.86	. 96	. 09
10	98.06	1.02	. 99	. 00
11	97.20	1. 43	. 98	. 02
12	97.62	1.59	. 98	. 01
13	98.04	1.22	. 99	.00
14	97.70	0.98	. 99	.00
15	97.44	1.50	. 99	.00
18	98.55	1. 27	. 96	. 04
19	95.44	1.62	. 97	. 03
28	96.16	1.50	. 92	.10
29	95.72	1.65	. 89	. 11
30	92.94	1.92	. 89	.10
31	93.50	2.12	. 89	.13
33	96.20	1. 87	. 97	. 05
34	95.14	1.45	. 98	. 02
35	96.04	1.73	. 95	.10
36	93.80	2.26	. 91	. 12
37	96.54	1.36	. 97	.19
38	96.84	1.84	. 95	. 22
39	95.36	2.11	. 94	.08
40	95.12	1.90	. 95	. 04
41	97.00	1.33	. 96	. 07
42	97.04	1.44	. 98	. 05
43	94.48	2.28	. 96	. 07

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
45	96.86	1. 41	. 95	.08
46	94.10	1.76	. 89	.11
47	95.38	1.89	. 87	. 16
48	94.52	1.88	. 89	. 12
49	95.06	1.93	. 91	. 11
52	94.08	2.06	. 91	. 12

Word % Correct and SCIM Scores - ITT PCM by Run No.

PCM	% Correct	Standard Deviation of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
2	72.96	6.37	. 55	. 34
3	77.64	3.38	. 55	. 31
6	69.16	6.62	.79	. 22
7	64.48	7.06	. 56	. 27
8	63.30	13.15	. 69	. 25
9	88.98	3.12	,75	. 21
10	84.10	4.56	.79	. 20
11	84.36	3.12	. 63	.20
12	93.70	2.34	. 86	. 1.8
13	94.42	1.83	. 83	.16
14	89.26	3.78	. 84	.16
15	90.24	2.47	. 69	. 24
18	NDA *	NDA *	. 40	. 30
28	92.94	2.39	.78	.15
29	97.26	1.51	. 83	.12
30	92.10	2.17	. 78	. 23
31	90.04	2.52	. 72	.18
33	96.40	1.31	. 90	.15
34	96.74	1.48	. 92	.04
35	81.92	8.55	. 65	. 32
36	85.04	2.55	. 59	. 28
37	87.36	3.19	. 80	. 18
38	95.64	1.64	. 89	. 08
39	87.46	2.86	. 74	. 28
40	92.84	2.61	. 80	.18
41	92.52	2.37	. 84	.17
42	94.46	1.70	. 89	.10
43	90.62	2.55	. 83	. 22

PCM	% Correct	Standard Deviation of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
45	96.90	1.48	. 83	. 22
46	93.08	2.80	. 80	. 22
47	94.18	4.67	. 81	.18
48	91.64	3.00	.78	. 21
49	95.66	1.85	. 86	.16
52	83.48	3.64	. 66	. 28

^{* &#}x27;NDA - No Data Available

Word % Correct and SCIM Scores - Martin FDM by Run No.

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
61	97.80	1.01	. 99	.00
62	96.70	1.75	. 90	. 12
63	97.74	1.20	. 98	. 02
64	96.00	1.66	. 92	. 07
65	NDA *	NDA *	. 91	. 13
66	94.66	1.70	. 84	. 11
67	94.14	2.06	. 83	.13
68	94.40	1.79	. 85	. 11
69	94.92	2.48	. 80	. 18
70	96.36	1.53	.79	. 16
71	93.04	2.61	. 85	.08
72	92.74	2.36	.77	. 16
73	95.56	2.58	. 91	. 11
74	NDA *	NDA *	. 94	.04
75	97.76	1.19	. 95	.03
76	NDA *	NDA *	. 94	.09
77	97.74	1. 40	. 98	. 02
78	96.44	2.42	. 99	. 26
79	96.26	1. 97	. 98	. 02
80	96.48	2.14	. 98	. 02
81	97.74	1.00	. 98	.03
82	96.60	1. 52	. 98	. 02
83	97.46	1.19	. 98	. 02
84	97.70	1. 47	. 98	. 02
85	98.20	1.11	. 98	. 03
86	97.30	1.33	. 98	. 02
87	97.88	1. 32	. 98	. 04
88	97.26	. 87	. 98	. 01
89	96.36	2.01	. 98	. 03
90	96.80	1.26	. 96	.06

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
91	94.16	4.08	.96	.05
98	95.56	1.44	. 93	. 12
99	96.36	1.68	. 95	. 05
100	94.06	1.98	. 83	. 20
104	94.46	2.34	. 91	.05
106	91.90	2.61	. 85	.11
107	93.34	1. 99	. 89	.10
108	95.20	1. 63	. 90	.10
109	93.90	1.86	. 91	.06
110	90.50	2.68	. 66	.19
112	96.80	1. 23	. 97	.03
113	91.22	2.64	. 97	.05
114	97.74	1. 43	. 98	.00
115	NDA *	NDA *	. 91	.10
116	96.70	1. 61	. 97	.01
117	96.26	1.90	. 95	. 02
118	96.84	1.39	. 88	.08
119	92.70	2.08	. 69	. 14
120	91.76	2.90	. 84	. 24
121	95.64	1.70	. 92	. 09
122	94.06	2.02	. 85	. 12
123	93.04	1. 97	. 88	.09
124	94.92	2.14	. 97	. 03
125	NDA *	NDA *	. 92	.11
126	93.14	2.14	. 82	. 15
127	93.86	2.05	. 83	.09
128	96.66	1.73	. 94	. 06
129	96.60	1.39	. 94	. 06
130	96.96	1. 50	. 96	. 04
132	96.06	1. 59	. 97	. 04
133	97.06	1. 49	. 97	. 05

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
134	95.90	1.56	. 98	. 02
135	96.36	1.46	. 95	.09
136	96.30	1.86	. 97	. 08
137	97.20	1.90	. 99	. 02
138	96.20	1.45	. 99	. 01
139	95.50	2.38	. 98	. 05
142	95.70	2.36	. 98	. 01
143	95.84	1. 61	. 98	. 03
144	NDA *	NDA *	. 98	. 07
145	88.10	2.73	. 59	. 19
146	96.86	4.35	. 57	. 20
147	94.76	2.09	. 83	. 13
148	95.12	1.75	. 89	. 11
149	94.92	2.87	. 88	. 15
150	NDA *	NDA *	. 53	. 21
151	NDA *	NDA *	. 54	. 19
152	89.16	3.52	. 69	. 18
153	91.76	2.44	. 64	. 15
154	92.46	3.08	. 79	. 11
155	94.64	2.03	. 90	. 16
156	91.74	3.31	. 89	. 13

Word % Correct and SCIM Scores - Martin PPM by Run No.

PPM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
61	91.96	2.45	. 32	. 08
62	64.68	6.40	.19	.06
63	91.62	2.98	. 52	. 12
64	72.76	5.32	.18	. 05
65	93.28	2.41	.36	.13
66	53.66	5.32	.16	.03
67	77.26	3.58	. 24	.08
68	81.34	3.97	. 34	.12
69	78.46	5.45	. 41	. 23
70	80.76	5.16	.39	.14
71	70.26	6.79	. 66	.07
72	67.44	5.61	. 26	.06
73	69.64	5.42	.06	.03
74	94.56	1.71	.35	.09
75	NDA *	NDA *	. 48	. 12
76	64.96	14.69	.06	. 02
77	96.74	1. 53	. 60	.11
78	86.48	3.33	.16	.11
79	81.52	3.10	.07	. 05
80	NDA *	NDA *	. 51	.09
81	96.04	1.66	. 61	. 07
82	NDA *	NDA *	. 69	.05
83	NDA *	NDA *	. 48	.10
84	97.30	1.29	.71	. 07
85	96.34	1.53	. 62	.11
86	96.54	1.57	. 56	. 09
87	85.88	4.40	.14	.08
38	90.84	2.60	.31	.11

PPM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
89	95.90	1.86	. 64	.08
90	91.94	2.08	. 34	.09
91	96.64	1.63	. 69	.03
98	83.24	13.24	. 56	.16
99	89.44	3.42	. 44	.18
100	46.80	6.32	.04	. 02
104	85.44	5.29	. 51	.16
106	73.14	3.83	. 47	.13
107	71.84	5.23	.30	.14
108	82.98	3.77	. 37	.17
109	80.84	4.39	. 33	.18
110	71.16	6.48	. 28	.17
112	95.66	1.67	. 63	.16
113	90.34	3.00	. 55	.14
114	88.72	2.94	. 33	.10
115	87.16	7.49	.11	.08
116	76.10	4.27	.20	. 12
117	87.90	3.40	. 34	.19
118	92.16	2.38	. 48	. 19
119	63.46	3.35	. 33	.13
120	87.66	3.48	. 53	.17
121	88.76	2.66	. 28	.16
122	85.28	2.60	, 48	.18
123	79.00	5.19	. 47	.16
124	91.88	2.15	. 40	.18
125	74.94	3.14	.15	.08
126	60.54	5.42	. 24	. 16
127	79.92	3.34	. 27	. 12
128	92.32	2.13	. 47	. 14
129	81.78	3.47	. 15	. 07
130	85.00	2.62	.18	. 07

РРМ	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
132	NDA *	NDA *	.20	.08
133	82.12	3.20	. 22	.10
134	81.78	3.68	.20	. 08
135	80.52	3.61	.23	.10
136	86.66	2.96	.25	. 05
137	89.78	2.76	. 33	.11
138	91.12	2.46	.38	. 09
139	91.08	2.77	.38	.13
142	NDA *	NDA *	. 26	. 07
143	94.94	1.86	. 49	.09
144	NDA *	NDA *	.20	. 12
145	87.16	2.90	. 32	. 05
146	90.56	2.62	. 33	.10
147	89.62	4.93	. 44	.10
148	NDA *	NDA *	. 27	.12
149	NDA *	NDA *	.17	. 08
150	NDA *	NDA *	. 51	.10
151	NDA *	NDA *	. 41	.10
152	77.68	4.76	. 22	. 13
153	79.24	4.44	. 24	. 13
154	92.40	2.22	. 34	. 09
155	85.62	2.62	.14	.08
156	84.96	3.89	.18	. 04

^{*} NDA - No Data Available

Word % Correct and SCIM Scores - Motorola FDM by Run No.

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
163	85.78	3.94	. 68	. 19
164	92.30	3.06	. 80	.13
165	93.04	2.05	. 80	.16
166	95.44	1.77	. 92	.10
169	94.48	3.21	.93	. 07
170	96.96	1.69	. 94	.08
171	94.74	3.91	. 97	.04
172	97.14	1.47	.95	.08
173	96.60	1.32	. 91	.10
174	93.86	3.68	. 92	.08
176	94.52	5.26	. 98	. 02
177	97.26	1.30	. 98	.06
178	NDA *	NDA *	. 98	. 05
179	97.46	1.83	. 94	. 07
180	97.30	1.51	. 97	.01
181	95.58	3.04	. 98	.00
182	95.20	1.74	. 91	. 05
183	93.00	2.13	. 82	.04
184	95.82	1.82	. 95	.08
185	87.46	13.14	. 78	. 05
186	93.56	2.33	. 77	. 05
187	93.36	1.94	. 83	. 17
188	94.36	2.33	. 83	. 12
189	83.80	3.82	. 65	. 20
190	88.48	6.94	.79	.18
191	81.48	12.36	.76	. 15
192	85.08	3.73	. 77	. 15
193	87.70	7.24	. 72	. 20
198	86.08	4.76	. 77	. 18

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
200	NDA *	NDA *	. 61	.18
201	82.36	4.48	. 64	. 21
202	88.88	2.78	. 73	.14
203	89.76	3.31	. 64	. 23
204	NDA *	NDA *	. 98	.00
208	89.94	6.42	. 93	.05
209	NDA *	NDA *	. 94	. 12
210	NDA *	NDA *	. 51	. 27
211	NDA *	NDA *	. 70	.16
212	NDA *	NDA *	. 70	.15
215	95.64	2.05	. 96	. 07
216	95.16	2.05	. 90	. 07
217	95.96	1.55	. 96	.01
218	94.58	1.70	. 90	.06
221	73.34	5.81	. 53	. 24
222	NDA *	NDA *	. 60	. 22
223	75.04	4.14	. 67	. 19
224	89.76	4.08	.74	.18
226	92.14	2.86	. 83	.10
227	NDA *	NDA *	.77	.18
229	NDA *	NDA *	. 92	. 07
232	NDA *	NDA *	. 83	. 05
233	NDA *	NDA *	.79	. 09
256	NDA *	NDA *	. 86	.10
257	NDA *	NDA *	.77	.01
258	93.84	2.26	. 67	. 24
259	93.96	2.33	. 78	. 12
261	96.56	1.38	. 80	. 02
262	92.08	2.20	.78	.01
263	NDA *	NDA *	.78	.03

FDM	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores				
264	NDA *	NDA *	. 94	.04				
265	95.94	1.91	. 87	.03				
266	96.00	1.82	. 87	.04				
267	97.24	1.77	. 90	.08				
268	96.56	2.10	. 88	.10				
270	98.18	1.24	. 90	. 05				
271	NDA *	NDA *	. 90	.04				
272	97.56	1.67	. 90	.08				
273	96.80	1.59	. 95	. 03				
274	96.86	1.85	. 90	. 07				
275	96.30	1.39	. 89	.05				
278	92.58	2.74						
280	91.80	2.69						
282	91.74	4.66	. 84	.09				
283	91.14	6.69	. 85	. 07				
284	94.44	3.22	.88	. 05				
285	96.20	2.26						
286	96.08	1.87	. 92	.08				
290	85.50	6.06	. 57	. 28				
292	89.92	2.91						
294	88.30	3.41						
279	58.32	5.79	. 45	. 05				
298	NDA *	NDA *	.36	.06				
299	NDA *	NDA *	. 48	. 17				
300	89.06	2.81	.72	.11				
301	85.62	3.68	. 70	.15				
310	91.00	3.02						
312	91.80	2.99		,				
313	89.42	3.65						
314	82.44	6.44						
315	90.56	2.91	•					
317	96.64	1.43						
318	80.36	5.05						

Word % Correct and SCIM Scores - Motorola Delta Modulation

Delta Mod.	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores				
160	95.04	1.97	. 85	. 07				
161	95.02	2.59	. 89	. 02				
162	95.84	1.70	. 89	. 01				
163	95.56	1.92	. 87	. 06				
164	95.04	2.01	. 77	.10				
165	94.50	1.98	. 88	.09				
166	94.78	2.68	. 92	. 02				
167	93.12	2.20	.76	. 20				
168	94.92	3.24	. 85	. 20				
169	96.44	1.88	. 91	. 02				
170	96.64	1.17	. 89	.08				
171	95.20	1.97	. 82	. 05				
172	96.60	1.39	. 89	. 04				
173	96.68	1.92	. 89	.04				
174	96.70	1.36	. 85	. 08				
176	95.80	2.12	. 90	. 02				
177	96.28	1.67	. 90	. 17				
178	92.94	3.11	.78	. 02				
179	95.30	2.10	.79	. 03				
180	97.64	1.29	. 80	. 04				
181	95.56	2.48	. 79	. 03				
182	93.70	2.51	. 77	. 03				
183	92.06	2.54	. 77	. 04				
184	NDA*	NDA*	. 80	. 12				
185	94.50	2.27	.78	. 15				
186	NDA*	NDA*	.77	. 16				
187	93.30	2.07	.76	. 02				
188	93.48	2.29	.79	.06				
189	86.02	4.31	. 64	. 25				
190	88.82	4.20	.75	. 11				

Delta Mod.	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores				
191	90.78	2.87	.70	. 14				
192	84.22	3.68	. 65	.16				
193	91.82	3.46	.78	.06				
198	92.16	3.05	.75	.07				
200	81.22	3.71	. 65	.13				
201	90.98	2.37	. 69	.16				
202	89.76	3.31	.70	.14				
203	NDA*	NDA*	. 65	.01				
204	NDA*	NDA*	.76	.10				
208	NDA*	NDA*	.77	.01				
209	NDA*	NDA*	. 83	.01				
210	NDA*	NDA*	. 52	. 27				
211	NDA*	NDA*	. 65	.18				
212	NDA*	NDA*	.78	. 09				
213	92.84	4.31						
214	92.34	3.45	40 40 40					
215	89.06	2.90	. 83	. 02				
216	NDA*	NDA*	. 80	.06				
217	92.12	2.00	. 83	. 02				
218	92.34	2.16	. 83	. 05				
219	93.50	2.28	. 63	.16				
220	93.38	2.21						
221	NDA*	NDA*	. 63	.16				
222	NDA*	NDA*	. 61	. 22				
223	80.56	1.65	. 57	. 06				
224	91.52	2.74	.79	. 09				
226	93.24	2.26	.78	.10				
227	90.66	3.40	. 82	. 07				
228	88.76	2.58	. 83	. 02				
229	NDA*	NDA*	. 84	. 02				
232	92.76	2.36	.78	. 02				

Delta Mod.	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores
233	87.38	5.48	.77	.08
235	91.38	2.70	.79	. 04
236	89.42	2.91	.76	. 03
237	88.20	3.18	.77	. 02
238	NDA*	NDA*	.78	.02
239	89.16	3.41	.78	.05
240	90.36	2.31	. 80	.04
241	.92.16	2.27	. 81	.03
242	92.04	2.29	.79	.06
243	91.56	2.36	. 80	.03
244	92.96	2.21	.78	. 03
245	92.92	1.90	.79	. 03
246	93.06	2.20	. 79	.04
247	92.18	2.47	. 80	. 03
248	86.82	5.00		
249	NDA*	NDA*	.71	.11
250	90.84	3.24	.76	. 04
251	91.52	3.07	. 82	. 03
252	83.04	5.08	. 68	.13
256	NDA*	NDA*	. 85	. 02
257	NDA*	NDA*	. 86	. 02
258	96.92	1.63	. 87	. 02
259	96.68	1.70	. 85	. 02
261	97.28	1.62	. 86	. 02
262	96.92	1.84	. 87	. 02
263	NDA*	NDA*	. 83	. 02
264	91.86	2.97	.76	. 04
265	90.88	3.56	.74	.01
266	91.02	2.57	.75	. 03
267	93.12	1.93	.75	.01

Delta Mod.	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores				
268	93.34	2.36	.76	. 04				
270	92.10	2.38	.78	.08				
271	93.70	2.08	. 80	. 02				
272	90.26	2.98	.79	. 02				
273	90.08	4.06	. 79	. 05				
274	87.70	5.07	. 80	. 02				
275	92.54	2.70	. 80	. 02				
277	92.52	5.77						
278	NDA*	NDA*	. 82	. 02				
279	NDA*	NDA*	. 83	. 02				
280	89.60	3.50	. 81	. 04				
281	NDA*	NDA*	. 83	. 02				
282	NDA*	NDA*	. 81	. 02				
283	NDA*	NDA*	. 81	. 03				
284	93.38	2.42	. 80	. 02				
285	91.40	3.01	.79	. 02				
286	89.84	3.91	.78	. 02				
287	NDA*	NDA*	. 68	. 21				
290	92.72	3.10	.71	.16				
291	90.36	3.42	.79	.06				
292	90.52	2.76	.78	.03				
293	NDA*	NDA*	. 80	.05				
295	88.64	1.21	. 80	. 04				
296	88.88	3.21	. 69	. 12				
297	69.6	6.06	. 32	. 15				
298	NDA*	NDA*	. 35	. 27				
299	84.14	4.56	. 49	. 16				
300	91.28	2.72	.70	.14				
301	NDA*	NDA*	. 63	. 17				
310	91.44	2.95	.78	. 03				
312	90.14	3.39	. 80	. 04				

Delta Mod.	% Correct	Standard Deviations of Errors	Average SCIM Scores	Standard Deviations of SCIM Scores			
313	90.94	4.43	. 81	. 02			
314	89.42	2.69	.71	.16			
315	89.86	2.76	.78	.03			
317	92.84	2.27	. 80	.07			
318	74.6	1.54	. 60	. 22			

О	Time Remarks		0455-0505	0615-0625			2205-2210	2300-2310	0020-0025		0935-0940	1235-1240	1705-1710	1135-1140	C Occurrence of possible aircraft	D Omit due to apparent power failur	
				Ü			74	7	•		0	-			O	н	
O	Time													1106-1108 1110-1113	receivers	pre & post	
Ø	Receiver	9	9	9						1					Calibration differences between receivers	Calibration differences between pre & post	
	i.						121								differ	n differ	
₹	Receiver	5,6	5, 6	5,6	9,6	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6	1, 3,5, 6	5,6	9 %	1, 3;5, 6		A Calibration	B Calibration	
	Run No.	-	7	m	4	'n	9	~	œ	6	10	11	12	13			

	Remarks		/	No post tape calibration												
Ω	Time	1405-1410					1740-1750	1150-1210								
υ	Time		1535-1538								1605-1607		1625-1626	1442-1444	1600-1602	
Ø	Receiver					9							9	•	9	4
<	Receiver												5, 6	5, 6	5, 6	9.5
	Run No.	11	15	81	19	28	62	30	31	32	33	34	35	36	37	*

	tun No. Rece	39 5, 6	40 5, 6	41 5,	42 5, 6	43 5,	44 5.	45 5,	46 1, 3;	47 1, 3;	48 1, 3;	49 1. 3;	52	29	63	,
4	Receiver	9	9	5, 6	9	5, 6	5, 6	5, 6	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6				
Ø	Receiver	5, 6	5, 6	5, 6	. ,	5, 6	5, 6	5, 6	5, 6	5, 6	9, 6	9, 6				59 Mc 73 Mc
U	Time							1316-1318								
Ω	Time															
	Remarks															

	Remarks						Omit period 1345-1350 due to bad time	Omit period 1435-1440 due to bad time	Code Omit period 1545-1550 due to bad time	epoc.	Omit period 1110-1115 due to bad time	e poo	Power failure G. T.I.	Omit period 1505-1510 due to bad time		
Д	Time												1342-1355			1607-1610
U	Time															
rī,	Receiver	69 Mc, 73 Mc	69 Mc, 73 Mc	69 Mc, 73 Mc	8	æ	8	٣	m							
4	Receiver		67, 69 Mc	67, 69 Mc	67, 69; 71, 73;1, 3	67, 69; 71, 73;1, 3	67, 69; 71, 73;1, 3	67, 69; 71, 73;1, 3	67, 69; 71, 73;1, 3	67,73	67,73	67,73	67,73	67, 73	67,73	
	Run No.	9	99	29	89	69	02	n	72	73	74	75	92	77	78	62

	Remarks		Omit period 1805-1810 due to bad time	ode				Calibration curves not available							No post tape calibrations for R x 69 Mc,	(3 Mc, 1 and 3
Q	Time	1649-1700			1933-1936											
υ	Time	·-														
М	Receiver			r.		73	73		29	29	19	29				73
∢	Receiver			1, 3	1, 3			Omit runs 86-87								1,3
	Run No.	80	81	82	83	20	80	98	&	89	8	16	92	93	**	86

	Remarks															
Ω	Time															
υ	Time				1628-1631	1644-1647						1054-1100				
Ø	Receiver	73	73	1	. 	Ā	1	-	÷	-	69, 71	-	1		1	Ā
<	Receiver	1, 3	69, 73			69, 73	69, 73	69, 73	69, 73	69, 73	69, 71				69, 71, 1, 3	69, 71; 1, 3
	Run No.	66	100	104	105	901	107	801	109	110	112	113	114	115	116	117

Run No.	Receiver	B Receiver	C	D Time	Remarks
		m			
		m			
	62, 69	29			
	69'29	29			
		67	1514-1517		
		44			
		29			
		73, 1, 3			
	67, 73	73			
	1, 3	. 1			
	1, 3	-			
	1, 3	7			
		-			
		-			
	1, 3	1,3	1245-1247	-	

	Remarks				Omit channel 4, R x 1 out 1622-1625						No pre tape calibration for R x 5 and 6	no signal on R x 5 and 6 No pre tape calibration for R x 5 and 6	no signal on $R \times 5$ and 6 Rapid fading channel 4, $R \times 5$	No signal on R x 6 channel 5		
ρ	Time															
υ	Time			1533-1537						1623-1626				1108-1110		
Ø	Receiver	1, 3	1, 3	1, 3	1,3				1, 5	1, 5						
<	Receiver	1, 3	1,3	1,3	1, 3	1, 3	1, 3	1, 3		1, 3;5, 6			1, 3	1, 3	1, 3	
	Run No.	151	152	153	151	155	156	157	158	159	160	191	162	163	161	165

			4 and 5	Omit channels 4 and 5; Omit channels 2	and 3 (1345-1350) due to power failure		No Run 171 recorded; High signal on Run 172 caused data to go out of range on all			orded		Data unreliable for these runs				
	Remarks		Omit channels 4 and 5	Omit channels	and 3 (1345-135		No Run 171 rec	receivers		No Run 175 recorded		Data unreliable				
Д	Time			1345-1350												
υ	Time				1613-1616											
Ø	Receiver		5, 6	5, 6	5, 6	5, 6										
∢	Receiver		5, 6	5,6	5, 6	5, 6	Omit rune 171-172			Omit run 175	1, 3	Omit rune 177-178	5, 6	5, 6	5, 6	1, 3;5, 6
	Run No.	166	167	168	169	170	171 Omi	173	174	175 Omi	176	177 Omi	179	180	181	182
								44								

	Remarks		No record on sanborn charts		Rapid fading on channels 4 and 5 at 1345-	1350										
Ω	Time															
υ	Time															1625-1628
Ø	Receiver							1, 5	1, 5	1, 5	1, 5					
∢	Receiver	1, 3;5, 6	un 184			5, 6	9,6			1, 3;5, 6	1, 3;5, 6				1, 3	1, 3
	Run No.	183	184 Omit run 184	185	186	187	188	189	190	161	192	193	194	195	196	198

	Remarks		All channels either limited on tape or in	transmitting or receiving (particularly 5) All channels either limited on tape or in	transmitting or receiving (particularly 5) All channels either limited on tape or in	transmitting or receiving (particularly 5)						All channels either limited on tape or in	transmitting or receiving All channels either limited on tape or in	transmitting or receiving All channels either limited on tape or in	transmitting or receiving	
Д	Time															
U	Time	1154-1157				1039-1053										
Ø	Receiver					7	-	-	7	1						
<	Receiver								1, 3	1, 3	1, 3			1, 3;5, 6		
	Run No.	200	201	202	203	204	205	902	207	208	503	210	211	212	213	214

	Remarks	High signal level		High signal level	Omit channel 4, R x 5 at 1335 to end of	run (signal out of range) High signal level going out of range 142	1440 and 1455-1500	Omit channels 4 and 5 for period 0945-	0950 (transmitter off at 0948)							
Ω	Time							0945-0950								
υ	Time															
Ø	Receiver				1, 3;5, 6	1, 3;5, 6	1, 3;5, 6		ĸ	Ŋ	ĸ	'n	្ស	S	\$	ĸ.
∢	Receiver															
	Run No.	215	216	217	218	219	220	221	222	223	224	225	526	227	228	525

	Remarks			Low signal level on channel 5, $R \times 6$												
Q	Time															
U	Time															
Δ	Receiver	ĸ	ĸ	ů,	, I					1	1	1	1	-		
∢	Receiver		5,6	5, 6	5, 6											
	Run No.	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245

246 247 249 250				
20				
253				
254		-	ν.	No pre tape calibration for R
255	1, 3	Ħ		
256	1, 3;5, 6	1, 5		Rapid fading
257	1, 3;5, 6	1, 5		
258	1, 3	1, 5		
259	1, 3	1,6		
260	1, 3	1, 6		

			Channel 3 has break or disturbance in	. 555												
	Remarks		Channel 3	signal at 1555												
Δ	Time															
υ	Time										1041-1043	1130-1132				
Ø	Receiver	1, 6	1,6	1,6		1		•	r	r	ĸ	មា	s.	s	۱ń	ч
<	Receiver	1, 3	5, 6	5, 6	1, 3;5, 6				1, 3;5, 6	1, 3;5, 6	5,6	5, 6	9.6	3,6	5, 6	7 3
	Run No.	261	292	263	264	592	566	267	268	569	270	172	272	273	274	276

	Remarks	Rapid fading channel 3	Rapid fading		Channel 2 is noise limited from 1620 to	end of run				1609-1614		Rapid fading		Channels 2 and 3 are noise limited	Channels 2 and 3 are noise limited	Channels 2 and 3 are noise limited
Ω	Time															
υ	Time					1139-1141	1303-1307									
Ø	Receiver															
<	Receiver	1, 3	1, 3	1, 3	1, 3	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6	1, 3;5, 6		5, 6				
	Run No.	278	279	280	281	282	283	284	285	286	287	290	291	262	293	295

	Remarks									High signal level	Rapid fading	Rapid fading	High fade rate	High fade rate	High fade rate	No post tape calibrations R x 1
Q	Time															
υ	Time															
Ø	Receiver		1, 5	1, 5	1, 5	1, 5	1, 5				-	-			-	
<	Receiver					9,6	5, 6							1, 3	1, 3	
	Run No.	962	297	298	562	300	301	303	304	305	306	307	308	309	310	312

Q

B

250 250 250 250 300 11MF RATE CHS - 40.0 505 505 505 505 505 505 505	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	35 35 35 35 35 35 35 36 36 36 36 36 36 36 36 37 37 37 37 37 38 38 38 38 38 38 38 38 38 38 38 38 38	47 40 47 50 50 50 50 50 50 50 50 50 50 50 50 50	FRENCE FRENCE O.5330	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	E R R R R R R R R R R R R R R R R R R R	2
255 255 250 250 300 11 of tate CHS 510 520 520 520 520 520 520 530 530 530 530 530 530 530 53		25 17 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	17 NO 50 SE	FRED POPE	TO T	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8. F.
250 250 300 300 510 510 520 520 520 520 520 520 600 600 600 600 600 600 600 6		25 12 2 1 1 2 1 2 2 2 4 2 2 2 4 2 2 2 4 2 2 2 4 2 2 2 4 2 2 2 4 2 2 2 2 4 2	77 NON TY NONE	F R R R R R R R R R R R R R R R R R R R	TYPE NON TYPE NON EN	28 88 08 08 08 08 08 08 08 08 08 08 08 08	REAL
11	י של משל מ	SSINGS 33 33 34 33 34 33 34 34 34 34 34 34 34	TY DE TYPE ASSETT ASSET	F R R R R R R R R R R R R R R R R R R R	7 N N N N N N N N N N N N N N N N N N N	E 22 02 02 02 02 03 03 03 03 03 03 03 03 03 03 03 03 03	REM
11 ME HATE CHS - 44.6 550 550 550 550 550 550 550 550 550 55		33 35 35 36 36 36 36 36 36 36 36 36 36 36 36 36	17.55 NONE 17.75 1	FRENCE FRENCE O.5330	1	28 28 08 08 08 08 08 08 08 08 08 08 08 08 08	REMARKS
11		35 35 34 34 34 35 36 36 36 36 36 36 36 36 36 36 36 36 36	17 NO 50 SE	FR ROLL 0 -5330	FIN BE	ERROR CRAOR	REMA
11 MF HATE CHS 505 510 510 510 510 520 600 600 600 600 600 600 600 600 600 6	6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00	SSINGS 34 34 34 35 35 35 36 36 36 36 17 17 17 17 17 17 17 17 17 17 17 17 17	17 A DE TYPE AC TYPE A	######################################	F.M M.M.	ERROR CAROR CAROR	REMA
505 515 516 517 518 519 510 510 510 510 510 510 510 510		34 31 34 35 36 36 24 24 24 24 17 17 17 17 17 18 18 18	NONE TYPE SSC4	E KROH 6 RROH 0 - 5330	NONE NONE	E RROR	
510 525 525 525 525 525 525 525 505 50		31 34 35 35 36 36 37 30 24 24 24 17 17 17 17 17 17 17 17 17	17 PE 17 PE 35 C &	E RROH FRROR 0.5330	TYPE	FROR	
515 520 520 520 520 520 520 520 520 520 52	\$\$\$\$ \$\$\$\$\$ \$	34 35 35 35 30 30 30 30 30 17 17 17 17 17 17 17 17 17	17 PPE 17 PPE 17 PPE 18	E HROH FRROR 0.5370	NON	ERROR	
520 525 525 550 550 560 605 500 11ME 24TE CHS 190 150 1510 1525 1510 1525 1510 1525 1510 1525 1510 1525 1510 15	ቁው ፍጋልዳ ሴኮፋውስውክ (ኮሪ ኮሽ።ስ ጋኮፍሠውሳው (36 35 36 39 24 24 24 24 24 17 17 17 17 17 17 17 18 18 18	17PE 40VE 17PE 65C4	E HROW F RROW 0.5330	NON	ERROR	
525 555 605 605 605 605 605 605 60		35 35 35 35 35 35 35 35 35 35 35 35 35 3	17 AO ≥ 17 AO	E HROF RROR 0.530	NONE	ERROR	
114E AATE CHS AEDTAN 5550 AEDTAN 5550 ATE CHS		35 1 1 2 2 4 2 2 4 2 2 4 2 2 4 2 2 4 2 2 4 2 2 4 2 2 4 2 2 4 2 2 4 2 2 2 4 2	17 N V V V V V V V V V V V V V V V V V V	E HROH FRROR 0.5330	NON	ERROR	
553 560 600 600 605 1000 1500 1500 1510 1510 1510 1510 1510 1510 1610		30 24 24 24 24 24 24 17 17 17 17 17 17 17 17 17 17 17 17 17	17 17 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	FR000	NONE		REMARKS
555 605 1506 1506 1507 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 1508 16	្រែក្រុង ស្រុក្សិក្សាទីស្មា (ស្រុក្សាទីស្មាទីស្មា (24 24 24 24 24 24 17 17 17 17 17 17 18 18 18 18	179E 6SC4	FRR0R 0 • 53 3 0			•
605 605 11 ME 24TE CHS 1604 1500 2400 24 145.7 1510 1525 1510 1610 24 145.7 1510 1610 24 185.4 2040 24 185.4 2055 2400 24 185.4 2055 2400 24 185.4 2150 245.5 2150		24 24 24 24 17 17 17 17 17 18 18 18	1745 6504	FRROR 0.5330			
11ME PATE CNS 1605 1505 1506 2406 24 - 64 - 7 1510 1510 1510 1525 1510 1646 2045 2045 2055 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2106 24 - 85 - 4 2055 2107 2106 24 - 85 - 4 2055 2107 2106 24 - 85 - 4 2055 2107 2106 24 - 85 - 4 2055 2107 2106 24 - 85 - 4 2055 2107 2107 2107 2107 2107 2107 2107 2107		25 1465 17 17 17 17 17 17 17 17 17 17 17 17 17	7 Y PE 6 S C 4	ERROR 0-5370			
11ME PATE CMS MENTAN 1500 24 -84.7 1500 2400 24 -84.7 1500 1500 1500 24 -83.5 1500 2400 24 -85.9 2000 24 -85.5 200		17 17 17 17 17 17 18 18 18 18 18 18	776E 6804	E-RROR 0.5370	100		
1500 2400 24 -86-7 1515 1515 1515 1515 1515 1515 1515 151	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	17 11 17 11 12 11 12 12 12 12 12 12 12 12 12 12	65C4	0.5370		00000	200
1515 1515 1515 1515 1515 1515 1515 151		17 17 17 18 18 18 18 18	4000	0.5310	3 1	THE PARTY	NC MANN S
1555 1510 1510 1520 1520 1520 1646		12 15 15 12 15 15 15			MONE		
1515 1515 1515 1515 1526 1530 11mE Hale CHS Has Has 1 1530 2045 2045 2045 2055 2100 2140 2150	A 2	17 15 12 12 15 15 15 15		0.00.0			
1515 1520 1520 1530 1146 2035 2045 2045 2055 2055 2145 2145 2150 2150 2150 2150 2150 2150 2150 215	188.9 186.5 186.5 185.6	15 12 12 15 15 0551NGS		0.0000			
1520 1525 1530 1130 2035 2040 2040 2040 2050	-85.6 -85.6 -85.6 -85.6	12 12 15 15 15 15		0.0000			
1525 1530 114E HATE CHS HABIAN 2035 2400 24 -85.4 2040 2040 2040 2050 2050 2100 2135 2400 24 -85.5 134E HATE CHS HENTAN 2140 2150	-86.5 -85.6 ANS	12 15 15 15 15		0.000			
1530 114E HATE CHS HEILAN 2035 2400 24 -95.4 2045 2055 2055 2055 2100 24 -95.5 2100 2100 2100 2100 2100 2100 2100 210	-85.6 ANS	SSINGS		0.0000			
11ME HATE CHS MEDIAN 2035 2+00 24 -85.3 2045 2045 2055 2055 1ME HATE CHS -85.5 2135 2+00 24 -85.5 2136 2406 24 -86.5 2146 2146 2406 24 -86.0 2150 2406 24 -86.0 2150 24 -87.4 2150 24 -87.4 2150 24 -87.4 2150 24 -87.4 2150 24 -87.4 2150 24 -87.4 2150 24 -87.4 2150 24 -87.4 2150 2500 24 -87.4	ANS	SSINGS		0.0000			
2035 2400 24 -85.4 2045 2055 2400 24 -85.4 2055 2055 2055 2055 206 2136 2406 24 -86.7 2145 2406 24 -86.7 2156 2156 245 -86.7 2156 255 2606 24 -87.4 2156 256 24 -87.4		**	TYPE	FRROR	TYPE	ERROR	REMARKS
2046 2055 2055 2100 2135 2145 2145 2156 2156 2156 2156 2156 2156 2156 215	70		4259	00000	ANCW.		
2045 2055 2055 2056 2100 114F HATE CHS -85.6 2150 2409 24 -80.7 2145 2150 2150 24 -87.4 2150 2150 24 -87.4 2150 2150 24 -87.4		2		00000			
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2100 KATE CMS 4601AN 2135 2409 24 - 80-7 2145 2145 2150 2150 2150 2150 2150 2150 2150 215	_			0000			
2135 2400 24 -80.7 2145 2145 2145 2156 2200 245 -65.0 2200 2200 245 -65.0 2200 245 2155 2155 2200 245 2155 2155 2155 2155 2155 2155 2155	• -	. <u> </u>					
2135 2409 24 -80.7 2145 2156 -65.0 2156 -67.9 2155 -67.9 2200 -67.9 1166 -47E CHS -60.0	ANS	SSINGS	TYPE	FREDR	TYPE	FDROB	REMARKS
2140 2150 2150 2155 2200 2200 1140 2200 2200 2200 2200 2200	-63.6	15	4389	0.0160	JNON		
2150 2150 2200 2200 11ff wate CHS - Weblan		*		0.0130	?		
2150 2155 2200 2200 2200 2200 2200 2200	_	-		0-0170			
2200	_	16		0.00.0			
2200 - PATE CHS MEUTAN		15		0.0140			
TIME HATE CHS MEDIAN		2		0.000			
2036 3400 34	ANS MEDIAN	CROSSINGS	TYPE	FREDO	TVPF	60800	PFUADKS
	-86.5	3.5	4789	0.2400	NONE		•
2240	•		1000	4.60			
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		2.		0.000			
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	EDIANS 1 183.3 1 1883.7 1 1883.7 1 1884.7	Z	FUIANS 177-2 177-7 175-4 175-5	UIANS 178.5 178.5 176.2 176.2 178.5 178.5 17.9 17.1 17.1 17.2 17.2 17.2	FCI IAN 3
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TYPE	6050											TVDF		6SC4							1404	1	NON										TYPE	65C4										TYPE	6SC4						TVPE	2050	1		TYPE	FRED	1							
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EUZANS	-A1 - 1		-86.4		-06.5	A. CH-	200	-6	-A1.7		-10.4	FUTANS		-88.2	4.00	- 6.6-	-61		7 - 1	-88.1	FOTANS		-63.4	-020	7 60-	****	4. C6-	6 60	2026	-92.3	4	0.00	EDIANS	+-96-		0.04	-97.2	-97.3	- 67	2016	-97.7	-07.0		MEDIANS	-95.5	-93.7	40		4006		MEDIANS	7.96-	3	4.04	MEDIANS	96.6	94.6		2056	-93.4	-93.8	4 40-		-93.2
MED	-81.4		0. I	6	A.Tu	A 18-		E - 18-	8.00		-78°B	AF.	•	-87.2	1 500	- 40	4.00-		2006-	-87.S	3	1		7.60-	40	0.4	-63.B	00	173.0	-43.2		0.57	MED	4.56-		5.00	9.96-	-96-2	0 90	14304	-96.5	A . 20-		MED	-05.8	7-56-	-05		7.46	-94.6	MED	105° X	96-	0.04	MED	-46.5	-06.1	. 70	-40-3		-95.5	•	•	•
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REMARKS								DENABRE								RFHARKS								REMARKS	NO SYNCH				NO SYNCH		REMARKS							REMARKS							Series Series	CAMERIC					
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FRROA	0.2100	0.1900	0.110	0.000	0.060		0.000			0.720	00000	122000	61000	0.00.0	0000	FROCE	0.0010	0.0025	0.2200	0.0650	0.1100	0.0420	0.0140	ERROR	14.4100	2.1400	3.1600	3.3000	27.1300	2.7000	FRROR	4.3000	3.0000	3.9000	2.6800	2.3900	4.R200	ERROR	•							NO NA					
TYPE	FRED							TYPE	2000	1361						TYPE	FRED							TYPE	6504						TYPE	4000						TYPE	MACN						100	NOW O					
SURSSINGS	94	10)	15	ž	, <u>~</u>		? . ₹	SOSSINGS	53	9	9	e a	0 10	9	7	SSN15505	\$	55	Ç	56	73	65	20	SUZENES	9	5	4	92	25	46	SONISSON	2 4	6 4	4	33	;	56	SUZZE	36	25	7	6	Ç !	37	POCETMEN	AF.	4	1	47	65	1
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EULANS	-00-	-91.1	-86.5	-84.6	-85.			WEUTANS	-46-5	2.88	- BB -	2.48		-86	-84	Z		-84°C	-67.3	-87.7	06-	-94.9	-85.0	Ž	D. 80-	-87.4	-87.7	2.88-	0.69	1-00-	Ž	200	-07.4	06-	9.06-	-91.0		Z	5-16-	1.06-	-00	200			FUTANS	-86-0	C. 584-	-86.2	-86.7	-85.6	
Ŧ		-03.2	-A8.7	-P6.4	-49-	63.5	000	MEUT	4.04	6.03	9	4.70	9 68	196.7	F. 6. 2	3		-85.6	E. 20	4.68-	-01.0	-RB.7	•	<u>.</u>	0.0	- d - 3	8-14-	0.64-	0.04		_	9	2000	E-00-	0.00-	٦٠١٠٩	_	<u> </u>	9.64-	-40.3	D	0.00		0.65	. 2	-8-	C. H.	7.44-	-H4.7	-84.3	
CHO	5							CHS	7	:						CHS	24							CHS	\$					9776	£ 6	Ü						CIE							CHS	!					
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TITE	1305	1510	1515	1520	1525	1530	1535	TIME	1605	1610	1615	1620	1625	1630	1635	TIME	1750	1755	1900	1805	1810	1615	1820	I ME	1330	1335	0461	C+5 T	0001	1 335	367	1430	1435	1440	1445	1450	1455	1	1535	3467	1967	1666	1600	1405	TIME	1625	16.30	1635	1640	1645	
200	35							S	33							SON	ŧ							2	32						5 6	2						200	7						NOW	38					

FON	DATA										
200	1146	MATE	CHS	MEDIANS		MFRIAN CRUSSINGS	TYPE	FHROS	TYPE	ERROR	REMARKS
6	120	· 0+2	2	4.73-	-87.7		*259	6.0000	NONE		
	125			4.48-	-87.3	50 45		00000			
	730			1.68-	-8h.	-		0.000.0			
	735			0.74	-87.			0.0007			
	5 1 1 1			-KH-	- 94° -	55		0.0010			
	750			2.4.5	- 44-7			40000			
5	JIME	RATE	C.	MEDIANS	ANS	CRUSS	TYPE	FFBOG	TYPE	ERROR	REMARKS
0	470			-49.3	-91.n	64 74	NONE		NONE		
	515			-46.2	-63.3	41 42					
	924				0-16-						
	C C			TO TO	10 a	35					
	635				C	76					
	H			- TI	-63-1						
RUF	TIME	RATE	CHS	MEIN	SAV	CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
7	£=5.			2.74-	7.68-	6+ 0+	NONE		NO.N		
	e -			-44.5	-88.7						
	2 2			4.4.4	7.58-						
	200			7. C.	-86-	•					
	5			7 . CH	-24.5						
	25.5			[-23-]	V 4 4 5						•
3	44.47		2		200	24 25					
5 3	3000	200	5	1 (1)	ENS	80000		HOOM	404	ERMOR	REMARKS
1	1010		•	9 0 0 1	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		\$259	2200-0	NON		
	1015			7 7 1	180	30 00		000000			
	1920			4.0×	-70.4			0.000			
	1025			- (4.	-70.5			0.000			
	1030			4-64-	4 · E	12 71		0.0003			
	1035	,		-79.5	-81.c	~		0.0007			
5	-	RA .	SES	MFIJ	ANS	CROSS	TYDE	FRADA	TYPE	ERROR	REMARKS
•	5077	(40.)		7.62	1.74		6SC4	0.0010	NONE		
	1116			- R 3 - 5	303			0.0015			
	1120					22 50		E000-0			
	1125			1 1	- 46. 2						
	1130			-44.7	-87.7	# Pu		0.0040			
	1135			4.00	-E.V.			0.0003			
25	114	RATE	CHS	J (13W	ANS	CROSS	TYPE	EHROS	TYPE	ERROR	REMARKS
*	1205	1400	* 2	73.5	-75.3		920	000000	NONE		
	26.5		٠	11/0	78.0	171		0.000			
	500			2007	V	52		0.0046			
	1236			-74.5	7-69-		•	0.0130			
	1235			3.74-	-81.5	20 17		0.0210			
200	TIME	RATE	CHS	4ED1	ANS	CROSSI	TYPE	FRROW	TYPE	ERROR	REMARKS
45	1250	2400	2	-73.1	-75.1		65C4	.021	MONE		
	1255				-77.2			0.0000			
	1300			-77.9	-74.5	19 22					
	200			175.3	14.4	82					
	3161			173.0	40.4						
	1320			C. T.	1019	51 46					

		ST.U	4E to 1	MEUT ANS	MEDIAN CROSSINGS	INGS	TYPE	EPROR	TYPE	ERROR	RFWARKS
9. 4.6	0042 99	*	45.	-91.6		35	65C4		MONE		
			- 43-	-65		, [0.0640			
>	90		4.50-	95.0		33		0.0840			
5	905		1.55	7.50		0		0.0400			
3	01		100-	1-56-		11		0.3000			
5	5		6.40-	-95.5	5.9	¥.		0.4400			
•			7.50-	7-50-	36	7		0.3100			
AUN TIP	ME RATE	CIS	1034	Z	MEDIAN CROSSING	INGS	TYDE	FREGG	TYPE	ERHOR	REMARKS
~		2	-42.5	9.26-	39	34	4089	0.0330	HUCH		
10	01		F-40-	H. V6-	64	0.4		0.1900			
101	5		105.4	E-96-	94	45		0.4400			
			-65.5	+-56-	**	94		0.1600			
		S	MF.U.	MEDIANS	MEDIAN CROSSINGS	INGS	TYPE	FREDR	TYPE	ERROR	REMARKS
		2	H. +C-	-93.1	43	**	4359	0.0180	NOW!		
11	16		6.071	4.16-		32		9.0120	:		
111	15		4.50-	-63.4		25		0.0430			
115	e .		-03.3	-94.0		35		0.0000			
112	5		-45.5	-96-		35		0.6500			
11	30		-05.1	H. 76-		32		0.400			
			-97.1	-45.1	35	27		0.2230			
		CHS	JUB/	ANS	CROSS	INGS	JCXL	ERROR	TYPE	ERROR	REMARKS
49 140	15 2400	2	-05.6	-45.7	31	56	FAED	0.0450	NONE		
141	6		1.00-	-63.6	36	34		0.0240			
1+1	5		B.64.	8-16-		36		0.0170			
14	3.		e · ra ·	8.26-		5		0.0470			
-	S.		F. 16-	104.4		34		0.00 HH			
-	2 1		E. X	-65.1		28		6.0045			
		97.0	* úo-	-93.4	£ 4	36		0.0510			
NOW	7	£3	10.4.	₹.	CAUSS	INGS	TYPE	FREDR	TYPE	ERROR	REMARKS
		2	U . / 0-	-100.0		7.	4259	0.1800	NONE		
10	5.5		-65.3	-0H-0		28		0.1750			
<u>.</u>	. ·		200	T. T.		٠.		0.1500			
6	<u>.</u>		200	0.00		¥ .		0.1000			
				***		٤		0.00			
1 2			1040	107				001.00			
		CHS	Taries.	3	CUCK	TNE	TVOF	0000	202	9090	37071130
62 145	55 2400	2	F - F -		2		A J S S	0.1547	PACIN	2004	
					, -		;	0-1620			
15	ý.		2.56-		64			1.1205			
15	2		-01.7		35			A-2378			
15	Š		2.47-		ńń			0.774R			
15.	0		-43.5		63			0.1710			
			-63.4		55			0.1630			
	AE RATE	CIS	HEDIANS	ANS	HEDIAN COOSSINGS	SSAI	TYPE	FHROR	TYPE	ERROR	REMARKS
3 155	0		-41.5		27		NON		NONE		
12	25		4.64-								
1600	00		C. F. H.		7						
15.	5		-13.2		2.5						
9	<u>c</u> (9 - Lu-		ç: ;						
0	r.		9-23-		30						

REMARKS								DENABLE								REMARKS								970	MEMAKE S							NO STREET	KEMAKKS							REMARKS								REMARKS						
ERROR								9090	Lund							ERROR								0000	CHACK								EMMON							ERROR								ERROR						
TYPE		NONE						1404	NONE							TYPE	NONE									MONE								NONE						TYPE	NONE							TYPE	NONE					
ERROR	0000	000000	0.000	0.00.0	0.000	0.000			0000		00000	000000	0.0000	0.0000	0.000.0	ERROR	0.2900	0.1350	0.220	0.2010	2010	000		40000	2000	0 5 2 5 0	0-2340	0.3040	0.0790	0.1450	05.01.0	00000	NAME OF THE PERSON OF THE PERS	05-1-0		0.140	00000	00000	05130	FRROP	0.0000	0.0430	0.1390	0.3560	0.2200	0.1320	0.3630	FRROR	0.3790	0.2640	0.2240	0.22-0	0.2460	
TYPE	1000	68C+						TVDE	4759							TYPE	6504							2004	1000	4364							3000	***						TYPE	6SC4							TYPE	9204					
HEDIAN CROSSINGS	71	<u>e</u> (22	35	2	23	10	MENTAN COOSSINGS	~) (Ç.	ð.	33	11	52	MFDIAN CROSSINGS	5.8	9.	84	45	12	- F	? 7	MEDIAN COORCINGS	CONTRONAL NATURE	• (2 r) ((0 f		10	MEDITAL COORTINGS	TO CECUSOLING	24 22						CROSS		22 15		23 21			37	CROSSI			15 22			,
EDIANS								TOTANS								HEDIANS								Sint age								ME II A A I C	2 64		0	9-16-	-010-	-90.1	-93.5	EDIANS	-88.1	1.48-	1.68-	29.50	-93.5	1-25-	-93.5	Z	26-	6.06-	61 3	-9r.3	0.10-	
Ŧ	9 49	E . C.	-04-	-A7.6	-84.5	-01.0	4-16-	Ŧ	0.0%-	0	7	-06.3	2.65-	F. HIL	2-00-	HED	-03.5	-92.1	F. + + 1	-94.	200	F-00-	A . 10				8.50				200	100		03.5	40	100	-03.7	-92.3	-00-	MEO		-47.A	S. 26-	T. Ta-	1-96-	1.65-1	1-65-1	1034	1.00-	-05-	-04.0	F. 45-	- 40-	1000
CHS	24	•						CHS	24	ì						CHS	*							1	**	,						SHO		3						CHS	\$2							CHO	24					
HATE	2007	2031						KATE	1200							LATE	2400							SATE	2400	?								15.00						HATE	1290						1	TAL	2400					
TIME	1100			1115	1120	1130	1135	TIME	1155	1200	1000	-621	1210	1215	1226	11ME	1510	1515	1520	1525	1530	1535	1540	THE	1605	2001	1416	1430	1426	1430	1636	TIME	20.46	10.0	1045	1050	1055	1100	1105	1 1 ME	1135	1140	1145	1150	1155	1200	1265	1	1340	1350	1355	1400	1405	201
S	4	5						202	65							2	99							200	7							200	4	3						202	59							Š	2					

REMARKS								REMARKS								HEMARKS							REMARKS						REMARKS							REMARKS				REMARKS					
								IATT																																					
ERROR								ERROR								ERMOR							ERROR						ERROR							ERROR				ERROR					
TYPE	SNON							TYPE	NONE							3461	Zaron.						TYPE	NONE					TYPE	NONE						TYPE	NONE			TYPE	NONE				
FRROP	0.6110	0.5230	0.4840	1.1550	0.3610	0-2470	0.3480	FRROR	0.1440	0.4010	0.1770	0.2590	0.1740	0.1350	0.3500	T KROK	00.000	0.0030	0.0000	0.0000	0.0000	0.00.0	EHROR	0.000E	0.0010	0.00	0.0903	0.0005	EHRON	0.0005	0.0004	0.00.0	9-0110	0.0000	0.00.0	FREOR	0.0010	0.0000	00000	FROR	0.0000	0.0000	0.000.0	0.0000	
TYPE	65C4							TYPE	6SC4							4000	1000						TYPE	4089					TYPE	6SC4						TYPE	6SC4			TYPE	65C4				
SSINGS	23	19	22	54	6	36	27	SSINGS	21	22	54	27	23	23	25	CHATCE	. 5	7.0	1	99	99	85	SSINGS	26	•		2	20	SENISS	7.	Ľ d	C 4	4	6	06	SSINGS	60 0	20	200	CROSSINGS	53	53	20	7	•
MEDIAN CROSSINGS	*	21	77	62	33	32	56	MEDIAN CRUSSINGS	8-5	25	ű.	4 6	25	72	92	TO THE CHOOSENIES	6	2	85	7.8	83	2	MEDIAN CROSSINGS	*	99	. œ	2	**	MEDIAN CROSSINGS	50	x 0	87	2	6	26	MFDIAN CROSSINGS	136	7	66	MEDIAN CRO					
Shi	-94.5	4.46-	-95.4		1-96-	-94°6	-92.7	INS	-93.5	-95.1	7.46-	-95.5	-94.1	7°E6-	4.56-	A BB.	-87.0	2.08-	-88°C	-87.5	0.06-	-89.3	ANS	-84		ROS	-89.0	-89.0	ANS	14.0	107.0	- 100	-87.8	-87.4	1.78-	ANS	2.46.	2.50	4.4	ANS	-71.5	4.69-	-72.0	0.69-	
SHI I JA	-05.5	5.40-	-16.9	0.40-	-46€	1.46-	-63.7	MENTANS	2.46-	-96-1	-45.4	-05.7	-45.n	4.96-	-	-	6.98-	-87.K	1.74-	-47.1	2.151		Ξ	0.7.	7.74	-67.6	1000		Ξ	1. W.	3.13		* HO 3	-87.3	•	=	153.4	E 3	F 2 2 2	7					
CHS	5*							S.F.	2						1	24	,						SE CE	\$					3	2						£ .	•			CHS	7.				
MATE	2400							PATE	1204						47.45	1200							KATE	1600					KATE	1200						X	1 200			MATE	1200				
LIME	1435	1440	1445	1450	1455	1500	1505	TIME	1525	1530	1535	1540	1545	1550	CCCT	1005	1010	1015	1020	1025	1030	1035	1 1 1 E	0001	1166	1115	1120	1125	1146	1150	1200	1205	1210	1215	1220	1 1 1	1 324	1330	1335	TIME	1445	1450	1455	1500	
Z Z	1							35	72						7110	73	?						S. F	t					S. S.	12					3	5	2			Ş	11				

-	11 ME	147	Į,		ENTANS	SENTA CHOSSINGS	SENISSO	TYOF	ERROR	TYPE	ERROR	REMARKS
-	040	1203	50		-60.0		ŧ	4289	0.0000	NONE		
-	345				2.59-		25		0.000			
-	550				-74.6		36		0.000			
-	555				-15.4		æ		0.00.0			
Ä	900				7.01-		25		0.000.0			
-	609				1.17-		X.		0.000			
-	61°				-71-		4		0.0000			
-	1	F. B. Tr.	CHS	10,44	2	MEDIAM CHOSSINGS	SSINGS	TYPF	FRADR	TYPE	ERHOR	RFWARKS
~	1535	1600	2.	-7H.	-75.4	4.9	37	64C4	90000	LNCN		
~	540			5-64-	1. W.1	i,	5		0.00.0			
~	545			×-	-10.4	e u	Š		0.0400			
-	550			- E C -	2.17-	1.7	3		00000			
-	555			7.11.	-79.7		, C		0.000			
~	204			5.13.	-10.7	8	4		21.9860			HUNKS ON
-	TIME	MATE	SIO	1034	2	HFD1AN CA	CHUSSINGS	TYPE	FRADA	TYPE	FRROR	REMARKS
~	1625	1200	*	-19.5	-77.2		4	4286	0.0006	JNON		
_	435			-7.4.7	-14-1	3.			0460-0			
	635			- KM-	-77.	, c	57		0.00			
-	5.0			A CHE	-77.4		5					
_	144	77.74	7	11.4F		SOUL COOSSINGS	SOLINGS	TVDE	20003	TVDE	00000	0 × 0 × 0 × 0
_	147	107	2		0 17	4/	27.00	100	0000	9,40,4	KOKKI	OKKERK
-	750			2 6 4	19	2	- 9	*15:	******	Janne.		
-	1755			3	100	7.	, 64		0.000			
-	008			1	9 9	7.	7 0					
-	10			200	-79-	6	1		0.000			
-	HIS			-47.0	-80.3	7.	-		0.000			
-	TIME	MATE	CHS	I i alu	A	MEDIAN CHRSSINGS	SSINGS	TYPE	FRACA	TYPE	ERROR	RFWARKS
=	435	1600	₹.	2-11-	-78.3	F9	6.3	6504	0.0003	NON		
7	840			-14.2	-79.5	55	53		0.008			
=	145			-77.5	-78.7	4	57		0.00.0			
=	950			-77.6	-79.6	53	47		0.0000			
~	855			-77.1	-78.4	4.9	Œ.		0.0003			
~	006			-74.A	-77.1	3	1.9		0.0000			
-	1905			-17.4	-74.6	95	;		0.0006			
-	<u>ال</u>	MATE	,	396	4	MFIJIAN CONSSINGS	USSINGS	TYPE	ERROS	TYPE	ERROR	REMARKS
-4	647	1200	4	-74°H	-75.6	24	27	7059	0.0003	NONE		
-	745			4.51-	-14.6	94	S.		0.00.0			
-	という			-14.4	-74.j	55	0		25.0430			NO SYNCH
~	955			4-51-	-77-1	46	55		19.6220			
:V	2000			-75.0	-17.5	45	9		0.0030			
N	500			-7.7.e	-78.3	40	4		0.0000			
_	ME	PATE	STO	46.0	EULANS	AFDIAN CROSSINGS	SSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS
~	420				-73.4		17	NONE		NON		
~	425				4.17-		<u>*</u>					
٠,	130				-74.4		11					
-	1435				-71-0		E :					
-					x. c.		21					
-	0 4				7.71		02.					
•							e.					

	DENABRA							DENABRE								REMARKS								REHARKS							PFWARKS							9200000	O YEAR LE						
	FBBOB							FOROS	Canon							ERROR								ERROR							FDROB							9000	NA CHANGE						
	TVPF							TYPE	NON							TYPE	NONE							TYPE	NONE						TYPE	HONE						1005	- NOW	}					
	48808							FREDR								ERROR							Y	FRROR							FRROS							50000							
	TYPE	BNON						TYPE	JNON							TYPE	NONE							TYPE	NONE						TYPE	MONE						TVDE	NONE						
	MEDIAN CROSSINGS	71	12	10	13	13	2 :	MEDIAN CROSSINGS	15 16		11 15	11	9 11		12 12	HENIAN CRUSSINGS	-		T.	_	14 16	14 2)	12 11	CROSSI	_		- 1				CROSS	•	-	P				COUCET							33 24
	ME DI ANS	-75.7	-78.h	-78.5	-75.3	-12.5	176.4	MEDIANS	6.48-	-H3.7	-63.	-81.7	-79.5	-82.2	-85.c	AKS	-83.7	B . E	-87.3	-84.5	-63.1	3.	-82.3	Z	-19-	-79.0		1	C C X	-81.52	Z	-70.9	-61.0	H-6/-	1 - 1 - 1	6 1	182.0	3	1.69-	-90.0	-91.5	1-16-	7.00-	-04°	7
	# C.							NEUT	-84.5	9-1	-14.5	- HC - S	-11-4		-45.4	MEDTANS	¥ 7 7 1	1.7.T	-41.3	-42.1	-45.A	£	- KS. 3		-100	-77-0	1.07	100		-6.1.0	1034	-41.0	- P.C. B	F-61-			0 0 0	TITELL	-48.1	-40.	F. 5. 5.	-40.6	2.65	D. C.	c c r
	CHS							CHS								CHS								5							CHS							CHS							
	HATT							RATE								KALA								A A							AATE							SAFE							
DATA	TIME	1530	1535	15+0	1545	1550	1600	TIME	1420	1425	1430	1435	1440	1445	1450		1530	1535	1540	1545	1550	1555	3001	-		1045	1666	1700	1705	1710	TIME	1750	1755	9047	000	1816	1920	1 I VE	1020	1025	1936	1035	1040	600	> -
20	200	85						2	96							2	68						3	5 6	2						Š	6						25	26						

FOM	DATA										
25	TIME	HATE	CHS	MEDIANS	SNA	AFOLAN CROSSINGS	TYDE	FREDO	TVDE	90809	DELLOKE
F. 6	1350			-	-84.3	22 24			1000		- Current
	1355			6 6 9 1		27	MONE		2020		
				3000		•					
	1001			-42.8	-84.5						
	1405			- B4 . S	-85.6						
	1410			-43.6	-85.0						
	1415			8-24-	-84.7	27 20					
7	1145	DATE	975	- H- F	0.00	7				0.000	
1	1466	2400	5 6	200	:	CKOSSI	344	FKROK		ERMOR	REMARKS
	15.00	1047	ţ		60	_ ,	43S5	0.0110	NONE		
	15.05			200	100			0.000			
	1610			7 P.C.		67		1100.0			
	1515			24.				0520-0			
	1626			0.07				0.0170			
	1526			1	0.10	02		0.0011			
200	1365 TIME	PATE	Y.	1097	C.08-	23000	-	0.000	407.	0000	and the
ő	1650	1260	200	102.1	000	בער בער בער בער	344	S S S S S S S S S S S S S S S S S S S	100	EMMON	MEMBARS
2	1466		,	100			636	0.000	ACME.		
	1400			* 1	0.06	12 62		0.0003			
	1706			6.17	200			0.0330			
	0011			2016				0.00			
	1716			1.26-	1.69-	35		0.0150			
NO.	T I ME	HATE	SEC	4. C.	AFT TANS	22007	1007	0.0970	100	90901	
00	1750	1200	42	405.7	BO. B	42 CF	900		1	ENAUM	REMARKS
	1755			C- [>-	-80.6	95 75	2000				
	1800			E-00-	-80			00000			
	1865			11.7	-89.5			0.0440			
	1810			-42.2	-80.6			0.0040			
	1615			-05.4	-89.7			0.0000			
	1820			-05.6	-90-1	46 41		0.0330			
Ş	TIME	RATE	CHS	MEUI/	Ž	CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
100	1935	1200	\$	-98.3		37 31	95C4	16.0700	NONE		NO SYNCH
	1940			-0B.7				0.3340			
	1945			0.65-		45 44		0.1200			
	1930			£ 66-	-98.1			0.4200			
	1433			2.86-		6E 04		0.2800			
	2000			0.00	7.00	99		0.4200			
S	TIME	MATE	CHS	-ED	4	CROSS	TYPE	FREGO	TVDF	2000	DENABRE
104	1535	1200	54	-63.3		2	6SC4	0-000	MON		
	1540			-91.5		17 16		0.0000			
	1545			-41.1		12 20		0.000			
	1550			E-63-3	9.46-	17 16		0.0000			
	1555			-93.3		_		0.0000			
3	1000	27.40	200	2.78-	3	=		0.000			
	3641		ָרָבָּי בּי	MED!	ANS	CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
	1430	7007	t		0.00	n ı	6204	0000-0	MONE		
	1656			8.00				00000			
	1635			2.26	7.26-	52 52		00000			
	1445			200	5.56-			00000			
	1660			500	300	• •		00000			
	1050			1.10-	0.46-	51 21		00000			
	6661				2.64-	21 21		000000			

1775 1200 24 -99.6 17 1725 1720 24 -99.6 17 1725					
RATE CHS	CROSSINGS		TYPE	ERROR	REMARKS
RATE CHS	2	GSC4 0.0000	NONE		
AATE CHS		00000			
RATE CHS		00000			
RATE CAS — 96.9 -97.7 -96.9 -100.2 -100.3 -100.2 -100.3 -100.2 -90.1 -90.1 -90.1 -90.1 -90.1 -90.1 -90.1 -90.1 -90.2 -90.3 -90.2 -90.3 -	30				
RATE CAS					
RATE CAS MEDIANS 4EDI -99.2					
RATE CHS	CROSSINGS	TYPE ERROR	TYPE	FREDR	REMARKS
RATE CHS			NON		
RATE CHS	15				
RATE CHS	_				
RATE CHS					
RATE CHS96.495.7 -96.1 -94.9 -96.1 -96.1 -96.2 -96.1 -96.2 -96.1 -96.3 -96.2 -96.4 -95.5 -96.4 -96.5 -96.7 -96.2 -96.7 -96.2 -97.8 -96.2 -97.8 -97.8 -97.8 -					
RATE CHS	_				
RATE CHS	21 19				
AATE CHS	CROSSINGS	PE ERROR	TYPE	FRROR	REMARKS
RATE CHS MEDIANS MEDIA		NONE	NON		
AATE CHS	72	!			
RATE CHS					
RATE CHS					
RATE CHS -96.1 -95.5 -94.2 HEDI -99.3 -94.2 -96.7 -97.0 -96.7 -97.3 -96.7 -97.3 -96.7 -97.3 -96.4 -97.3 -97.	51 33				
RATE CHS					
RATE CHS MEDIANS MEDIANS 197.0 196.2 197.2 198.4 197.2 196.7 197.3 196.7 197.3 197.3 197.4 197.3 197.4 197.1 180.24 193.5 120. 24 197.5 196.7 120. 24 197.5 196.7 120. 24 197.5 196.7 120. 24 197.5 196.7 120. 24 197.5 197.7 187.6 187.8 187.8 187.6 187.8 187.9 187.6 187.9 187.6 187.9 187.6 187.9 187.6 187.9 187.6 187.9 187.6 187.9 187.6 187.9 187.6 187.9 187.9 187.9 187.9 187.9 187.9 187.9 187.9 187.9 187.9 187.9					
AATE CHS -97.0 -96.2 -96.7 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -97.5 -98.2 -97.3 -97.5 -97.5 -97.5 -97.5 -97.5 -97.5 -97.5 -97.7 -97.5 -97.5 -97.7 -97.7 -97.5 -97.7 -97.7 -97.5 -97.7 -97	CROSSINGS	TYPE ERROR	TYPE	ERROR	REMARKS
HATE CHS -99.3 -98.4 -97.2 -96.7 -97.3 -96.7 -97.3 -96.7 -97.8 -97.3 -97.3 -96.7 -97.8 -97.3 -97.8 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -97.3 -98.2 -98.2 -98.4 -98.4 -103.5 -102.8 -103.5 -103.	ŧ	NONE	NON		
AATE CHS #EDIANS #EDI PATE CHS #EDIANS #ED					
RATE CHS MEDIANS MEDIA					
RATE CHS #601ANS #601 -97.8 -97.3 -96.4 -97.8 -97.1 -97.1 -99.4 -97.1 -99.4 -97.1 -97.3 -97.1					
RATE CHS					
AATE CHS					
AATE CHS MEDIANS MEDI -97.8 -97.1 -99.3 -98.9 -98.2 -97.3 -98.2 -96.2 -99.4 -98.4 -103.0 -102.8 -103.0 -102.8 -103.5 -96.7 -103.0 -96	45 44				
-97.8 -97.1 -99.3 -99.9 -99.3 -98.2 -98.2 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.6 -99.7 -99.6 -99.7 -99.6 -99.6 -99.7 -99.6 -99.7 -99.6 -99.7 -99.6 -99.7 -99.6 -99.7	CROSSINGS	TYPE ERROR	TYPE	FRROR	REMARKS
RATE CMS -99.3 -98.9 -99.9 -99.9 -99.9 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.4 -99.6 -103.5 HEDI 200 24 -87.5 -87.9 -87.9 -87.9 -87.9 -87.9 -87.9 -87.9 -87.9 -87.9 -87.9	0+	NONE	NONE		
100.24 -07.3 -08.2 -07.3 -09.4 -103.6 -103.0 -102.8 -103.6 -103.5 -103.5					
-98.8 -99.4 -103.6 -103.8 -103	37 38				
-99.4 -102.8 -102.8 -103.5 -102.8 -103.5 -10					
-103.0 -102.8 -103.5 -1					
RATE CHS					
1200 24 -87.5 -86.7 4E01 1200 24 -87.5 -87.3 -87.3 -87.5 -87.7 -87.6 -87.7 -87.6 -81.2 -81.2 -81.2 -81.2 -81.2 -81.2 -81.2 -81.2 -81.2	37 31				
1200 24	CROSSINGS	PE ERROR	TYPE	ERROR	REMARKS
197.5 - 697.3 197.5 - 1697.7 193.1 - 1697.6 191.1 - 1691.2		GSC4 0.0000	NONE		
197.6 -07.7 -193.1 -087.4 -191.1 -091.2 -195.6 -064.4	23				
- # 1 - # 1					
-#1.1 -#1.2 -#5.6 -#4.4					
1910 1910 1 1910 1 1910 1 1910 1					
4	• 0	00000			
	**************************************	•			
	30	000000			

12 12 12 12 13 14 15 15 15 15 15 15 15		4				SETTIES	TYPE	-	TVDF	FOROR	
		SES	MEDI	SZZ	MEDIAN CRO			T K K O I			MEMAKES
HATE CHS HEDIAS CHOS SING TYPE ERROR TYPE ERROR TYPE CHS		2	5.06-	-92.1	22	19	6SC4	0.0003	SNON		
HATE CHS			-H7.6	-90.5	2	23		0.0044			
HATE CHS	in		-89.2	-90.1	54	18		0.0003			
HATE CHS	0 1		- K - K	-88.5	23	25		0.0003			
HATE CHS	n «		- X		2 :	- (800000			
HATE CHS HELIANS HEDIAN CAOSSIMS TYPE ERROR TYPE FROM THE ERROR HATE CHS HELIANS HEDIANS HEDIANS TYPE FROM TYPE FROM THE ERROR HATE CHS HELIANS HEDIANS HEDIAN	P 14		4.45		•	9		0.0436			
1200				- 3	34	1		0.0350			
HATE CHS WITH STATE C		6	5	2	SHEDIAN CHO	CONTES	1	EMROR	JAA.	ERMOR	REMARKS
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE FRROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE		*	0 · 1 ×	1.48-	77	£ ;	6264	000000	NO.		
HATE CHS WEDLANS HEDLAN CROSSINS TYPE FROM NONE EAROR 120 24 -91.5	S.		4.64-	-85.0	13	16		0.000			
HATE CHS TYPE TO 13 00000 HATE CHS TYPE CHS TYPE TRROW TYPE ERROR TYPE TO 13 17 14 14 14 14 14 14 14 14 14 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	9		-A1.6	-84.3	17	13		0.000.0			
HATE CHS	ī.		-77.6	-78.9	10			0.0178			
HATE CHS -76.2 -77.5 13 17 0.0133 HATE CHS -76.7 -80.2 13 17 0.0133 HATE CHS -76.7 -80.2 13 17 0.0133 HEDIANS -90.4 20.2 29 17.5 18 17 0.0100 HATE CHS -90.4 -90.3 3 18 32 18 18 17 0.0100 HATE CHS -90.4 -80.2 18 18 17 0.0100 HATE CHS -90.5 -90.2 18 18 17 0.0100 HATE CHS -90.5 -90.2 18 18 17 0.0100 HATE CHS -90.6 -90.7 -90.0 18 18 18 18 18 0.0100 HATE CHS -90.5 -90.2 18 18 18 18 0.0100 HATE CHS -90.5 -90.2 18 18 18 18 0.0100 HATE CHS -90.5 -90.5 18 18 0.0100 HATE CHS -90.5 -90.5 18 18 0.0100 HATE CHS -90.5 18 18 18 0.0100 HATE CHS -90.5 18 18 18 0.0100 HATE CHS -90.5 18 18 0.0100 HATE CHS -90.5 18 18 18 0.0100	3		2.87-	-10.4	17			0.0000			
HATE CHS HOTANS HOTANS 11 0,0003 TYPE FRROR TYPE FRROR 12 0,0003 TYPE FRROR 12 0,0003 TYPE FRROR 12 0,0003 TYPE FRROR 12 0,0000 TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	S		-76.2	-77.5	13	17		0.0133			
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE FRROM TYPE FROM T			-74.5	-80.2	2			0.00.0			
RATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -01.5 -99.2 13 12 14 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 12 0.0000 NONE ERROR 1200 24 -01.5 -99.2 13 14 0.0000 NONE ERROR 1200 24 -01.5 -99.2 17 7 20 0.0000 NONE ERROR 1200 24 -99.2 17 7 20 0.0000 NONE ERROR 1200 24 -99.2 17 7 20 0.0000 NONE ERROR 1200 24 -99.3 17 20 0.0000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 24 -99.3 16 16 16 0.00000 NONE ERROR 1200 25 -99.3 16 16 16 0.00000 NONE ERROR 1200 25 -99.3 17 20 0.00000 N		CHS	2	Z	3	SSINGS	TYPE	FRROR	TYPE	FRROR	RFMARKS
RATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR					_	22	NONE		MONE		
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RATE CHS 120 2 -97.0 26 22 22 22 17PE FRROM TYPE 120 2 -97.0 26 22 22 22 22 22 22 22 22 22 22 22 22	9		C X6-	-00-	¥	; e					
RATE CHS HEDIANS HEDIAN CROSSINGS TYPE FRROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	- N		-05.0	-07.0	90	0					
RATE CMS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 120 24 -91.4 -89.0 11 17 65C4 0.0000 NONE CAPE CAPE CAPE CAPE CAPE CAPE CAPE CAP			-92.8	-93.9	23	25					
120		CHS	MEDI	~	MENIAN CRO	SSINGS	TYPE	FRROR	TYPE	FRROR	REMARKS
HATE CHS — 49.0 — 67.7 13 21 0.00000 0.000000 0.000000 0.00000 0.00000 0.00000 0.00000 0.000000 0.000000 0		54	-0].		18	17	85C4	0.000	NON		
HATE CHS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -91.1 17 0.0001 19001 10001 1900			0.58-	-67.7	13	2		0.000			
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -91.5 -90.0 11 17 10 0.0014 15 12 0.0000 15 1200 24 -91.5 -90.2 10 13 14 65C4 0.0005 17 15 15 15 15 15 0.0055 17 15 15 15 15 15 15 15 15 15 15 15 15 15	•		-41.0	-89.2	81	<u>*</u>		0.000			
HATE CMS — 66.9 13 12 0.0000 -97.8 — 68.9 13 12 0.0001 120. 24 — 91.5 — 99.3 13 14 GSC4 0.0005 -93.2 — 91.3 17 20 0.0055 -94.9 — 92.5 17 20 0.0055 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 92.5 17 20 0.0056 -94.9 — 94.5 12 14 GSC4 0.0147 -93.4 — 93.5 12 15 0.0039 -93.4 — 93.5 12 15 0.0039 -93.8 — 93.5 16 16 0.0047			-016-	4.19-	2	11		0.030			
HATE CHS — 66.9 13 12 0.0000 RATE CHS — 68.9 15 12 0.0003 120. 24 -91.5 -90.2 13 14 05C4 0.0005 -93.2 -91.1 17 15 0.0050 -94.9 -92.3 17 20 0.0050 -94.9 -92.5 17 20 0.0050 -94.9 -92.5 17 20 0.0050 -94.9 -92.5 17 20 0.0050 -94.9 -94.5 12 15 0.0044 -93.4 -90.5 12 15 0.0039 -93.4 -90.5 16 16 0.0007			1.26-	90.0	: =	17		0.0014			
HATE CHS			- AB. A	-KA. C							
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE ERROR 1200 2491.5 -91.2 13 14 GSC4 0.0000 NONE -93.2 -91.3 13 13 13 0.0050 1.0			H-00-	T . C.		2 0					
1200 24 -91.5 -90.2 13 14 05C4 0.0000 NONE 1200 24 -91.1 10 13 14 05C4 0.0005	E T	CHS	MED!	ANS	Z	SSINGS	TYPE	FRROR	TYPE	FOROR	RFMARKS
-03.2 -91.1 10 13 0.0005 -04.1 -92.5 17 20 0.0050 -04.1 -92.5 17 15 0.0050 -04.1 -92.5 17 15 0.0050 -04.4 -96.0 13 13 0.0050 -04.5 -93.3 12 14 GSC4 0.0144 NONE 1200 24 -04.5 12 14 GSC4 0.0147 -93.4 -90.7 13 10 0.0103 -93.4 -90.7 10 16 0.0007	120	24	5-10-	-90.2	~	*	4080	00000	ANON		
-03.9 -92.3 17 20 0.0050 -04.1 -92.5 17 15 0.0050 -04.1 -92.5 17 15 0.0050 -04.1 -92.5 17 15 0.0050 -04.5 -96.0 13 13 0.0050 -05.0 24 -06.0 12 14 65C4 0.0144 NONE -03.3 -89.4 13 10 0.0103 -03.4 -90.7 13 10 0.0103 -01.2 -90.9 16 16 16 0.0007			-03.2	-91.1	10	13		0.0005	To the second se		
	•		-63.0	-92.3	17	20		050000			
	2		-04.1	-92.5	17	15		0.0025			
-44.9 -96.4 -22 19 0.0694 -43.3 12 15 0.1649 TYPE ERROR 1200 24 -43.3 MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -56.8 -96.4 13 10 0.014 NONE -93.4 -90.7 13 10 0.0103 -90.01 12 15 0.0039 -91.2 15 0.0007 -91.2 15 0.0007	ç		F. 65.	-96.0	13	13		0.00.0			
HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -94.5 HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -94.5 HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -95.4 -96.7 H3 10 0.0103 1.93.4 -93.5 H2 H5 10 0.0047 1.93.5 H5 10 0.0047 1.93.5 H5 10 0.0047	ŵ		0.25-	-96°	25	19		0.0694			
MATE CHS MEUJANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1200 24 -96.8 -94.5 12 14 GSC4 0.0144 NONE 1200 24 -93.3 -89.4 13 10 0.0103 1-93.4 -90.7 13 10 0.0103 1-93.4 -93.5 12 15 0.0039 1-91.2 -90.9 16 16 0.0047			\$	-43.3	12	15		0.1649			
1200 24	7	CHS	MEUI	3	MEDIAN CAN	SENISS	TYPE	FRROR	TYPE	ERROR	REMARKS
-93.3 -89.4 13 9 0.0147 -93.4 -90.7 13 10 0.0103 -93.8 -93.5 12 15 0.0039 -91.2 -90.9 16 16 0.0067		24	-66.8	-94.5	12	* 1	6504	0.0144	NONE		
-93.4 -90.7 13 10 -93.8 -93.5 12 15 -91.2 -90.4 16 16 -99.6 -98.7 10 16			-03.3	1.08-	13	•		0.0147			
-43.4 -93.5 12 15 -41.2 -90.9 16 16 -89.6 -88.7 10 16			-03-	1.00-	-	9		60.0			
-41.2 -90.9 16 16 16 16 16 16 16 16 16 16 16 16 16) C		-03. B	4.60-	2.5) <u>v</u>					
01 01 L-988 9-64-	y v		6.10	2 0 0	7.	2		0.003			
0 0 0 0 0 0 0 0 0			3.14		2						
	2 4		0000		2 :	9		00000			

CHS - 10.0	Trees. Sector						1				
CHS -100.6 -100.9 52 27 05.200 NOWE	4	CHS			MEDIAN CH	10551R65	TYPE	ERROR	TYPE	ERROR	REMARKS
CHS WELLANS	2	24	-100.6	-100.0	35	27	4086	0.3200	NONE		
CHS - 100.6			0.60-	-101-	66	25		0.5000			
CHS99-4 197 124 0.351099-4 197 124 0.351099-4 197 124 0.351099-4 197 124 0.351099-4 197 124 0.351099-799-2 197 124 0.351099-799-2 197 197 197 197 197 197 197 197 197 197			7. HO-	-1001-	19	47		0.4840			
CHS -110.26 -10.06.4 -99.2			-08.0	-99.5	137	124		0.3510			
CHS - 10.0.2 -99.4 HG 61 0.4100 TYPE ERROR OF 10.4100 TYPE CHS - 10.4100 TYPE FRROR OF 10.4100 TYPE TYPE TYPE FRROR OF 10.4100 TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE			8. HO-	-44.2	100	117		9000			
CHS -110.6.5 -10.6.5			-100.2	£.66-	36	61		0.3220			
CHS #EDIANS #FDIAN CAOSSINGS TYPE FRROR TYPE FRROR CHS #EDIAN CAOSSINGS TYPE FRROR TYPE FRROR TYPE FRROR CHS #EDIAN CAOSSINGS TYPE FRROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE			-100.6		36			0.4100			
CHS	TE	CHS	MEDI	SAVE	MEDIAL CA	SSAISSO	TYPE	FRACE	TYPE	ERROP	REMARKS
			6.96-	-95.2	37	30	NONE		MONE		
CHS			4-90-	4-60-	96	8					
CHS			7.96-	6.70	4	ď					
CHS #ENTANS #EDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE CHS #ENTANS #EDIAN CROSSINGS TYPE ERROR TYPE ERROR #ENTANS #EDIAN CROSSINGS TYPE ERROR TYPE ERROR #ENTANS #EDIAN CROSSINGS TYPE #ENTANS #EDIAN CROSSINGS #EDIAN CROSSINGS #EDIAN CROSSINGS #EDIAN CROSSINGS #EDI			4.00	5.00	3 2	2 6					
CHS -01-5 -0				400	7 6						
CHS #EPITANS #EDITAN CROSSINGS TYPE ERROR TYPE ERROR CHS #EDITAN CHS #			0.17	-06-	£ .	02					
CHS -48.5			**Zb-	-61.5	35	:					
CHS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 10.050 NOWE CAS. 10.052			-08°5	-96.3	38	24					
2+ -00.6 +90.0 30 35 65C+ 0.0550 NONE -02.4 -02.2 37 50 0.0135 -02.4 -02.2 37 44 0.0115 -02.4 -02.2 37 44 0.0115 -02.4 -02.2 37 44 0.0115 -03.0 -04.5 -06.4 32 25 0.0022 -04.5 -06.4 46 24 0.030 -04.5 -06.4 -06.6 30 0.0120 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -04.5 -09.1 -09.2 70 6 0.030 -07.5 -09.1 -09.2 70 6 0.030 -07.5 -09.2 70 6 0.030 -07.5 -09.1 -09.2 70 6 0.030 -07.5 -09.2 70 6 0.030 -07.5 -09.2 70 6 70 -07.5 -09.2 70 6 70 -07.5 -09.2 70 6 70 -07.5 -09.2 70 -07.	ATE:	CHS	HED 1	LANS	MEDIAN CR	SUISSU	TYPE	ERROR	TYPE	ERROR	REMARKS
CHS WED1ANS	÷00	2*	9.00-	-90.0	30	35	6504	0.0500	NON		
CHS WELLANS			-46.6	-87.1	37	20		0.60.0	•		
CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR CHS HEDIAN CROSSINGS TYPE ERROR T			-92.4	-92.2	7.	1		0.0176			
CHS HEUTANS HEDTAN CROSSINGS TYPE ERROR TYPE			-92-8	-89-	4	36		0.0015			
CHS WELLANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE ERROR TYPE ERROR TYPE ERROR TYPE ERROR CHS WELLANS MEDIAN CROSSINGS TYPE ERROR TYPE TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE			-47.5	-85°E	30	2		05500			
CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR CHS			-46-2	186.1	200	, K					
CHS MEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR CAS			3	-80.6	4	2 4		7.00.0			
24 -88.4 -88.6 34 36 65C4 0.0300 NONE -91.3 -91.2 40 43 65C4 0.0120 -93.8 -92.6 39 49 0.1050 -94.5 -93.1 51 41 0.1440 -91.2 -92.2 73 63 0.0740 -92.2 -95.2 71 56 0.0990 -92.2 -95.2 64 0.1760 NONE -97.2 -95.3 64 0.1920 -97.2 -95.3 64 0.0950 -97.2 -95.3 64 0.1920 -97.2 -95.3 64 0.0950 -97.2 -95.3 64 0.0950 -97.2 -95.3 64 0.0950 -97.2 -95.3 64 0.0950 -97.2 -95.3 64 0.0950 -97.2 -95.3 71 56 67 0.0950 -97.2 -95.3 64 0.0950 -97.2 -95.3 77 77 77 77 77 77 77 77 77 77 77 77 77	416	CHS	MEDI	3	AFDIAN CO	POSSINGS	TYDE		TVDE	90906	9704270
CHS # -97.6	2409	24	-88-4	1	2.8	36	4788	0.0300	MONE	-	-
CHS			-91.3	-91.2	•	5		0.010.0			
CHS			-0.1.B	9000	2	9		0.100			
CHS			-04	102	ì	•		001.0			
CHS				100	5	7		6+1-0			
CHS #F01ANS #F01AN CROSSINGS TYPE ERROR TYPE ERROR CHS #F01AN CROSSINGS TYPE ERROR TYPE TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE			6-17-	0.00	20	C :		0.00.0			
CHS HF01AN CROSSINGS TYPE ERROR 24 -36.2 -95.2 71 56 65 0.1470 NONE 24 -36.2 -95.2 64 0.1470 NONE -97.2 -94.9 55 64 0.1470 -97.2 -94.9 55 64 0.1470 -97.2 -94.9 55 64 0.1470 -97.2 -95.9 80 56 0.0890 -97.2 -95.9 80 56 0.0890 -97.2 -95.9 80 56 0.0890 -97.2 -97.9 44 43 NONE -80.4 42 42 NONE -80.2 -77.4 59 25 -97.5 -77.4 59 25 -97.5 -77.4 59 25 -97.5 -77.4 59 25 -97.5 -77.5 44 40 -97.5 -77.6 75 75 75 75 75 75 75 75 75 75 75 75 75			6.50	2.26-	73	63		0.0740			
CHS MFDIANS 4EDIAN CROSSINGS TYPE ERROR TYPE ERROR 24 -36.2 -95.2 71 58 657 0.1760 NONE -97.2 -94.9 55 64 0.1920 -95.9 -93.2 80 56 0.0360 -95.9 -93.2 80 56 0.0360 -95.4 -91.1 57 44 42 0.015 -19.5 -17.4 29 25 -19.5 -17.5 20 25 -19.5 2	ì		5.45		0,	25		0.0990			
24 -36.2 -95.2 71 58 65C4 0.1760 NONE -90.7 -95.8 56 64 0.1470 -97.9 55 64 0.1470 -97.9 55 64 0.1470 -97.9 55 64 0.1470 -97.9 55 64 0.1470 -97.9 -91.1 57 44 62 0.0360 -90.4 50 57 44 42 NONE -78.6 -81.7 44 42 NONE -78.6 -81.7 44 42 NONE -79.5 -77.4 52 25 -77.4 52 25 -77.4 52 25 -77.4 52 25 -77.4 52 57 40	AIE	CHS	I WE II	Z	AEDIAN CA	POSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
-46.7 -95.8 66 67 0.1470 -97.2 -94.9 55 64 0.1920 -92.4 -91.1 57 44 0.0450 -92.4 -91.1 57 44 0.0450 -90.6 -89.1 34 37 0.0360 -90.6 -89.1 45 32 0.0175 -90.6 -89.1 44 42 NONE ERROR -78.2 -77.2 44 42 NONE ERROR -78.5 -77.9 41 54 42 -77.9 41 54 -77.9	004	*2	2-96-	-95.5	=	200	6SC4	0.1760	NON I		
-97.2 -94.9 55 64 0.1920 -95.9 -93.2 80 56 0.0830 -92.4 -91.1 57 44 0.0850 -90.6 -89.1 37 0.0850 -90.6 -89.1 45 32 0.0175 -90.6 -89.1 44 42 NONE ERROR -78.2 -77.2 44 42 NONE ERROR -78.5 -77.4 29 25 -81.5 -77.4 29 25 -81.5 -77.4 70 40 -47.1 -86.2 75 57				-95.3	99	67		0.1470			
CHS HENIANS HOUSE ERROR TYPE ERROR NONE HOUSE HO			2.16-	5.46-	55	• •		0.1920			
-92.4 -91.1 57 44 0.0450 -86.5 -95.9 34 37 0.0360 -90.6 -89.1 45 0.0175 -78.2 -77.2 44 42 NONE ERROR TYPE ERROR -78.6 -81.7 44 42 NONE -79.5 -77.9 41 54 42 -79.5 -77.4 29 25 -77.4 29 25 -77.4 20 34 40 -47.1 -86.2 75 57 57 57 57 57 57 57 57 57 57 57 57			6.56-	-93.2	08	26		0.0890			
-86.5 -85.9 38 37 0.0360 -90.6 -89.1 45 32 0.0175 -90.6 -89.1 45 32 0.0175 -78.2 -77.2 44 42 NONE ERROR NONE -81.7 44 42 NONE -80.5 -77.9 41 54 -80.5 -83.9 70 40 -47.1 -86.2 75 57			-45.4	-91.1	57	;		0.0450			
CMS HENIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR -74.2 -77.2 44 43 NONE NONE -82.6 -81.7 44 42 -79.5 -77.9 41 54 -80.2 -77.4 29 25 -81.5 -83.9 70 40 -47.1 -86.2 75 57			-88.5	-85.9	38	37		0.0360			
CMS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR -78.2 -77.2 44 42 NONE -42.6 -81.7 44 42 -79.5 -77.9 41 5H -79.5 -77.4 29 25 -81.5 -77.4 40 -47.1 -86.2 75 57			9.00-	-89.1	45	32		0.0175			
-78.2 -77.2 44 43 NONE NONE -18.6 -81.7 44 42 NONE -17.9 41 St17.4 29 25 -17.4 29 40 -145.9 34 40 -147.1 -86.2 75 57	ıTċ	CHS	HEDI	ANS	Z	SSINGS	TYPE	ERROR	TYPE	FPROR	REMARKS
-81°-7 -77°-9 -77°-9 -77°-9 -15°-9 -18°-9 -1			-78.2	-77	4	6.3	NON		NONE		
			7.00	7 10	**		1		34.04		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			9.75	- 10		Y					
177.4 185.0 183.9 105.2			-19.5	-77.9	₹	Į.					
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			-80.2	-77.	5	\$2					
-83.9 70			- P] . S	-#5.0	3 ¢	9					
-86.2 75			-95.5	-83.9	20	04					
			-47.1	-86.2	75	57					

TIME HATE	CHS	MEDIANS	SNY	MEDIAN CROSSINGS	SINGS	TYPE	ERROR	TYPE	EAROR	REMARKS
		-R4.4	-86.4	5.0	45	NONE		NONE		
1455		-A7.H	-89.1	53.	34					
0		-A7.0	-87.B	5.5	54					
1505		7. VH-	-84.5	36	39					
S		-H4.6	-85.1	*	51					
S		-86.0	-68.0	33	2					
0.		-85.9	-86.4	35	1.4					
E MATE	CHS	MEDI	ANS	MEDIAN CROSSINGS	SINGS	TYPE	FRROW	TYPE	ERROR	RFMARKS
•		-A7.1	-87.4	53	54	MON		PNON		
Š		-84.S	-89.4	65	89					
0		-92.1	-93.2	63	48					
Ť.		0.45-	-94.5	76	29					
e		-63-1	-94.4	95	78					
Ñ		9.40-	-96-3	96	6.6					
0		-05.6	4.40-	9	12					
NE NATE	CHS	T (1) IN	Z	JEDIAN CROSSINGS	STAGS	TYPE	60000	TVDE	90905	DELLOKS
		5.40-	-96-3	95	77	NO.		NON		
30		9-65-	-94.5	69	89					
1635		-63.1	-94-1	£ 2	11					
1640		0.46-	B. 46-	6	89					
5		-45.4	-96-	106	76					
90		-04.2	6-76-	A.						
		-64.5	-95.7	101	2					
	CHS	MEDI	ANS	HEDIAN CROSSINGS	SINGS	TYPE	FREDE	TYPE	FOROP	PFUARKS
15 1200	54	-R4.9	-84.3	16	78	6504	41000	LNON		
		-87.6	-86.5	104	100		0.0159			
ũ		-86.5	-85.0		78		0.5320			
9		-86.0	-83.9	7.3	7.		0.0040			
10		-46.2	-85.	6	82		9010			
		49.6	92.0	- 1 -	. 6					
- in		-H5.2	184.0	5			9000			
	CHS	MEUI	ANS	MEDIAN CROS	CROSSINGS	TYDE	FRECE	TYPE	FDROD	PEMARKS
1035 1200	2	-H3.2	-81.8	72	72	6504	0.0370	NON		
•		-46.1	-78.6	9	84		90000			
ŭ		-82.7	-81.9	69	64		0.0450			
0		-82.4	-80.5	53	+ 1		0.0019			
ĵ.		-HO.2	-79.6	56	56		0.0031			
0		-82.4	-89.2	6	55		0.0220			
		-82.1	-80°5	55	50		9500.0			
IE MATE	CHS	HEO I	4	MEDIAN CHOSSINGS	SINGS	TYPE	FROS	TYPE	FRROR	AFMARKS
	2	-79.6	-77.5	45	28	4258	D.000.	JNON		
3		-76.5	-75.0	0	-		6.0033			
1140		4.67-	-78.6	; ;			0.016			
4		4.77-	-76.4				7060			
		276.0	78.0	7 6						
2 1			100	Ç. ,	20		1110-0			
6611				C 1	\$:		0.0450			
		C - 1 E -	+ - 5/1	•	24		00400			

THE RATE CAS TAPE										
HATE CHS 174.7 17.0 17.0 NOWE FIRSON TYPE FROM THE THE FROM THE THE FROM TH		CTS	MEDI	ANS	MEDIAN CROSSINGS	TYPE	FRROR	TYPE	ERROR	REHARKS
NATE CHS 170 150 170 150 170 150 170	55		1.77-	-77.0	64 25	NONE		NONE		
HATE CHS -170-6 HOLD A HOLD A GOOD A HOLD A HOLD A GOOD A HOLD A GOOD A HOLD A HOLD A GOOD A HOLD A GOOD A HOLD A GOOD A HOLD A	00		8.0%-	-78.7	77 65					
NATE CHS NEDIANS			-79.6	-74.5						
HATE CHS THE THE TOTAL T		CHS	MEDI	Z	MEDIAN CROSSINGS	TYPE	FRROR	TYPE	ERROR	REHARKS
HATE CHS -79-6 95 52 HATE CHS -77-1 - 80-0 70 66 HATE CHS -77-2 - 80-0 70 66 HATE CHS -77-2 - 80-0 70 66 HATE CHS -77-2 - 80-0 70 60 HATE CHS -77-2 - 70-0 70 HATE CHS -77-2 - 7	145		-17.4	-80.2		NONE		NONE		
HATE CHS THE TABLE TO 66 66 1791 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	150		-76.B	-79.6						
Table Tabl	155		-14.1	-81.X						
HATE CHS FIGURES 1913 60 60 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	200		-77.5	-80°0						
HATE CHS TYPE ENROR TYPE ERROR -77-9 -61-1 73 62 -77-9 -61-1 73 72 HONE CHS TYPE ERROR TYPE ERROR -77-9 -77-1 73 72 -77-1 -77-1 73 74 -77-1 -77-1 74 -77-1 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-1 75 -77-	505		-79.1	-61.3						
HATE CHS -78.9 FOLIANS	110		-H1.2	-64.1						
HATE CHS MEDIANS HETLIAN CROSSINIS TYPE EMPON TYPE ERROR -7.4 - 0.0.1 F. 2.7 1.0 1.			-7H.9	-81.0						
### ### ##############################		CHS	1034	ANS	MEDIAN CROSSINGS	TYPE	EHROW	TYPE	ERROR	REMARKS
RAIL CHS	555		-11.9	-81.1		NONE		NONE		
HATE CHS 179-0 -872-3 70 59 HATE CHS 177-4 -872-3 70 59 HATE CHS 177-5 -76-3 69 63	200		14.1	-80°C						
HATE CHS "FEDTANS" 49 55 HATE CHS "FEDTANS" 49 55 HATE CHS "FEDTANS" 49 55 "The Transmission of the Tra	505		-14°0	-R2.3						
## FILE CHS	910		4.57-	- R.S.						
HATE CHS -75.6 -75.7 -75.1 69 63 HATE CHS -75.6 -75.4 60 63 -75.6 -75.7 -75.7 50 53 HATE CAS -75.7 -75.7 75.7 50 53 HATE CAS -75.7 -75.7 75.7 75.7 75.7 75.7 75.7 75	515		-75.1	-78.7						
HATE CHS -75.5 -79.1 52 53 TYPE ERROR TYPE ERROR -75.6 -75.6 -76.3 67 67 67 67 67 67 67 67 67 67 67 67 67	520		17 x . x	-81.5						
RATE CHS VEDTANS 4ENTAN CROSSINGS TYPE ERROR TYPE ERROR -75.0 -77.1 61 64 NONE NONE NONE ERROR -75.0 -77.1 61 53 -75.0 -77.1 61 54 -75.0 -77.1 61 54 -75.0 -77.1 61 64 -75.0 -77.1 61 64 -75.0 -77.1 61 11 15 FRED 0.0034 -75.0 -77.1 61 11 15 FRED 0.0034 -75.0 -77.1 61 11 15 FRED 0.0034 -75.0 -77.1 61 12 16 0.0034 -75.0 -77.1 61 12 16 0.0037 -75.0 -77.1 61 15 19 FRED 0.0037 -75.0 -77.1 61 17 19 0.0037 -75.0 -75.1 70 70 70 70 70 70 70 70 70 70 70 70 70			-75.5	-78.1	52 53					
PATE CHS FIRST FROM	147	CHS	103%	ANS	JENIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
### Fig. 1. The state of the st	240		-75.€	-7A.4		MON		NON		
HATE CAS HELDLAN TO STATE TO STATE TO STATE CAS HELDLAN TO STATE CAS HE STATE CAS HELDLAN TO STATE CAS HELDLAN TO STATE CAS HELDLAN TO	545		-73.4	-76.3						
######################################	950		-75.0	-77.						
## FE CAS	555		-76.5	-78.2						
## FOR TABLE CAS	00		-16.7	-14.1						
## FULL CAS			-76.0	-78.X						
## E C45		,	-75.3	-78.1	60		10 may 17 may 18			
### 24 - 24 - 2 - 49.2		245	1014	NAS.	HEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
## 12 9 0.0034 ## 12 9 0.0034 ## 12 9 0.0037 ## 13 9 10 0.0037 ## 14 7 9 10 0.0037 ## 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2	2.44-	-45.	_	FRED	0.000.0	NONE		
HATE CHS HELIANS HELIAN CHOSSINGS TYPE ERROR TYPE ERROR TYPE CHS HELIANS HELIAN CHOSSINGS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	90		4.18-	E . C. 20			0.0034			
HATE CHS HELD 9 12 0.0017 HATE CHS HELD 19 12 0.00034 HATE CHS HELD 19 0.00037 HATE CHS HELD 19 0.00037 HATE CHS HELD 17 19 0.00037 HATE CHS HELD 19 0.0004 HATE CHS HELD 19 0.0007 HATE CHS	35		-45.5	- W.			0.0002			
Heate CHS Heat Heat Heat Heat Heat Heat Heat Heat	0		2 - 2 -	-63°C	_		0.0017			
HATE CHS HELIANS HELIAN CHOSSINGS TYPE ERROR FALL HELIANS HELIAN CHOSSINGS TYPE ERROR FALL HELIANS HELIAN CHOSSINGS TYPE ERROR HELIA -78-1 15 19 FHED 0.0059 HATE CHS HELIAN CHOSSINGS TYPE ERROR FALL HELIANS HELIAN CHOSSINGS TYPE FAROR FALL HELIANS HELIAN	45		-H4.7	185.0	_		0.0024			
HATE CHS HELIANS WENTAN CHOSSINGS TYPE ERROR TYPE ERROR HELIANS WENTAN CHOSSINGS TYPE ERROR TYPE ERROR HELIANS HELIAN CHOSSINGS TYPE ERROR TYPE ERROR HATE CHS HELIAN CHOSSINGS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	0 1		F. 04-	-62	⊶ .		0.0038			
### 15 19 FHED 0.0059	44	SHO	10.00 P	A 20 A	AN CORESTAIR	902	0.0304	200		970
HATE CHS HEDIANS TYPE EAROR TYPE EAROR 17.0 C		2	40-	1 44	15 CAN 30 10		CARD C	1	CHAUM	MEMBERS
HATE CHS HEDIAL -79.4 14 15 0.0051 -A1.4 -79.4 14 11 0.0052 -A1.4 -79.4 14 11 0.0053 AATE CHS HEDIAL CHOSSINAS TYPE ERROR 240. 24 -50.0 -79.4 32 29 0.0050 -75.4 -75.4 56 49 0.0050 -75.2 -75.5 9 12 0.0503 -75.3 -75.5 9 12 0.0503	,		- HA-	7.44	71	1	00000	2020		
HATE CHS HEDIAL -70.4 -41.4 -7	0		1.54		27		0000			
HATE CHS HEDIAL CROSSINGS TYPE ERROR TYPE ERROR TYPE CASON TYPE TRACE NONE TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYP	***			- 10-	***		1000			
HATE CHS HEDIAL CHOSSINGS TYPE ERROR TYPE ERROR 17 PPE ERROR 11 11 65C4 0.0220 NONE 17.5.0 17.5.0 10 8 0.0420 0.0420 1.75.0 10 8 0.0420 1.75.0 10 8 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 0.0420 1.75.0 11 11 11 0.0420 1.75.0 11 11 11 0.0420 1.75.0 11 11 11 0.0420 1.75.0 11 11 11 11 11 11 11 11 11 11 11 11 11	0		7	7.8.7			1000			
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HATE CHS HEDLANS HEDLAY CROSSINGS TYPE ERROR TYPE ERROR 179E ERROR	20		4	-81.9	-		0.000			
240, 24 -F3.0 -79.4 31 11 05C4 0.0220 NONE -79.6 -79.4 32 29 0.0240 0.0240		CHS	HEDI	Z	-	TYPE	FREDR	TVPF	FORCE	DEMARKS
-79.6 -79.4 32 29 0.0240 -75.4 -75.4 56 49 0.0400 -75.3 -75.0 10 8 0.0400 -77.4 -75.0 10 8 0.0400		54	- F.C O			94C4	0.020	NOW.		
-75.8 -75.4 56 49 10 8 177.4 175.6 10 8 12 12 12 12 12 12 12 12 12 12 12 12 12			-19-6	101-			0.0260			
175.3 175.6 10 8 177.4 175.5 6 12 175.8 175.5 1 1			9.4	75.						
77.4 77.5 G 12 175.8 175.5 G 12	100		6.46	75.6						
174.0 174.0 T	200		77.4	7.87	•		0.0300			
A HILLS BILLS	350		-75-8	76.2	· -		0.0703			
	10		0.22	1	. 4					

REMARKS							REMARKS								REMARKS	100h							REMARKS	1000						REMARKS	L00P							9704730	REMARKS	REMARKS	REMARKS	REMARKS LOOP	REMARKS LOOP	REMARKS LOOP	REMARKS LOOP	REMARKS LOOP LOOP RFMARKS	REMARKS LOOP RFMARKS LOOP	REMARKS LOOP RFMARKS LOOP	REMARKS LOOP REMARKS LOOP	REMARKS LOOP RFMARKS LOOP	REMARKS LOOP RFLARKS
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TYPE	9SC4						TYPE	NON							TYPE	NONE						000000	TYPE	NON						TYPE	NON						-		NONE	NONE	HONE	NONE	NON	NO.	N C C C C C C C C C C C C C C C C C C C	NONE TYPE	NOW TYPE	1	M 4 M 6 M 6 M 6 M 6 M 6 M 6 M 6 M 6 M 6	M 4 M 6 M 6 M 6 M 6 M 6 M 6 M 6 M 6 M 6	
HENTEN CRUSSINGS		11 8			•	**	MENIAN CROSSINGS	_	1	14	•	14 10	•		CROSS	35 34						•	MEDIAN CROSSINGS	11 21	-	_	æ (31	CROSS			23 23			53	Santagora Matoak		16 19	16 19	16 19 22 19	16 16 16 17 19 19	16 16 17 22 23 19 24 24 24	16 16 17 26 19 27 27 27	16 16 16 17 19 19 19 19 19 19 19 19 19 19 19 19 19	16 19 16 17 26 24 19 27 22 24 23 21 23 21 85) AEDIAN CROSSINGS	16 19 16 17 26 24 19 27 27 24 23 24 23 24 24 23 24	16 19 16 17 22 19 26 24 19 27 23 24 23 21 MEDIAN CROSSINGS 19 16	16 19 16 17 26 24 19 27 22 24 23 21 MEDIAN CHOSSINGS 19 16 16 10	16 19 26 24 26 24 19 27 22 24 23 24 23 21 23 21 19 16 16 10	16 19 26 24 26 24 19 27 22 24 23 21 23 21 23 21 19 16 10 17 22
SNA	-14.9	-14.4	-77.4	-76.4	-70-7	-76-5	SNA	-70.7	-77.1	-79.4	-70.5	-78.5	-79.7	-85.3	SNO	-83.0	F- UR-	-85.C	-60.0	-84.6	-B.3.C		Z	-12.4	-73.5	-74.1	-77-H	9.07	-73.5	IANS	-93.2	-63.0	-94.1	7.46	200	5.60	3		+	-95.0	1001 1001 1001	1 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0	1 1 1 1 1 4 0 0 0 0 4 0 0 0 0 4 0 0 0 0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		3	3	<u> </u>	₹	<u> </u>	<u> </u>
SNA T. 1 ANS	-16.7	-75.0	-75.h	-15.3	-76.6	1.61-	1090	4.67-	-16.3	-19.6	- R.O	-96-5	-41.0	-45.1	WE'U I	9.40-	4 . Ed .	-45.0	2.4E-	L. S. L.	-85.	x . 7 4 -	1035	-14.4	-74.B	-73.4	2.21-		73.7	MFUT	4.64-	-64.7	T . T	4.64	I .		1031	# # Z		-36-	-30.1	-100-1	1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		Lord Sections of the control of the		
SES	*						CHS								CHS								CHS				,			CHS							SH.									CAS	CHS	CH3	Ş	S	Š
NATE.	2400						MATE								RATE								4							1 × 1							DATE									A Te	HA TE	H≱Te	# #	# # T	# #
114	1525	1600	1605	1610	1415	1625	11%	1655	1700	1705	1710	1715	1720	1725	TIME	1605	191	5191	1950	1625	1630	5641	1	1245	1250	1255	1300	1310	1315	TIME	1105	1110	5111	2717	5211	1136	111	1205		1210	1210	1210 1215 1220	1210 1215 1220 1225	1216 1226 1226 1226 1230	1220 1220 1220 1230 1230	1210 1220 1225 1230 1235 1746	1225 1225 1225 1326 1326 1326 1326 1326	1225 1225 1225 1306 1306 1306	1210 1225 1225 1235 1305 1310 1310	1225 1225 1225 1315 1316 1316 1316 1316	1225 1325 1325 1325 1325 1325 1325 1325
25	38						30x	139							Z C	141							2	2+1						SCN.	145						NIIG	146								2	BUN 141	RUN 147	HON 147	741	141

FOM NATA

FOM	DATA										
5	TIME	WATE	CHO	MEDIANS	ANS	MEDIAN CROSSINGS		ERROR	TYPE	ERROR	REMARKS
148	1405			-B6.8	2.48-	13 16			NONE		1000
	1410			-78.4	-77-A	T					
	1415			-17.7	-77.0	7 11					
	1426			\		011					
	1430			4.68-	60.0	13 10					
j	1435			-61.2	-86.5	9 10					
2	1 1 F	PATE.	CHS	4E0I	Z	MEDIAN CROSSINGS		ERROR	TYPE	ERROR	REMARKS
149	1505			-80.5	-80.7	13 11	NONE		NONE		L000
	1515			- XX-	4	9 61					
	1520			100		11 0					
	1525			-46	-85-						
	1536			1.65-		18 13					
2	TIME	RATE	CHS	HED1	Z	MEDIAN CROSSINGS		ERROR	TYPE	ERHOR	REMARKS
150	1235	2400	5¢	-ca-5	-91.3		65C4	3.4070	NONE		400T
	1246			1.05.	-63-3	m, 1		14.400			
	1256			600	700	50		9.77.00			
	1255			# 00°	7.01			2.4900			
	1300			-02.1	-84-1	r (P)		2.0500			
	1305			F-00-	-87.2	31 32		1.4100			
2 2	TIME	HATE	CŦ2	1036	Z	HEDIAH CROSSINGS	TYPE	ERHOR	TYPE	ERROR	REMARKS
151	1325	2400	54	-03.5	0.06-	37 40		5.1000	NONE		1000
	1330			4.46-	1-96-	50 44		4.9200			
	1335			-04.5	-89.2			12.6100			
	1340			80	C. B. C.	40 32		9.3000			
	1365			-0] -0]	4.79			2.5100			
	1 356				100	AS 24		0041-			
9	1 1 1 1	T a O	37.0	1.50	5 - 66 -	34 85		00100			
200	1	1 6	֝֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֓֓֓֓	10.36	Ę	MEDIAN CROSSINGS		FREDR	I YPE	ERMOR	REMARKS
261	424	3044	Ç	***	0.40		4086	00000	NON		1000
	1425			7	1000	E4 04		0000			
	1430			5000	-84.4	64		1.0400			
	1435				-83.5	44 39		9.1070			
	1440			-99.5	185 ° 5			0.1950			
	1445			R.68-	-86.0	45 42		0.3200			
2		KATE	CHS		~	CROSSI		ERROR	TYPE	ERROR	REMARKS
153	1505	7400	*	5.00-	05-	44 50	6SC4	0.8720	NONE		1000
	1151			-92-1	2.16-	94		5.4500			
	1520					46 53		0000			
	1525			6.09	7-06-	44		0000			
	1530			-92.5	-92.3	700		1.5800			
	1535			-AH.2	-84.4	40 45		0.000			
Ş	#11	HATE	CHS	ME01	A	MEDIAN CROSSINGS		ERROW	TYPE	EAROR	REMARKS
154	1615	5400	2	-96-1	-94.7	54 51	92C4	0.2840	HONE		L009
	200			•	6.46	m :		31.0500			
	1620			4.50-	- 60 - 1 - 60 - 1	74		23.1900			
	1635			1000	100	10		0.7100			
	1640			-93.1	0.66-			0.1300			
	1645			2.06-	-60-1			0.0740			

10 10 10 10 10 10 10 10 10 10 10 10 10 1	FED TAN THE TA	1	6 000000000000000000000000000000000000	NONE TO NONE	ERROR	REMARKS LOOP
355 240 24 -76.9 415 415 -77.0 415 415 -77.0 415 415 -77.0 415 540 24 -78.7 46.0 55.5 55.5 55.5 55.5 55.5 55.5 55.5 5		0	6.000000000000000000000000000000000000	NO ME	ı	4007
100	HED I A STATE OF THE STATE OF T	1 × PE 6 × C + C + C + C + C + C + C + C + C + C	6.000000000000000000000000000000000000	1 V P		
115 125 125 125 125 125 125 125	HEDIAN SECTION	0	00000000000000000000000000000000000000	1 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2 × 2 ×		
110 115 120 120 120 120 120 120 120 120	HEDIAN SECTION 110	0	00000000000000000000000000000000000000	1796		
115 125 145 145 145 146 146 146 146 146 146 146 146	HEDIAN SECTION	0	0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	1 Y PE		
14.5 ATE CHS	HED THE STATE OF T	0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 × 0 ×	0.0570 0.0570 0.0570 0.0570 0.0570 0.0550 0.0550 0.0550 0.0550	14 PE		
105 RATE CHS	MED AND AND AND AND AND AND AND AND AND AN	0	6.000000000000000000000000000000000000	TYPE		
100 KATE CHS	HED I A SECOND	- 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0 + 0	CAROR 0.0520 0.0250 0.1030 0.2730 0.2730	TYPE		
1455 1455 1456 1456 1456 1456 1456 1456	HEDIAN	00 00 00 00 00 00 00 00	0.0110 0.0520 0.0280 0.10480 68808 0.4900	PONE	ERROR	REMARKS
150 550 550 550 550 550 550 550	MEDIAN	4 × 6 × 6 × 6 × 6 × 6 × 6 × 6 × 6 × 6 ×	0.0520 0.0019 0.0019 0.10430 0.4000 0.4900	1		2001
155 505 515 516 517 518 518 519 519 519 510 510 510 510 510 510 510 510	MEDIAN		00000000000000000000000000000000000000			
550 5515 5516 5516 5516 5517 5517 5518 5519 5519 5519 5519 5519 5510 5	MEDIAN	1 ∀ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹ ₹	0.0250 0.10450 0.2750 0.4900	•		
505 510 51	MEDIAN	680 680 64	0.1040 0.1040 6.2750 0.4900			
510 54.7 5115 5116 515 516 516 517 518 518 519 519 519 510 510 510 510 510 510 510 510	HEDIAN	TYPE	0.1030 0.2750 ERROR 0.4900			
115 RATE CHS	MEDIAN	TYPE GSC4	0.2750 ERROR 0.4900			
100 E RATE CHS	MEDIAN	TYPE GSC4	ERROR 0.4900			
535 240 24 -83.2 545 -77.0 545 -77.0 555 -74.5 556 -74.5 557 -74.5 558 -74.5 600 -40.1 551 -40.1 551 -40.0 552 -40.0 552 -40.0 553 -40.0 553 -40.0 654 -91.0 655 -64.0 655 -64.0 656 -64.0 657 -64.0 658 -64.0 658 -64.0 659 -64.0 660	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	6 SC +	0.4400	TYPE	ERROR	REMARKS
556 555 555 555 555 555 555 555	61799			NON		1000
545 550 550 550 605 605 605 605 60	11-000		0.0004			Ĭ,
555 555 560 600 600 600 600 600	, - 0 6 6		0.0980			
555 600 1ME RATE CHS H0.1 510 510 520 520 520 520 520 520 520 52	200		0.0170			
600 518	•		0.0520			
11 RATE CHS HEDIAN FEDIAN	•		0.0740			
IME RATE CHS MEDIAN 5510 24 -96.9 5510 24 -96.9 5515 -99.0 5520 -99.9 5520 -99.9 5530 -97.6 5530 -9	•		0.1420			
505 2400 2466.9 51098.0 52599.0 52599.0 52599.0 52597.4 52697.4 615 2400 2497.4 615 2400 2497.6 62097.6 63097.6 63097.6 63097.6 63097.6 63097.6 64097.	MEDIAN CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
510 515 520 525 525 530 1ME RATE CHS	æ	6504	0.2630	NON		
515 520 520 535 535 1ME RATE CHS	÷5		0.5280			
520 525 533 535 535 540 615 620 620 620 630 645 645 645 645 645 645 645 645 645 645	*		0.2050			
525 530 530 540 615 620 620 620 630 630 645 645 645 645 645 645 645 645			0.4190			
530 535 515 516 518 618 620 620 625 631 630 640 645 645 645 645 645 645 645 645	55		0.1180			
1 ME RATE CHS	+ 2+		0.0048			
INE RATE CHS MEDIAN 615 2400 24 -91.0 626 -93.7 630 -92.1 635 -92.1 645 -89.9 645 RATE CHS MEDIAN	53 50		0.0660			
625 2400 24 -91.0 625 -93.7 630 -92.1 636 -89.0 645 -89.0 645 -89.0 645 -89.0	MEDIAN CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
625 -93.7 63.7 63.0 63.0 63.0 63.0 64.5 64.5 MEDIAN	33	6 SC4	0.0350	NONE		
630 -93.7 635 -92.1 635 -89.0 645 -88.5 IME RATE CHS -88.5			0.0272			
6435 - 492.1 6435 - 494.0 645 - 488.9 IME RATE CHS - MEDIAN	2		0.0854			
640 -89.9 645 -88.5 IME RATE CHS MEDIAN	52		0.0968			
040 645 -AB.5 IME RATE CHS MEDIAN			0.0156			
645 -84.5 -94 IME RATE CHS MEDIANS	50		0.0340			
IME RATE CHS MEDIANS	2		0.0115			
	MEDIAN CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
4°18- 42 0042 ccc	9	65C4	0.0035	NO.		
6.98-	45		0.000			
-86.7	04		0.0003			
4.48-			0.0003			
	27		0.0035			
8.48-	‡		0.1020			
	*		0.0747			

RELARKS	REIFFE	RETARKS	REHARKS	REIFARKS	REMARKS	RELEARS
E 2200	ERROR	ERROR	2 2 2 3	E440A	ERROR	FROR
NONE	NONE	TYPE SVPE	7 X 0 V P	7 × × × × × × × × × × × × × × × × × × ×	NONE	NONE
6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	66 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6			FRROR	A00000	6.0012 6.0012 6.0012 6.0012 6.0012 6.0012
1 Y PE 65C+	17PE	→ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	17PE 6SC4	TYPE SVON	17PE 0SC4	0 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
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FOH DATA

REMARKS					-	MEMARKS							REMARKS								REMARKS							MEMAMAS							DEC DAY						RFWARKS	DEC PAD						
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1 Y PE	302				-		NO.						TYPE	NONE	-						TYPE	MON						344	NONE						1						TYPE	HON						
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NO.	TIME	RATE	CHS	#£0	MEDIANS	MEDIAN C	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	FDROP	PEARKS
192	1520	2400	2	-160.0		25		ASC4	2.8100	NONE		
	1525			-1001-	-103.0	ž.	17		1.4600			
	1530			2.66-	-103.0	23	18		1.4100			
	1535			8.86-	-105.4	23	23		1.2500			
	1540			-101-0	-103.4	23	=		2.3100			
	1550			2-101-		5 6	01		2.7000			
Ş	TIME	RATE	CHS	O AM	MEDIENS	MEDIANC	MEDIAN COOSSINGS	TVDE	2000	TVD	2000	DELLABORE
193	950	2400	24	-96-3	-103.5	32	12	65C4	1.1100			MEMBERS
	955			-97.3	-103.4	27	9		0.8610			
	1000			-97.4	-103.3	20	15		1.6200			
	1005			-97.2	-103.3	92	25		2.0700			
	1010			-97.3	-103.4	21	18		1.0300			
	5101			2-96-	-102.9	28	21		1.2700			
	1020			-97.4		25	16		0.9250			The second second
5 6	2 4 4 5	346	S 6	200	SNY	MEDIAN	AN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REHARKS
	0001	2007	\$	2.66-	-101-	23	8	65C4	0.3010	NONE		
	1055			4.46-	-101-5	17	=		0.5210			
				E * 6	-100-1	0	9		0.5010			
	5011			-161-7	-101-	17	5		0.3340			
	0111			-03.7	-100-	6	EI :		0.3810			
	5111			-101-7	0.101-	± :	2		1.2500			
200	1146	RATE	CHS	TIL SHI	ANS	MEDIAN	NA CONSCILLOS	1000	0.000	1000	0000	97077
198	1605	24.00	54	2.76-		22	23	85C4	0.1430			MEMBERS
	1610			-97.3	-102.4	12	35		0.1070) E		
	1615			4-76-	-103.5	72	3 2		0.1500			
	1620			0.96−	-102.8	39	107		0.2280			
	1625			-101-1	-98.2	83	142		0.0800			
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2	10.50	DATE	VHU	1037	101-	45.74	75 42	407	0.2340			
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	1135			-05.0				1364	34.45	1		
	1140			-95.2		4			39.8600			
	1145			-92.2		•			27.3500			
	1150			9.46-		25			1.6700			
	1155			-92.1		31			1.0200			
3	174	DATE	977	200	• 3 • 50 T 6 1 6	5	3000.3300		3.1500			
201	1415	2400	2	-1001-	2 30 L	751144	1000	1776	NOW S	3441	ERKOR	REMARKS
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	1425			9-20-	-104.7	37	: 2		0.5770			
	1430			-48.1	-104.0	4 3	72		0.3010			
	1435			8.66-	-104.5	53	11		0.7220			
	0			-99.7	-105-1	53	2		0.5260			
				7.66-	-102.0	24	92		0.8040			

REMARKS	RELARKS	REMARKS	REBARKS	R E E E E E E	RELARKS
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TYPE	NONE	17PE NONE	NOME NOME	F 20 20 20 20 20 20 20 20 20 20 20 20 20	NON
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NONE	NON NON P	NONE	NONE	NONE	NONE
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FOH DATA

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7 7		4365							1405	4266							TVDE	6SC4							TYPE	6SC1							TYPE	6SC4						TYPE	65C4			1	4286					
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E STATE	6 141	2019 602			79.1 -78.5	-78-7 -78-0			LANS	-82.4	-77				-77-3 -77-0		TANS	1.18	-87						SMAIC				-74.8 -80.2			0.78-	SHATC				-/A.c -63.c	-71-5	-77.3		74.8	-77.2	17.3	SNAT		•		1 70 1 10	200-	
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	ERROR							5012.1	ERROR								ERROR								ERROR								ERROR		•					ERROR							
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	MEDIANS	-77.7	-73.2	-16.3	-70.0	-77.6	2.6	-75.7	TEUI ANS	9.68-	-87.1	-85.3	-93.3	-91.7	-89.7	-86.8	MEDIANS	9.66-	-99.5	-96.H	9.96-	-96-0	96-		Z	9.46-	-94.2	-94.7	2.16-	-94.9	-94°C	-95.1	MEULANS	97.6	6.96-	-96.2	4.46-	-100.5	-100.6	SKI	-43.7	2.16-	1.05-	-92.0	-93.0	-04.0	-63.3
	MED	-78.n	-77.5	-41.8	-B4.9	-14.6	-79.8	-A2.5	150	-82.4	-81.5	-79.5	-R6.7	-H7.2	-F3.2	6.68-	HED	-91.4	-94.5	-98·S	-46.3	-87.9	-00-	9.06-	MEDI	1-16-	-95.7	-92.6	-88.3	F- 25-3	-05.5	-92.8	HED.	1000	4-96-	1-95-7	-93.A	-49.5	-09.6	"EUI	-01.0	-49.3	0.06-	-91.5	T	•	-61.3
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REMARKS	REMARKS	REMARKS LOOP	REMARKS LOOP	REMARKS LOOP	LOOP LOOP
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NONE	TYPE NONE	N V V P E	TYPE NONE	NONE	NONE
FAROR	ERROR	EAROR	ERROR	ERROR	ERROR
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MEDIAN CROSSINGS 26 24 26 23 26 30 26 36 62 31 30	CROSS	CROSS	MEDIAN CROSSINGS 4) 28 20 19 15 14 21 23 30 29 36 29	CROSS	C
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FOM DATA

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	LIAN	CROSS	TYPE	ERROP	TYPE	ERROR	REMARKS
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Ì		17 21					
ī		50 16					
•	-85.3 -81.9	17 16					
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	MIC	CROSS	TYPE	ERROP	TYPE	ERROR	REMARKS
Œ	9.2 -87.3	15 19	NONE		NONE		1000
ï	-89.7 -87.6		!				
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	UTAN	MEDIAN CROSSINGS	TYPE	00004	TVDE	90804	DEMADES
			PACA	2000		-	
		17	2002		NOME		-00
ī	-84.0 -83.0						
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	MAIC	CHUSS	TYPE	TAROR	TYPE	ERROR	REMARKS
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	JIAN	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
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1		19 14					
	JIAN	MEDIAN CROSSINGS	TYPE	ENROR	TYPE	ERROR	REMARKS
•	-84.4 -82.5	20 14	NONE		NONE		LOOP
•	H4.9 -86.8	17 20					
•							
•		19 21					
•							a
•		56 23					
ı	-RE.0 -86.2	_					

REMARKS	REMARKS	REMARKS	REMARKS	RETARKS	REFERENCE
ERROR	ERROR	E R R O R	ERROR	ERROR	ERROR ROR
TYPE	TYPE	TYPE	TYPE	TYPE	NONE
A 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	R P P O B P P P P P P P P P P P P P P P P P P	A S S S S S S S S S S S S S S S S S S S	ERROR	ERROR ROS	ERROR
NONE	NONE	NOVE	NONE	NONE	NONE
26 22 22 26 25 28 25 26 25 25 25 25 25 25 25 25 25 25 25 25 25	CA0SSI	CROSS	CROSSI	CROSS	CR0 SS
		MEDIAN COLUMN			REDIAN RE
NA1071 NA1071	#EDTANS - 4 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	2	Ž	MEDIANS 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MEDIANS 1.2 - 83.2 2.2 - 81.2 2.4 - 81.5 1.4 - 79.8
01111111 0110000 01100000 01100000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				\$ 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
SE S	C is	S.	CHS	CHS	SE .
KATE	HATE	MATE	RATE	RATE	PATE
11205 12205 12205 1225 1225 1225 1235	1410 1410 1420 1420	1136 1525 1525 1530 1540 1550	1000 1000 1000 1000 1000	11111111111111111111111111111111111111	11225 12235 1236 1245 1255 1255
267 767	2 9 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	200	270 270	27. 17.	55 55

E A E E E E E E E E E E E E E E E E E E	RETARKS	E ARK	A A A A A A A A A A A A A A A A A A A	A A A A A A A A A A A A A A A A A A A	REMARKS LOOP
FROR	FROR	A C R R	R R R R	ERROR	EAROR
NOVE BNOVE	NON NON NON	NON NE	NON NONE	NON NEW NEW NEW NEW NEW NEW NEW NEW NEW NE	7 7 7 0 7 0 7 0 7 0 7 0 7 0 7 0 7 0 7 0
FROM	ERROR	ERROR	2008 2008 2008	R R R O R R	ERROR
TYPE	NONE	TYPE NONE	TYPE	NONE	TYPE
MEDIAN CROSSINGS 16 19 19 16 87 41 19 17 19 17 19 17 18 17 18 17 18 18 18	MEDIAN CROSSINGS 14 16 16 16 26 42 14 11 14 12 16 17	CROSSI 133 233 233 233 233 233 233 233 233 233	CROSS	SORO	CROS
4EOIANS -5 -77 -0 -7 -77 -0 -7 -77 -5 -7 -77 -3 -1 -75 -4	Z	741	N 10	7 A 1	MATO
, , , , , , , , , , , , ,	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		NM		*
CHS	§	8	S. S	&	£
RATE	A A A	A 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	* * * * * * * * * * * * * * * * * * *	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	MATE
1330 1330 1330 1330 1340 1340	15.00 15.00	1615 1615 1620 1630 1635	11 ME 111 S 111 S 112 S 113 S 113 S	112240 12240 12250 1300 1300	1355 1355 1400 1410 1415 1415
273 273	274 274	275 275	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

FOM DATA

REWARKS LOOP	RELABKS	REMARKS	REMARKS LOOP	REMARKS LOOP	REMARKS LOOP
ERROR	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	R C R C C C C C C C C C C C C C C C C C	A C C C C C C C C C C C C C C C C C C C	R R R O R	E ROB
NONE	N N N E E	NONE	NON	NONE	NONE
ERROR	ERROR	EAROR	ERPOR	ERROR	E RROB
NON	TYPF	NONE NONE	NONE	NON NE	TYPE
MEDIAN CROSSINGS 98 95 101 95 88 91 76 68	76 72 72 72 72 72 72 72 72 72 72 72 72 72	MEDIAN CROSSINGS 73 68 64 70 75 74 49 41 40 40	MEDJAN CROSSINGS 47 45 50 46 51 41 45 41 45 46 46 46 46 46 46 46 46 46 46 46 46 46	MEDIAN CROSSINGS 37 34 34 45 46 45 46 39 37 36 35	AN CROSSINGS 33 32 32 34 26 34 40 38
MEDIAN C 101 101 88 98 76	MEDIAN C 32 32 40 74 77 40 699 699 699	MEDIAN C 73 754 759 759 759 759 759	MEDJAN C 67 C 50 50 61 61 61 61 61 61 61 61 61 61 61 61 61 6	FEDIAL AND AND AND AND AND AND AND AND AND AND	MEDIAN C 33 34 36 36 36 36 36
ANS 1 1 88 8 2 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4EDIANS 44.0		\$11111	AN 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11000 H
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	# 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		46.8 196.9 197.4 197.4 197.4	\$11.0000 \$11.0000 \$4.00000 \$4.0000000000000000000000	107.5 T 110.0 T 10.0 T
CHS	S.	CHS	C t S	CHS	S.
2 P. T.	A 16	द ज	RATE	RATE	EATE
11 ME 1500 1505 1510 1515 1520	15330 1605 1605 1620 1633	11865 1655 1705 1705 1716 1715	11ME 1045 1045 1055 1100	11155 1120 1205 1205 1225	11ME 1255 1306 1316 1315
2 S S S S S S S S S S S S S S S S S S S	2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	290 290	297	298 298	299

	OR REMARKS								OR REMARKS							OR REMARKS	1006					OR REMARKS	L00P						L00P																					
	TYPE ERROR		,						YPE ERROR	NONE						TYPE ERROR	ONE					YPE ERROR	NONE					I TPE ERROR	JAN D																					
	ERROS								ERROR	2						ERROR	~		0.0981	0.3345			0.0078 A	0.0335	0.1872	0.00 E			1000-0	24.0.0	020100	66100	0.00.0	0-0211	•															
	TYPE	PACM							TYPE	NONE						TYPE	6SC4					TYPE	6.SC4					44	43SE																					
	MEDIAN CROSSINGS	EC #C		25 23			27 19		CROSS	45 48		32 23		23	56 24	CROSS	37 33		29 24	33 32	41 41	MEDIAN CROSSINGS			32 35		1E 24	2002	33 28	62		25		34																
	MED TANS		2 101			-101-			VED I ANS			-100.H				JIAN	-82.1				-84.3	MEDIANS		-63.1			1.68-	7	0 0 0 7 1			178-4											100						6.28-	•
	¥,	-1001	100	E-0.1-	F. 50-	4.70-	4.00-	0.00-	T.	4.60-	6.60-	-66-	-49.		2.66-	₩.	-42.5	-82.3	-A2.A	-83.9	- H4-1	1	7.40-	-43.3	-86.0	0.4	7+2+-	1031	200	1.20	1 1	72	-77.9	-75.7	-76.3	-78.3	-18.5	Ŭ•61−	-80.0	-80.6	1.79.0	1.11.		7.01-	***	4. LR.	0.18-	4 · C	7.74	- 600
	CHS								CHS							CHS	54					CHS	\$				270	ָרָהָ בַּי	5																					
	PATE								HATE							MATE	2400					HATE	2400				14.4	240																						
NATA	TIME	1405	1410	C1+1	1450	1425	1430	1435	TIME	1545	1550	1555	1590	1605	1510	71:4E	1255	1300	1305	1310	1315	1 1 ME	1425	1430	1435	6447	1 4 5 5	36.16	1 420	1436	1530	1535	1540	1545	1550	1555	1600	1505	1610	1615	1520	6261	9000	6501	0+01	1045	1661	1700	201	
F03	5	300							EN S	301						S	303				1	2	304				2	200	200																					

5	DATA							•				
202	TIME	PATE	CHS	134	HEUIANS	MEDIAN CRUSSINGS	OSSINGS	TYPE	FRRDA	TVPF	acaa.	RFWARKS
306	1220			6.46-	-92.1	101	103	NONE				900
	1225			4.46-	7.06-	106	107	!				
	1239			2.40-	-43.0	115	109					
	1235			-45.0	-63.7	103	107					
	1540			4.46-	-00·x	126	117					
2	11	MATE	SES.	ME.D	MAI	MEDIAN CRUSSING	OSSINGS	TYPE	FRROA	TYPE	ERROR	REMARKS
307	1305			-05.5	6-13-	123	117	NONE		NONE		1000
	1316				190.0	115	001					
	1320			0.10	400	7 2	- 6					
	1325			6.20	1-06-	113	109					
200	TIME	KATE	CHV	MENT	Z	MEDIAN CROSSING	OSSINGS	TYPE	FRACE	TYPE	ERROR	REMARKS
308	1350			-BH.	-87.0	145	134	MONE		NONE		1000
	1355			-HH.	-87.6	123	118					
	1400			-A1.2	-86.0	130	133					
	1405			-H7.6	-83.2	123	104					
1	1410			-HZ.2	-81.0	120	127					
Ş	114	KATE	CHS	JU3⊬	IANS	MEDIAN CROSSINGS	OSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
300	1500			1-25-1	-93.5	5.0	110	NONE		NONE		1000
	1505			2.26-	+* 26-	145	149)		
	1510			1.26-	6.26-	139	152					
	1515			4.26-	-92.5	141	142					
	1520		:	-41.5		145	131	100	NA CASSILL		100	200000000000000000000000000000000000000
5	T I WE	KATE	SHO	TOBE	S.N.	MEDIAN CROSSINGS	OSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
310	1550			V . O. C.	-89-	137	137	NONE		NON		L000
	6661			- C	700	64.	9					
	1605			× × ×	64.4	9 :	611					
	1010			T T	4	136	0 0					
	1615			200	-80-	110						
	1620			-00-	-80	*	22					
S	TIME	MATE	CHS	HEDI	Z	MEDIAN CROSSINGS	OSSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS
312	1205			-43.3	-88.h	157	147	NONE		NON		NOW DIV
	1210			-H3.0	-88.2	151	154	1				
	1215			-82.5	-88.5	152	138	•				
	1221			-A-0.8	-81 .3	89	16					
	1225			-82.9	-89.5	157	124					
	1230			-R1.0	-87.1	154	147					
	1235			-44.0		150	151					
2	TIME	HATE	CHS	HEO I	Ž	MEDIAN CR	AN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
313	1315			-42.7	-96-3	137	134	NONE		NONE		NON DIV
	1350			-82.5	-90.5	139	121					
	1325			- F. C.	-96.5	132	123					
	1001			E . I . I	***	96.	*21					
	1355			9.18-	2.88-	134	118					
	1 340			4. [1.	0.81	, A =	117					

REMARKS NON DIV	4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	000	REMARKS LOOP	REMARKS	REMARKS LOOP	REMARKS LOOP
ERROR			A SA	200 200 200	A S S	ERROR
TYPE	- L		NONE	TYPE	NONE NONE	TYPE
ERROR	800		8000 8000	00 ag	FREGR	FROR
TYPE	TYPE	NON	NOVE	14PE NONE	TYPE	TYPE
MEDIAN CROSSINGS 148 126 183 174	CROS	55 68 77 71 73 71 62 76 78 61 93 61	AEDIAN CROSSINGS By AD By AD By By By By By By By By By By By By	MEDIAN CROSSINGS 17 24 30 26 30 38 28 34 25 28 31 31	01av CROSSINGS 39 33 27 31 33 32 41 29	MEDIAN CROSSINGS 33 35 33 35
7.00		5255555	NN NN 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11276	ANS MEGI. -79-0: -75-4 -76-2 -78-6	
MEDIANS 186-2	A. W. A.	175.0 175.0 175.0 175.0 175.0	45.5 -75.5 -75.7 -75.7 -75.7 -77.0	AED 12 -94-1 -96-9 -96-9 -95-1 -95-2	MEO11 -78.8 -76.0 -77.4 -74.0	HEDIA -79.0 -79.2 -78.3
CHS	£		r E	S S	Ç i	Š
RATE	KATE		X 4 3	X T T	RA H	MATE
1415 1415 1420	1430 1445 1445 7146	1615 1625 1639 1640 1640	1105 1110 11120 1125 1130	17 1 1 2 3 5 1 1 2 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1350 1350 1400 1405	11#E 1425 1430 1435
314	5	že į	8 T T	318	319	320 320

FOH DATA

RELARKS	RELARKS	REMARKS	RETARKS	REMARKS		RELEAKS
E ROS	FRE	ERROR	FROR	44 00 44 00	N N N N N N N N N N N N N N N N N N N	28 20 20 20
NONE	NONE	TYPE	NON	NONE		NONE
0.0000 0.0000 0.0000 0.0000 0.0000	0.0017 3.0300 1.2700	0.0051 0.0051	27.300 0.000 13.500 3.000 4.200	2.8000 2.8000 3.7200	3.3700 3.3700 3.2800 10.4000 11.8300	5.7800 13.2300 5.3100 1.8300
TYPE 6SC4	TYPE GSC4	TYPE GSC4	1 ¥ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽ ₽	G > C G S S S S S S S S S S S S S S S S S S	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	179E 6SC4
MEDIAN CROSSINGS 34 33 40 40 40 40 40 42	CROSS	MEDIAM CROSSINGS 30 29 31 24 31 36	CROSS	MEDIAN CROSSINGS 30 25 17 20 17 20 17 39 17 34	406681	MEDIAN CROSSINGS 21 16 24 19 23 18 25 22 29 22
MEUTANS 197.0 193.5 196.1 193.7 116.6 193.5 187.0 193.6	MATO	MEDIANS -AB.5 -91.5 -A7.4 -91.6 -A8.0 -92.4	7 H	Z Z	-82.4 -91.7 -91.2 -91.2 -91.2 -90.2 -90.9 -90.9 -90.9 -90.9 -90.9 -90.9 -90.9 -90.9	MEDIANS -84.9 -93.2 -84.1 -91.2 -44.9 -92.4 -83.3 -91.5
HATE CHS 2400 24	740 740 740 740	RATE CHS 2400 24	RATE CHS 2400 24			HATE CHS 2400 24
RUN TIME 1 235 1 240 245 245 250 250 250	200 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 550 600	AUN TIME 1500 1510 1510 1515 1515 1526 1530			7 2235 7 2235 7 2235 2240 2245 2250

PCM DATA

5	DATA										
5	TIME	HATE	CHS	MEDIANS	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
©	0	2400	\$2	-84.0	-92.9	22 20		4.3100	NONE		
	S			-62.8	-92.4	26 24		21.7900	10000		
	10			-F2.8	-91.4			18.9000			
	15			-H3.1	8.16-			31-1400			
	2350			-A2.1	-91.0	16 20		4.8000			
	2355			-82.2	-91.9	21 20		3.6100			
2	TIME	RATE	CHS	HED I	ANS	CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
•	1810			-82.2	-86.5	33 34	NONE		NON		
	1815			-A2.2	-85.9						
	1820			-42.1	-86.1						
	1825			-82.6	-87.1						
	1830			-BO	-85.4	20.00					
	1835			-79.1	3-8-						
	1840			-79.6	-83.1						
5 S	TIME	HATE	CHS	MEDI	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	FRROR	REMARKS
10	1905	2400	54	-78.4	-8].4	N	FRED	0.0004	NON		
	1910			-78.4	4.18-			0.0001			
	1915			-76.2	-79.3			0.00.0		•	
	1920			-77.B	-80.6			0.0007			
	1975			-76.6	-79.5			0.0010			
	19:0			-77-3	-80.7	26 25		0.0011			
Š	TIME	RATE	CHS	103h	ANS	CROSS	TYPE	ERROR	TYPE	FRROR	REMARKS
=	1205	2400	54	-79.1	-84.5	28 32	FRED	7.4800	NON		
	1210			-A1.4	-86.5		<u>`</u>	9.2100			
	1215			-78.6	-R4.8			7.7000			
	1220			-79.3	6.48-	39 35		8.9800			
	1225			-77.A	-83.7			6.7800			
	1230			-7H-7	-85.2			8.7600			
Ş	TIME	RATE	CHS	MEDI	ANS	CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
12	1635	2400	54	-73.1	-77.5	16 18	FRED	0.6200	JNON		
	1640			-74.2	-77-7	• -		1.2700			
	1545			-73.2	-77.6	:		3.8500			
	1650			-73.4	-77.4			1.5700			
	1655			-13.4	-76.3	-		1.1500			
	1700			-72.7	-14-4	15 14	1.000	0.7800			
5	1	K A L	\ E \ (HEDI	ANS	CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
7	6011	2400	*	4 4 4 T	-96-1	77 74	FRED	1.8000	NONE		
	1115			4 4 4 4	. 44			0060-7			
	1126			20.0	-K6-4	22 T2		0000			
	1125			4	-45.4						
	1130			1.44	-H4.7			00040			
200	TIME	HATE.	CHS	1 (134	ANS	185092	TVDE		TVDE		DELLOVE
*	1335	2400	2	-87.8	-88-8	2	FRED	S.4400	PAONE		
	1340			8.7.a	2.08-			0010			
	1 345			47.6	20.64						
	1350			F 7 8 8	647.9			0.420			
	1355			4.79				1 0200			
	1400			0.10	10.10	20 20		•			
) }			4				0.1100			

	-				
REMARKS	REILARKS	REMARKS	A A A A A A A A A A A A A A A A A A A	REMARKS REMARKS	
EAROR	EAROR	ERROR	ER RO	ERROR OR	
N N N N N N N N N N N N N N N N N N N	TYPE	NON P	TYPE TYPE NONE	TYPE NONE TYPE	NON
# 00000 # P. N. O. N. O. E. C. O. C.	FRECR 0.00140 0.0150 13.0300 14.0300	200	2.4808 2.4808 2.3170 2.3170 2.4700 2.4700 2.4700 2.4700	ENROR 9.0200 7.0300 4.9100 30.7100 11.1300 9.1600 ERROR	10.4600 12.7500 13.0500 10.4000 3.1400
FRED	17PE 65C4	NONE	0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	FAED TYPE	A C
CROSSINGS 19 19 22 20 20 160	110 110 132 110 1108	05517 70 70 65 65 64 60 60 60 60	AN CROSSINGS 55 65 70 65 70 65 70 65 85 85 80 95 110 95 110 90 100 90 90 90 90 90 90 90	AN CROSSINGS 77 75 77 75 86 70 68 65 58 56 50 58	N 4 N 9 0 N 4 O N N O O N H
MEDIAN CR	MEDIAM CROSSINGS 109 110 129 132 110 110 111 10A	MEDIAN CROSSINGS 62 65 62 65 70 60 52 61 54 60	MEDIAN CROSSINGS 55 65 70 65 70 65 75 85 85 85 103 95 110 95 110 95 110 95 95 90 96 90	MEDIAN CROSSINGS R2 77 75 75 86 70 68 65 58 55 58 60 50 50 50 50 50 50 50 50 50 50 50 50 50	6 10 0 6 10 10 4 6 5 10 5 10 4 10
4 C 9 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2 C 2	NN NN NN NN NN NN NN NN NN NN NN NN NN	10000 100000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 1000	AN 1 1 NA 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2	MW 1 7 60 60 60 60 60 60 60 60 60 60 60 60 60
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1000 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	197.2 195.7 195.7 197.1 195.3 195.3 195.3 MEUIANS	
24	CHS 24	N E	7 P 8 8 8 8	S. S.	¢
2400	RATE 2400	HA TE	2400 E	RATE 2400	2400
1516 1516 1516 1526 1526 1536	11MF 2225 2230 2240 2240	11111111111111111111111111111111111111	11111111111111111111111111111111111111	11155 11155 11155 11155 11155 11155	1350 1355 1400 1405 1415 1415
15 E	20 c	19 P	Ze ze	Ze Z	E

PCH DATA

Š	DATA											
35	TIME	A	CHS	WFULANS	ANS	MEDIAN CROSSINGS	TYPE	EPROP	TYPE	ERROR	REMARKS	
35	1505	2400	9	-92.7	-94.5	94	FRFD	0.8900	NONE			
	1516			-43.7	-95.1	•		1.2500				
	1515			-41.1	-92.7	*		0.1800				
	0261			-47-7	-89.4	04 64		0.4400				
	1530			2000	- 101	14 95		0.2700	•			
	1535			-92.6	-96-1	90 EE		1.3000				
200	1 IME	RATE	CHS	MEUL	ANS	CRUSS	TYPE	FHROR	TYPE	ERROR	REMARKS	
	_	•	9	0.92-	-84.4		FRED		NONE	Ì		
•	1616			0.00-	-91.3	36 40		CONT. 100				
	1915			2.64-	-61.1			0.3500				
	1520			E. ##-	-H9.6			0.0480				
	1625			-86.E	-91.0	43 44		0.4300				
	1630			-87.7	2.68-			0.0740				
200	TIME	TATE	CHS	_	3	POOCT	1406	001100	-	90999	97647140	
ř	1750	2400	•	•		53 5335		0.6910		CHANGE	MEMANKS	
	1755			-A6.0	-88			0.0680				
	1800			-40.3	-93.2	70 05		0.3200				
	1805			-88.7	-92.5			0.3400				
	1810	•		-91.5	-94.6			0.5200				
	1815			-88.6	-92.4			0.6600				
	1420				-91.5	56 51		0.2000				
200	ME I	RATE	CHS	=	ANS	MEDIAN CROSSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS	
33	1330	0.0	ç	r7-	-67.5		4386	0.0940	NON			
	1335			1-96-	-84.0			0.0646				
	1340			-91.4	-88.6			0.1200				
	1360			200	6.69	46 60 10		0.0470				
	365			40	7			0.1200				
200	TIME	HATE	CHS	14401	ANS	SENISSORD NATURE	TVDE	0000	TVDF	90905	DELLEGUE	
36	1425	2400	71	-66-	-96-2		GSC.	0.4600	NONE.	KOKKY	MEMBERS	
	1436			1.60-	-34.2	71 57		0.4300				
	1435			F-77-7	-94.5			0.1000				
	1440			2.00-	-90.3			0.1300				
	1460			5.50				0.5200				
	1455			7 - 1	7-46-	69 50		0000				
\$ 2	114	MATE	CHS	Ξ	á	CROSS	TYPE	FPPOD	TYPE	FRROR	RFMARKS	
37	1535	2460	72	-45.0	-94.5	69 99	65C4	0.0150	NONE			
	1540			0.40-	-93.0	7		0.0250				
	1545			-62.8	-91.5	וחצ		0.1240				
	1555			- I 6-		 •		0.0140				
	1400			0.00	-	- 4		0.1540				
	1605			20.00	7.00	45 34		0.0230				
302	TIME	HATE	CHS	=	ANS	CROSS	TYPE	FRACE	TVPF	a Cao	DEWADER	
36	1625	2400	12			53 44	6504	0.0001	NONE			
	1630			-89.2	-68.S	47	}	0.0100				
	1035			-89.3	-84.4			0.0100				
	1640			-H0.1	-88-7	53 55		0.0050				
	1645			-A4.0	-44.5			0.0030				
	1650			-87.9	7. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15	20 C		0.00 T				
	5601	-		***	64.5	•		0.0007				

REMARKS								REMARKS								REMARKS								REMARKS								REMARKS								REMARKS								
ERROR								ERROR								ERROR								FRROR								ERROR								ERROR								
TYPE	MON							TYPE	MONE							TYPE	NONE							TYPE	LACA							TYPE	MONE							TYPE	NON	!						
FHROR								EHROR	1.4500	1.1600	7.3300	1.5100	0.8300	0.0940	0.5700	EAROR	1.3800	1.4200	1.3600	0.9700	1.8800	0.4700	0.2300	ERROR	0.600	0.2400	1.3200	0.6900	0.1600	0.4200	0.5900	ERROR	1.8900	1.6400	1.0700	3.4100	0.8500	1.0400	0.9900	ERROP	0.0010	0.5300	0.0015	0.6800	1.6200	2.4300	1.2000	
TYPE	NONE							TYPE	6SC4							TYPE	FRED							TYPE	65C4							TYPE	6504							TYPE	6504							
MEDIAN CROSSINGS	24 14	63 52	63 55			58 53		MEDIAN CROSSINGS	47 51	41 46	47 46				22 26	MEDIAN CROSSINGS			~	51 43		47 48	•	HENTAN CROSSINGS	39 39	32 26	25 45	21 21		25 28	36 36	MEDIAN CROSSINGS				32 27			23 24	MEDIAN CROSSINGS	15 15		15 16	_		19		
	-87.2	-d4.4	-86.4	-87.2	-87.9	-86.1	-88.6		+-06-	E-66-3	-49.1	-88-	-84.B	-82.5	2.18		-87.5	-88-	-84.4	-87.8	-85.5	-85.9	-83.5		-85.0	-81.3	-45.R	-81.4	-82.3	-83.4	2.5	ANS MEL	-90.3	-68.3	2.06-	+006-	-00-x	-88.5	4.00		18.2	-A0.1	-76.7	-85.0	-85.8	-86.1	-84	
HEDTANS	-45.5	-44-	-84.7	-85.3	-40.4	9.94-	-46.3	10	-88.6	-47.6	-87.0	-85.9	-84.0	-41.2	-60.5	2	5.98-	-86.5	-84.1	-85.3	-H4.7	-44.6	-A3.0	MEDIA	-A3.6	9.04-	-43.6	-74.5	-10.4	-80.9	-A2.7	5	-88.2	-P6.1	-98.0	-89.1	-88.0	-86.4	-86.0	MEDIA		-77.6	-75.0	-82.1	-84.8	-85.4	-82.6	
CHS								CHS	12						1	CHV	2							CHS	12							CHS	£.							CHS	•							
HATE								MATE	2400							TAN	2400							KATE	2400					٠		•	2400							HATE	2400							
TIME	720	175	730	735	740	745	751	11 FE	W I O	415	950	956	830	835	4	- 1	606	017	912	920	425	430	435	114E	1005	1910	1015	1020	1025	1030	1035	TIME	1105	1110	1115	1120	1125	1:30	1135	TIME.	1205	1210	1210	1215	1220	1225	1230	
200	30							200	04							2	-							2 2 2 2	45							Š	* 3							5 2	*							

4	Ľ	T C C C C C C C C C C C C C C C C C C C	MFUTANS	MEDIAN	MENTAN CONSTINCT	TVDE	50000	107	2007	DEMADOR
	£ •	-75°B	-77.	NA LOUAN	CROSSINGS	GACA	D-0410		ERHOR	REMARKS
	1, 1	-19.5	-81.2	21	10	1	0.1400	TACKET.		
		-A3.4	-82.7	23	_					
		-77-3	-78.9	20						
		-A1.5	-H3.3	20						
		-7H.7	-80.H	33						
		-R].0	-63.7	33	35					
MATE	CHS	MEDI	ANS	MEDIAN	CROSS	TYPE	ERRON	TYPE	ERROR	REMARKS
•	9	-43.7	-45.1	24		FRED		NON		
		0.40-	4.16-	+1	4.2		2.6600			
		-06.1		31			1.7700			
		-04.4		£.4			0.1600			
		1959-	-47.2	65	64		0.6000			
		-05.4	-9B.0	38	42		0.6800			
		5.46-		64			0.7800			
:41	CAS.	MEDIANS	PNS	MEDIAN	MEDIAN CROSSINGS	TYPE	ERROH	TYPE	FRROR	REMARKS
2400	9	9.47-	6.46-	63	4	9SC4	0.170	NONE		
		-45°F	46-	₩.	33		0.4200			
		-46.4		9+			1.1400			
		8.50-		58			1.0500			
HATE	CHS	MEDIANS	ANS	MEDIAN	MEDIAN CROSSINGS	TYDE	FHROP	TYPE	FRROR	REMARKS
0	٥	-43.6	-95.0	7		FRED	0.8200	NON		
		-03.1	-93.4	45			0.1100			
		1.40-	0.96-	31	33		0.7400			
		4.56-		98			1.1400			
		200		D (0.3100			
		6.00	200				3.7000			
	0			מי ל		1	000		1	
XAIR	CHO	MEDIANS	ANS	MEDIAN	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
0	v	P.00-	6			6 SC 4	1.0800	NONE		
		E . OK .					0.7800			
		-46.3	- HH-				0.5600			
		- KK - 3	4.06				0.2200			
		T P	2.26-				0.7100			
							0002.0			
	4	6.67	1.16-		3000 3000		0.5500			0.00
20047	2	F 60	•	AND TOTAL	2003	4 0 0 0	PERMON	I YPE	ERKOR	REMARKS
-	e.	****	-1001-			650	0.10.	NUN		
		1-96-	-98.6	5	9		4.2600			
		4.65-	-1001-	57	5		11.1100			
		2.00-	-99.1	14			7.3700			
		-040-	4.66-	7.6	68		3.4100			
		0./6-	-97°	60	77		3.8800			

REHARKS	RFM BRKS	REMARKS	REMARKS	REMARKS.	RETARKS	REM ARKS
ERROR	0.5% 0.0990 0.0990 0.0960 0.0060 0.0060	0.1270 ERROR	ERROR	EAROR	FROR	ERROR
NONE	TYPE	NONE NONE	NONE	N N N N N N N N N N N N N N N N N N N	14 NO NO N	NON
2.4090 3.1550 1.1330	11.3670 11.3670 1.8340 1.1840 0.7890	1.1339 1.0850 1.0970 0.2770 1.1680	11.1090 6.7550 7.4590 5.3930	3.6790 3.6390 3.4390 2.2760 2.2840	2.8300 2.8300 2.5300 2.5960	1.0690 1.0690 1.7210 7.0980 1.0530
TYPE	7	TYPE	179E	FRED	7 Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	FRED
4EDIAN CROSSINGS 7 7 7 12 10 19 14	MEDIAN CROSSINGS 13 19 16 11 8 255 15 26 13	#Enian CROSSINGS 10 7 16 14 16 26 26 21 16 18	HEDIAN CROSSINGS 20 20 14 12 15 16 15 17	C	CROSSI SS SS	CROSS
185 191.7 191.7 190.7		1871 1857 1867 1867 1867 1867 1867 1867	AN 11 11 11 11 11 11 11 11 11 11 11 11 11	ANS 1952 1957 1951 1951 1951 1951	NSA N 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ANS 4000000000000000000000000000000000000
MEDIANS 1922.0 1923.0 191.0	=	4	Ħ	1	=	5
\$ \$. .	CHS 24	12	S 4	12	S 9
HATE 2404	PATE 1200	1 4 6 6 4 6 4 6 4 6 6 4 6 6 6 6 6 6 6 6	1200 1200	140 140 140	2604 2604	PATE CAUS
1118 1498 1506 1516 1516	1550 1550 1550 1550 1550 1550 1550 1550	1115 1115 1115 1130	1255 1205 1205 1210 1215	1518 1510 1520 1520 1536 1536	11619 1619 1625 1630 1630	11:35 1:35 1:35 1:05 1:05 1:05
8 62 8	86 63	5 6	8 65 N	5.0	\$ to	2 6

Ī	DATA										
5	TIME	RATE	CHS	MEUIANS	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
69	1135	1200	G	-03.5	-91.2	16 18	4289	3.3050	NONE		
	1140			-92.7	06-	16 14		2.4210			
	1145			7.96-	-93.4	10 13		7.8050			
	1150				-97.2	13		18.2370			
	1155				7.66-	18		17.7920			
	1200				-93.H	٠,		14.8730			
	1205				-93.9	17		13,7330			
Ž	1146	MATE	CHS	MEDI	ž	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
70	1340	2604	٤		-98-1	¢	FRED	4.2880	NONE		
	1350			-06.2	-95.R	9 11		3.8930			
	1355			-43.A	9.46-	10 13		1.0470			
	1400			0.H3-	-99-1	œ		4.6170			
	1405			-97.8	0.46-	-		3.0880			
	3410			-47.7	-97.4	81		5.2740			
25	TIME	HATE	CHS	WEU1	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
1	1440	5604	12	4-10-	-97.7	15	FRED	3.4060	NONE		
	1445			0.80-	-00-	15 13	1	6.0070			
	1450			-97.1	-98.5			3.9780			
	1455				2.66-	19		3.9680			
	1500			-96.5	-98.0	11 14		3.9680			
	1505			-97.6	-97.4	17		2.7640			
25	TIME	MATE	CHS	MEDI	Z	MEDIAN CROSSINGS	TYPE	FRROR	TYPE	FBROR	RFMARKS
72	1525	2604	12	1.86-	7-96-	10 8	FRED	4.1130	NON		
	1535				-06-	15		4.9150			
	1540			9.90-	7.96-	21 14		2.6370			
	1550				-97.2			4.0090			
	1555				-97.4	19		3.4420			
25	TIME	HATE	CHS	7	Ž	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
7	1005	5604	54			84 57	FRED	0.2430	NONE		
	1010			-88.9	-84·4	57 40		0.3380			
	1015			-R9.4	-84·1			0.3980			
	1020			-89.0	-84.0			0.2780			
	1025			E. 80	-85.7	65 45		0.7540			
	1030			C 0	2.98	71 46		0.5680			
200	TIME	AATE	CHS	TOJN	4	POOS	TVDE	00000	1001	00000	970174
2	1055	1200	12	-89.1	-96.4	42 32	4085	6.6720	MON	2004	PERMINA
	1100			-88.A	-82·8	50 47	n	2.8910			
	1105			-80.4	-46.0	24 47		7.6450			
	1115			0.511	-84.4	65 54		4.7540			
	1126			4.64-	-84.9	•		3.8640			
	1125	į	,	6.64-	-86.7	63 73		3.5310			
2	T I	MATE	CHS	1034	ANS	CROSSI	TYPE	ERROP	TYPE	ERROR	REMARKS
75	1150	1200	9	0.7.	-85.6		6504	0.8340	NONE		
	1155			-49.5	- 96.5 - 5			1.0150			
	1500			-RK-3	-96.2			1.2440			
	1605			0.8x-	-84.9			1.0620			
	1210			4.8	-86.5	70 57		0.6320			
	1215			-84.3	-85.1	73 64		0.6300			
	1220			4.74.	-85.7	24 69		0.9010			

1300	46			Control of the contro					
	5	- MG- 3	7.48-	30	4256	10.3640	NONE		
		1 . O. Y.	-83.1			7.0330			
		-x8x-	+.EA-	81 67		7.0610			
		-43.K	-84.5	62 43		9.0550			
	CHS	Ξ	SNA	MEDIAN CROSSINGS	TYPE	FRADA	TYPE	ERROR	REMARKS
7604	12	-72.3	-72.4	34 6	FRED	0.000	NONE		
		-76.H	-69-	31 17		0.0010			
		-72.0	-70.7	40 23		2.0001			
		-72.7	-68.3	24 17		0.0001			
		-77.1	7.57-	35 24		0.0004			
		-14.4	-68.5			9.0006			
	CHS	SATION.	ANS	MEDIAN CROSSINGS	TYPE	FRROS	TYPE	FRROR	REMARKS
2604	2		-6A.2	30	-	0.0130	NONE		
			-67.4	13		0.0770			
			-67.4	17		0.020			
			-68.0			0.0140			
			-68.0	92		0.0140			
		-73-3	-70.H			0.0270			
		-72.0	-72.0	46 28		0.000			
14.	CHO	I	ANS	CHOSS	TYPE	FRACE	TYPE	FRROR	REMARKS
2404	24	-76.3	-77.0	47 25		0.000	PNON		
		-19-	-70.7			0.55			
		-19.0	-79.5			0660-0			
		-14.2	-79.5			0.0630			
		19:0	-79.1	33 34		0.1210			
			-79.6	4 3A		0.1360			
MATE	CIT	HEDE	AZS	MEDIAN CROSSINGS	TYPE	ERPOD	TYPE	FRROR	REMARKS
	12	-78.8	-79.5	40 43	FRED	0.0240	NONE		
		-77.6	-78.4	44 31		0.0160			
		-78.5	-19.6	43 49		0.0040			
		-78.6	-10-	52 54		0.0012			
WATE	CHS	Ξ	ANS	CROSS		FRROR	TYPE	ERROR	REMARKS
10	•	-84.2	-82.1		FRED	0.0003	NONE		
		2.46	2.26			0.0003			
			5.00			0.00.0			
		6.58	***			0.0230			
		9.25	2.09			0.0830			
2		2.2	2.	60		000000		0.0000000000000000000000000000000000000	
A P I	2	5	ANS	SSUda		ERROP	TYPE	ERROR	REMARKS
	•	-83.9	-81.5	56 50	FRED	0.1040	NONF		
		B. 4K-	-83-0	55 44		0.4330			
		-83.9	-82.2	41 45		0.0300			
		-84.2	-82.0	47 34		0.1380			
		-85.0	-81.3	39 40		0.0140			
		4.44-	-81.2	12 73					

## 179-6											
CHS		2	שבח ו	ANS	MEDIAN CHO	20160	1	TOWA'S	- 17	CHANIN	
CHS	*	12	T	-19.6	25	24	FREI	4.9830	NON		
CHS			4.50-	-80.2	36	35		0.1400			
CHS			3.00		37						
CHS				***				1160331			
CHS			2.11.	-10.5	3)	2		0.0160			
CHS -FF, -Bi-1 3 - 3 - 3 - 1 - 1 - 1 - 1 - 1 - 1 - 1			2012	-10-	9	2		0890			
CHS			631								
CHS -17-5 -17-5 FRED				9	,				10000		
CHS - 17.5 - 17.5 16 10 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0		2	3	Ž	2	2	-	PHROM	4	REAL REPORT	MEMBERS
CHS -72.6	*	*	-14.5	-14.3	2	1	FRED	0.000.0	NON W		
CHS -75.5 -75.5 16 10 0.0000 -75.5 -76.0 11 1 10 0.0000 -75.5 -76.0 11 1 10 0.0000 -75.5 -76.0 11 10 10 0.0000 -75.5 -76.1 11 10 0.0000 -75.5 -76.1 10 10 0.0000 -75.5 -76.1 10 10 0.0000 -75.5 -76.2 10 10 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 8 0.0000 -75.5 -76.5 -76.5 20 0.0000 -75.5 -76.5 20 0.0000 -75.5 -76.5 20 0.00000 -75.5 -76.5 20 0.00000 -75.5 -76.5 20 0.00000 -75.5 -76.5 20 0.00000000000000000000000				-72.h		Œ		0.0010			
CHS -76.0 11 0 0 0 0 0 0 0 0			-74.2	-75.5	16	10		0-040			
CHS -74.5 -74.5 18 17 00000			7 46-	-74 0	-	3					
CHS - T-5-0					4	C (0			
CHS			173.5	5.67	<u>.</u>	9 .		0.0140			
CHS -75.7			-72.A	2.01-	- E-	12		00000			
CHS			-74.2	78.7	00	2		0000			
CHS	4	37.5			3 3	30143	-		4074	0000	970
CHS						CONTE	1	TOWARD.		KOKKO	MEMBERS
TYPE TO THE TABLE TABLE TO THE TABLE TABL	40	c	-76-1	J. [9-	6	J	FRED	000000	NON		
CHS			-76.6	- NG	9	₫		8100.0			
CHS			1 36	4		,					
CHS -77-4 -77-1 17 9 0.0013 -77-4 -77-1 17 9 0.0013 -77-7 -77-5 50 0.0013 -77-7 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-7 -77-7 0.0013 -77-			0.0	0	C	2		000000			
CHS			1.47-	-1001	17	•		0.0013			
CHS			-76.9	-74.5	٢.	ď		0.00			
CHS					h (6 (0100-0			
CHS -75.8 HFDIANS 13 TPF ERROR TYPE ERROR -77.8 EPROR			1.5.	0.0	N	D		9000-0			
CHS #F01ANS MF01AN CHOSSINGS TYPE ERROR TYPF ERROR			-75.B	-77.H	25	S		400000			
CHS #EDIANS #EDIAN CHUSSINGS TYPE ERROR NONE ERROR	176	VIL	5	ANS		SSTNES	TVBE	20000	100	9000	DENABLE
CHS								-			PARMEN
CHS #EDIANS	*0*	•	2.18.	-83.	E .	•	FRFD	000000	NON		
CHS			-F2.4	-94.0	7	12		0.000			
CHS WENTANS MEDIAN CHOSSINGS TYPE ERROR -22.6 +33.4 12 10 10 10 10 10 10 10				-B 2.4	2.0	0		0000			
CHS					3 5						
CHS WEDLANS MEDIAN CRUSSINGS TYPE ERROR 12 -A2.7 -84.7 17 11 10 0000000000000000000000000000			N. 0	0.40	7	•		000000			
CHS WEDLANS 12 10 0.0000 12 -A2.6 -B3.5 12 10 0.0000 13 -A2.7 -A4.7 17 11 19 FRED 0.0000 -A2.4 -B4.2 14 19 0.0000 -A2.4 -B4.2 14 19 0.0000 -A2.5 -B4.1 12 19 0.0000 -A2.6 -B4.2 14 19 12 0.0000 -A2.7 -A4.7 17 11 11 FRED 0.0000 -A2.7 -B4.2 14 12 0.0000 -A2.7 -B5.0 19 12 0.0000 -A2.7 -B5.0 19 12 0.0000 -A2.7 -B5.0 19 12 0.0000 -A2.9 -A2.9 -A2.9 18 FRED 0.0000 -A2.9 -A2.9 -B2.0 18 18 12 0.0000 -A2.9 -B2.4 19 19 10 0.0000 -A2.9 -B2.4 10 FRED 0.00000 -A2.9 -B2.4 10 10 0.0000			-18.2	-85.0	01	0.		0.0000			
CHS WEDIANS WEDIAN CHOSSINGS TYPE ERROR TYPE TYPE TYPE TYPE ERROR TYPE ERROR TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE			9. 13.	-83.5	12	10		0.000			
CHS			4.50-	H-FH-	*	20					
CHS	31.	377	-	200		3014196	-				
LAZ-7 - R4-7	,	ה ב	7	2		CONTCO	-	CHROM	1	LKHOK	MEMARKS
CHS	904	12	-42.7	-84.7	17	7	FRED	00000	NON		
CHS			15/31	-84.2	*	0		0000			
CHS			6 40-			٠ ۵					
CHS				7 - + 0 -	יב	•		000000			
CHS			-R2.3	0.49-	7	*		0.000			
CHS			-85.0	-85.4	E .	72		00000			
CHS			-82.6	0.54-	7.	-		0.000			
CHS HEDIANS HEDIANS TYPE ERROR TYPE ERROR -31-9 -81-9 21 11 00000 -32-9 -42-2 18 B FRED 0.0000 -43-1 -81-7 12 9 0.0000 -42-9 -42-5 -81-4 12 9 0.0000 -43-1 -81-5 -81-4 18 12 0.0000 CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR -43-4 -83-0 28 10 FRED 0.0005 -43-7 -83-6 32 14 0.0056 -43-7 -83-6 32 14 0.0057			6 60	901							
CHS #ELIANS TYPE ERROR CHS #ELIANS	31	977	-	1000		21					
CHS #12.4 -81.4 -81.9 21 11 FRED 0.000 NONE	J .	6	5	PN.S	2	CONTCO	1	EHROR	I YPE	ERMOR	REMARKS
CHS	1	c	-H2.1	-82.K	21	C	FRED	000000	NON		
-42.9 -42.7 18 B 0.0000 -43.1 -81.7 12 9 0.0000 -42.5 -81.4 18 12 0.0000 -42.5 -82.4 19 10 0.0000 CHS ##UIANS #EDIAN CROSSINGS TYPE ERROR -43.4 -83.4 -83.4 58 9 0.0005 -43.7 -83.6 32 14 0.0056 -43.7 -83.6 32 14 0.0057 -43.7 -83.5 10 0.0057			3° [K -	6.18-	2	=		00000			
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		1.20-	-9 4.0	•	2					
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EATE	CIS	HEO1	ANS	HEDIAN CROSSING	SUZ	TYPE	FRROP	TYPE	ERROR	REMARKS
0017	*	-AB.0	125.1	54		6504	0.1330	NONE		
		Law.	-88.1	12 1	9		4.0700			
_		A-174-	-87.5	- 51	4		4.9100			
ď		4.64-	-80				2.1700			
		- AB.	- 404-							
		E. B.	- BB		· W		0.016.0			
		-47.5	-80				0.1150			
PATE	SH.	=	AMS	MEDIAN COOSTINGS	VUN	TVDF		1405	9000	DENABLE
ý)		87.8	23	27	The state of the s	r OK	1	2002	
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> t		200			0					
n ·		-F3.7	- F 3 - c		53					
E.		C . N.	-K2.K		S.					
S		E. 4K-	-83.7	20	•					
0		P. 2.1	T. C.		56					
N.		-83.6	-H4-0		17					
MATE	CHS	-	Z	22002	SEN	TVOF		TVDE	9090	DELLONG
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•		2.70-	10.	N (23		0.01A6			
		6.70-	-91.4	2	-		0.2580			
YA I	25	- FU	ANS	7S(C)2D	NUN	TADE	ERPOR	TYPE	EBROR	REMARKS
5604	2	- X - 1	\$ 10-	7	245	FRED	0.4040	NONE		
n		1.16-	-91.3		~		0.56.0			
0		¥.90-	-89.3		N.		0.2920			
		7.96-	-R9.2	35 5	0		0.2570			
•		-96-1	1.88.4		31		0.0370			
ıc.		-45.2	-BG-	40 2	52		0.0510			
		0.70-	-91.5	25	2		0.2490			
HATE	CHY	Ξ	SNA	MEDIAN CROSSINGS	NGS	TYPE	FRROD	TYPE	FRROR	REMARKS
5604	*	-171.6	-99.5	45	36	FRED	2.7500	LINCA		
		-162.2	-101-0		18		2,1200	•		
S		-101-3	-100.5	40	27		1.8000			
•		-101-8	-100.3		37		2.25.00			
5		-101-	-00-		27		1.8400			
			-102							
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011			0 601-				TORKS O	1	KOKK!	25411
000	D		5-201-		- (-	06.44.0	NON		
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Α.		-101-	-104.6		C		1.6300			
c		-101.9	-66-3	36 1	•		1.2600			
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2634 12 -130.3 -130.3 -130.3 -131.4 -131.4	12 - 120.3 -120.3 -120.3 -64.5 -121.4	2 3 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	100.00 100.00 100.00 100.00 100.00 100.00	24		CANSS	T V D F F Q F C	1.100 1.000 1.000	NON NON	ERROR	REMARKS
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## CHANGE CHE CHE CHE CHE CHE CHE CHE CHE CHE CH			•	1.20-		91 6	Į.	FRED	0.2900	NON		
ALTE CHS	: :				200	* :	02		0.0579			
## CHAILE CHS	4			-61.6	1000	5	<u>.</u>		0.0400			
ALTE CAS	ĭ	_			-88.5	61	27		0.0910			
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## 15	7	2.0		7.16-	-88.0	15	18		00010			
### C45 ### PLIANS ### PLIANS TYPE CAROOR TYPE TYPE CAROOR TYPE CAROOR TYPE TYPE	*			1.62-	-80.3	7	16		0.0003			
266* 2* - 1874 - 1874 30 15 FEE 01439 NONE 144.5 - 1874 - 1874 12 23 14 FEE 01439 NONE 144.5 - 1874 - 1874 12 23 14 FEE 011439	=		CHS	MEDI	Z		SEINGS	TYPE	ENROR	TYPE	FORCE	REMARKS
## 13.9 # 12.23	3		24	-87.4	-82		16	FRED	0.1410	NONE		
## 5 1 1 1 1 1 1 1 1 1	뿘			-R3.9	-83.4	12	23	3787	0.05.0			
## CHS ##	×	_		-H4.5	-83.0	21	28		0.0390			
## CHS ##	2			-92.1	-01.2	5	•		0.0140			
## CHS ##	-			-42.0	-82.4	22	27		0.0000			
## F CHS ## UINS 13 10 0.0020 201	41	16		-B19.7	-82.2	46	28		0.00.0			
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Z604 24 -04.0 -04.2 23 25 PAED 1.0570 NONE RATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR Z604 12 -01.0 -91.3 11 18 10.2440 HEDIANS HEDIAN CROSSINGS TYPE ERROR Z604 12 -04.0 -92.0 11 18 10.2440 HEDIANS HEDIAN CROSSINGS TYPE ERROR Z604 12 -04.0 -92.0 11 10.000 RATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR Z604 12 -04.0 -92.0 10 0.0000 RATE CHS HEDIAN CROSSINGS TYPE ERROR Z604 12 -04.0 -92.0 10 0.0000 HEDIAN CROSSINGS TYPE ERROR Z604 12 -04.0 -92.0 10 0.0000 Z606 12 -04.0 -92.0 10 0.0000 Z607 12 -04.0 -92.0 10 0.0000 Z607 12 -03.2 -93.0 10 0.0000 Z608 12 -03.2 -93.0 10 0.0000 Z609 13 -03.2 -93.0 10 0.0000 Z609 14 -05.0 -93.0 10 0.0000 Z609 15 -03.0 -93.0 10 0.0000 Z609 16 -03.0 -93.0 10 0.0000 Z609 17 -03	¥		CHS	MEDI	Z	MEDIAN CROS	SSINGS	TYPF	France	TVDE	FDROD	DEMADES
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Z604 12 -91.6 19 20 FRED 0.2100 NONE COST 0 0.270	۳.		CHS	MEDI	¥	Z	SSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS
AATE CHS	Z 4		12	-01-0	8.16	<u>•</u>	50	FRED	0.2100	NONE		
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HATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE CASON HATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	₹.	_		-04.1	2.96-	12	19		0.5440			
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HATE CHS HELIANS HERIAN CROSSINGS TYPE ERROR 2604 12 -94.0 -995.9 12 FPED 0.1200 -94.5 -93.9 20 16 0.2160 -95.7 -99.4 37 32 0.6100 -95.7 -99.4 37 32 0.6100 -97.9 23 1.0400 RATE CHS HEDIAN CROSSINGS TYPE ERROR FATE CHS HEDIAN CROSSINGS TYPE ERROR -97.9 23 1.0400 -97.9 23 1.0400 -97.9 29 23 1.0400 -97.9 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 29 29 29 10 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.9 20 20 20 0.0000 -97.1 -97.1 20 20 20 20 20 20 20 20 20 20 20 20 20	ĭ			4.64-	-91.3		18		0.2300			
RATE CHS HELIANS HELIAN CROSSINGS TYPE ERROR TYPE ERROR 2604 12 -04.9 -95.9 9 12 FPED 0.1500 NONE -02.8 -93.9 20 16 0.2460 -04.5 -93.9 20 16 0.2160 -04.5 -93.9 20 16 0.2160 -04.5 -93.9 20 16 0.2160 -04.5 -93.9 20 23 1.0400 RATE CHS HELIANS HEDIAN CROSSINGS TYPE ERROR -03.2 -93.4 18 19 0.076 -03.2 -93.4 18 19 0.076 -03.2 -93.4 18 19 0.0550 -03.2 -93.4 16 0.0550 -03.2 -93.4 16 10 0.0550 -03.2 -93.4 16 0.0550 -03.2 -93.4 16 16 0.0550	4,	10		E. DHI	-HO.7	17	(F)		0.2440			
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HATE CHS HEDIAN CROSSINGS TYPE ERROR 12 10 0.2560 0	Z		12	6.40-	-95.0	•	12	FRED	0.1500	MON		
HATE CHS HEDIAN CROSSINGS TYPE ERROR 12 18 0.2560 0.7954 0.93.9 20 16 0.2560 0.1000 0.2560 0.1000 0.2560 0.1000 0.2560 0.1000 0.2560 0.2560 0.2560 0.2560 0.0560 0.0560 0.2560 0.0560 0.2560 0.2560 0.0560 0.2560 0.	X.			8-20-	1-65.	£	19		0.2460			
HATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1937 37 32 0.6100	X	_		5.46-	-93.4	20	9.		0.2140			
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE EMROR TYPE ERROR 1.0400 NONE CAST 1	*			-45.7	-63.6	12	30		001.0			
HATE CHS HEDIAN CRCSSINGS TYPE ENROR TYPE ERROR 10400 12 -97.9 23 1.0400 10400	I			-08.7	-99.4	37	35		0.6100			
RATE CHS MEDIANS HEDIAN CRCSSINGS TYPE ENROR TYPE ERROR 12 -92.9 10 FRED 0.0240 NONE 12 -93.4 18 19 FRED 0.0746 -93.7 -95.2 9 14 0.2500 -92.0 14 0.2500 -92.1 -93.4 38 18 0.0550 -92.1 -92.3 20 20 0.2500 -92.1 -91.5 14 16 0.2920	7			-4B.9	-98.9	9	-		1.5600			
RATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 12 -92.9 10 FRED 0.0260 NONE FRED 10 FRED 0.0260 NONE FRED 19 0.0260 NONE FRED	3	•		-47.1	-97.9	2	60		1.0400			
7604 12 -93.2 -93.4 18 19 0.0260 NONE -91.7 -92.1 15 11 0.0776 0.0776 -93.7 -95.2 9 14 0.0550 0.0550 -92.3 20 20 0.2970 0.2970 -91.1 -91.8 14 16 0.2970	*		CHS	2	ANS		STAGS	TYPE	FUDUO	TVDE	00000	DENABLE
-03.2 -93.4 18 19 0.0460 -91.7 -92.1 15 11 0.0476 -93.7 -94.2 9 14 0.2500 -93.4 39 18 0.0550 -92.1 -92.3 20 20 0.2970 -91.8 14 16	_		12	١.	0		10	1000	0 03C0	3.00	5 5 7	A CLEAR
-91.7 -92.1 15 11 -93.7 -95.2 9 14 -92.6 -93.4 38 18 -92.1 -92.3 20 20 -91.8 14 16			ļ	C. FO.	4.50-	•	2 -	L	00000	-		
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-42.6 -93.4 38 18 -92.1 -92.3 20 20 -93.1 -91.8 14 16	5			-63.1	2-56-	•	<u>.</u>		0.2500			
-92.1 -92.3 20 20 -91.1 -91.8 14 16				4.20-	4.66-	3.9	18		0.0550			
1-0).1 -91.8 14 16	٠			-92.1	-92.3	20	20		0.1060			
	3			-61-	-91.B	*	16		0.2920			

1	DATA								7.			
5	TIME	HATE	CHS	MEU1	HEUT ANS	MEDIAN CI	CROSSINGS	TYPE	FRROP	TYPE	FRROR	REMARKS
119	1025	5604	2	-98.7	86-		35	FRED	5.3800	NON		
	1030			2.66-	-98.0	34	33		6.3100			
	1035			5-14-	7.96-	37	30		0006.4			
	1040			E-16-	-94.3	92	63		4.4300			
	1045			4.00-	-98.5	69	•		1.9600			
	1050			-04.1	1-96-	25	23		1.4900			
	1000		97.5	6.86-	6.86	N	24	!	2.4400		•	
200	1126	2606	SE S	10.4	SNA	MEDIAN C	CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
	1130	1007	•	6.00	104	000	n e	-	1	NON		
	1135			446.5	10.1	2	. e		0.250			
	1140			-03.7	9.26-	25	8		0.2500			
	1145			-05.6	+.26-	23	5-		0.4300			
	1150			-64.0	-91.3	1	æ_		0.1940			
	1155			0.60-	-96-	4	54		0.6710			
Ş	116	KATE	CHS	MEC.	ANS	MFDIAN C	AN CROSSINGS	TYPE	ERROD	TYPE	ERROR	REMARKS
121	250	2400	12	-91.3	-87.3	23	16	6904	11.1500	NON		
	455				-83.1	60	œ		7.1300			
	1000			1010	-89.5	1 *	_		13.3100			
	5001			-00-5	-87.0	>	E.		10.5600			
	1010			- PB - 3	-86.7	25	13		4.9400			
	1015			-88.6	20.	21	9		5.5100			
	1020			-41.6	-80.3	Ň	12		9.5100			
2	T I I	4	CHS	MFU	UIANS		CRUSSINGS	TYPE	EBROS	TYPE	ERROR	MEMARKS
721	0+07	2400	12	2000	-88-	51	18	65C4	14.9600	NON F		
	5001			4.20-	-60-	21	20		11.3600			
	1050			-65.3	-05-	000	2		20.8600			
	1100			0.40		m 0	6 T		13.7100			
	1105			2.7.0	4 60-				2000			
	1110			0.70-	-63-6	3.6	7 5		23.7900			
Ş	TIME	HATE	CHS	MED	ANS	YENTAN C	CROSSINGS	TYPE	FRRDS	TYPE	FDROD	DEMADES
123	1150	2400	12	-97.6	-95.5	(6)	24	4366	23.7800	NON		
	1155			-07.0	-95.1	7.2	36		27.1300			
	1206				F. 69-	1	13		26.9500	٠		
	5021			-66-	-96.5	42	8		24.0300			
	1216			* * * * * * * * * * * * * * * * * * * *	***	6 G	5		17.7000			
	40.00			100	3		21		9.1800			
4	3771	1	310	2. I 6.	-88-7	90	26 13		9.4200			
124	345	1000		2 1 7	7.040	27	CONT.CCO.	100	CHACK C	1	EMMOR	REMARKS
4	97.		j	7 - 7 - 1		5 2	٥.	-	6.00	MONE		
	1350			7.52.1	7.02	36	9 7		0.9740			
	1400				E - C - C - C - C - C - C - C - C - C -	C &	, c		0000			
	1405			5	-78.0	23	2		0.0780			
	1419			0.7x-	-81-8) (F)	. 6		0.1730			
	1415			4-14-	-63-7	3) '		0.2980			
					1	r	•					

RELABRES	REMARKS	REMARKS	REMARKS	RELATER
R R R O R	ER OR	E R O R	ERROR S	ER ROR
NOV NOV	2 4 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TYPE	NOY NOY NO	NONE
1.0970 1.3800 1.5500 1.0500	6.5000 0.5000 0.7370 1.1200	0.52400 0.1840 0.1840 1.52440	0.0010 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	0.00150 0.00150 0.0037 0.0174 0.0163
TYPE	FRED	7 4 9 F.	TYPE TYPE FAED	FHED
MEDIAN CROSSINGS 29 28 27 27 31 29 29 21 28 22 26 19	CROSSI 3 3 4 8 8	CROSS	MEDIAN CROSSINGS 44 29 44 29 68 44 50 46 50 46 48 53 63 39 44 34 31 27 39 20 26 19 25 19	SSOS
6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		**************************************		
2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	W	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
\$ \$	0 4 %	CHS	2	S & S
1 2 4 2 5 6 0 4 5 6 0	2604	2604 2604	25 0 4 5 0 4	2504 2504
1455 1455 1500 1500 1510 1510	1555 1555 1555 1655 1655	110 160 160 160 160 160 160 160	10000000000000000000000000000000000000	11140 11150 11150
125 125	126 126	127	128 128 128 129 129 129 129 129 129 129 129 129 129	300 130 mg/s

MEDIANS	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
-82.1	-85.4	33 43	NONE		NONE		
-P0.5	-82.4						
	-83.5	32 38					
1	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
-78.6	-61.4		NONE		NONE		
-B0.4	-83.3						
-H2.4	-84.2						
-A2.5	-84.1	,					
-H3.1	-82.4						
-82.0	-81.7	21 30					
-F2.0	-82.2	35 26		35		8	
MEDIANS		CROSS	TYPE	ERROR	TYPE	ERROR	REMARKS
-61.2	-77.3	57 30	MONE		NONE		
0.0	-78.4						
-81.2	-77.9	33 35					
-82.0	-80.2						
-79.6	-76.6	29 28					
-81.1	-77.8						
-A0.4	-77-1	38					
10	ANS	CROSS	TYPE	FRROP	TYPE	FDROD	BEWARKS
-81.1	-76.8	51	NONE		NONE		
-80.8	-76.0						
-A3.2	-77.8						
-A1.2	-78.2						
PH1.9	77-						
-A0.8	2.77-		`				
-79.8	-16.7	90					
H	ANS	CROSSI	TYPE	ERROR	TYPE	ERROR	REMARKS
0.64	-26-		NONE		NONE		
4.64	0.06-	20					
010	6.89-						
-H7.3	1-16-	N					
-40.0	0.06-	10					
N - SH -	-89.7						
	C						
7		2	1	EKKOK	341	ERMOR	REMARKS
- 25	1.68-	21 01	NONE		NON		
-44	7.89-	201					
4.64-	+.19-	14 15					
-46.6	-84.9	14 12					
-88.4	-85.6	10 11					
-88.5	-85.3						
- 1	-87.5						
5	ANS	MFDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
-H2.9	-90-1	6 0	FRED	0.0000	NON		
-84.3	-81.3	17 16		0.0000			
-78.5	-77.5			0.0000			
-R1.3	-78.7	11 8		0.0000			
-A1.1	-78.7	13 9		0.000			
-40-1	-10.8	22 10		0.0200			
277-	-76-6	46					

Ş	TIME	HATE	CHS	MED	MEUIANS	MEDIAN CROSSINGS	TYPE	FRROR	TYPE		RFWARKS
136	1555	2604	34	5.07	F . 18-	23	2000	0000	PACA		
	1600			-77-5	-78.9	2.5	1	2000			
	1605			7.67-	-80.5			0.0282			
	1610			-77.2	-79-1	4		0.0200			
	1615			-78.6	-81.5	16		0.0248			
	1620			-76.R	-77.5	13 17		0.0003			
	1625	1		-16.7	-77.0	13 9		0.0027			
2	TI.	PATE	SHO	MED	TANS	MEDIAN CROSSINGS	TYPE	FRROR	TYPE	FRROR	REMARKS
130	1655	1092	24	-72.	-81.0	14 0	FRED	0.0240	NONE		
	1700			-80.3	-81.6			0.0540			
۰	50/1			-43.0	-84-1	16 13		0.0290			
	07/1			0.0	C-19-			0.0440			
	17.15			E-11-	9.64			0.0242			
	0271			5.18-	7.68	24 10		0.0549			
200	1145	MATE	S T	1067	1.68-	904193000 P4103W	6	1820.0	62	900	-
	1606	2604	2	100		CONTROLL NATURE	-	CHACK	1	EKNOK	MEMPHEN .
	1414	1003	•		- VO	٠.	PWED	0002-0	NON		100
	1416			5.09-	5 - 19			0680-0			
	6101			S . C . C	6.0			01210			
	4301				6.19-	(2) (2)		2.4800			
	1625			-85.4	-86.1	20 10		0.6200			
	1630			-82.2	-82.2			0.1900			
2	1020	200	4	1.08-	-82.4	42 6I		0.5100			
5	T.	NA IE	2		MEDIANS	MEDIAN CROSSINGS	TVPE	ERROR	TYPE	ERROR	REMARKS
741	1245	1092	*	-75.4	-72.4	21 15	FRED	0.0340	NONE		L00P
	1256			1.8.1		<u>c</u>		0.1310			
	1200			7.5.6		0		0.0210			
	3000				7.50	13 10		0.100			
	2007			4.01	-13.4	21 41		0.0350			
	1777			1.5.1		P) (9060-0			
1	1313	DATE	370	-75.3	H			0.0250			
146	100	2604	5		T OO T	CKONS	145	FROR	344	ERMOR	HEMARKS
	211		4	67.0	6.00) () () () () () () () () () (C LANGE	00000	MONE		1001
	1115			97.0	476-			0.6010			
	1120			-63.A	-98.5			0.8140			
	1125			2.85-	-98.3	15		0.4640			
	1130			A-10-	-97.0	~~		0.3330			
	1135			-169-1	-100-1			0.6210			
Ş	114	MATE	CHS	MED	Y	CHUSS	TYPE	EPROP	TYPE	EAROR	REMARKS
146	1205	₹097	•	-141.2	-101-3		FRED	0.69.0	NONE)	L00P
	1210			-100.4	-100.4	16 22		0.3560			
	1215			-101-	-102-0			0.8150			
	1220			-106.3	7.26	17 21		0.5880			
	1225			-08 · H	-97.0			0.4830			
	1230			B. L?-	-98 · i	10 22		0.3790			
	1235			-66-3	-98.5	15 19		0.5950			

CHS NEUTANS 122 122 124 124 124 124 124 124 124 124												
13.05 26.04 12 206.27 24.05 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 13.15 14.15	Z	1 IME	PATE	C:4S	MEUT	ANS	MEDIAN CROSSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS
1310	2	1305	2604	12	96-	-94.0	16 22	FRED	0.1100	MONE		
1315		1310			-04.5	-95.0	13 22		0.0740			
320		1315			-03.H	-95.0	16 16		0.1140			
1325		1320			E. 47-	-94.6	14		0.1270			
1330		1325			10401	-65-1	•		0-1100			
1335 1416 240 240 240 240 240 240 240 240 240 240		1330			-44.6	-BR. G			0.0340			
TIME HATE CHS		1335			8-74-	-87.0	_		0.0230			
1410 250+ 24 -47.4 -47.5 15 10 1410 1420	z	TIME	HATE	CHS	MEDI	ANS		TYPE	ERROR	TYPE	ERROR	REMARKS
1410 1415 1425 1426 1435 1435 1440 1427 1435 1435 1435 1435 1435 1435 1435 1435		1405	2504	54	-87.4	-87.5	15 10	FRED	0.1030	NONE		
1415 1415 1420 1420 1420 1420 1420 1421 1431 1431 1431 1420 1420 1420 1420 1420 1420 1420 142		1410			-7H.0	-78.5	13 3		0.0340			
1420 1425 1436 1435 1435 1435 1435 1436 1436 1436 1436 1437 1437 1437 1437 1437 1437 1437 1451 1515 1510 1510 1510 1510 1510 1510		1415			4.16-	-80.1	13 13		0.0450			
1425 1425 1435 1435 1435 1435 1435 1435 1435 143		1420			-A3.3	-80.7			0.0550			
1435 1435 1435 1441 1441 1441 1441 1441		1425			-R6.9	-86.2	21 12		0.0850			
1435		1430			-43.5	-83.5	20		0.0500			
TIME HATE CHS HEDIANS HEDIAN CROSSINGS 1505 260 22 11 1510 1520		1435			-H6.3	-86.4	_		0.0390			
1505 2604 24 -85.5 -87.0 22 11 1510	7	TIME	MATE	CHS	MEDI	Z	AN CROSSING	TYPE	ERROR	TYPE	ERROR	REMARKS
1510 1515 1516 1515 1516 1517 1518 1518 1519 1519 1519 1519 1519 1519	_	1505	2604	\$ 2	-A5.5	-67.0	22 11	FRED	0.0500	NON		
1515		1510			-H7.2	-84.5			0.1170			
1520 1525 1535 1536 1546 1546 1546 1547 1546 1546 1546 1547 1547 1547 1547 1548 1559 1559 1559 1559 1559 1559 1559 155		1515			- 96.F	-83.4	14 12		0.0700			
1525 1530 1540 1540 1551 1552 1545 1546 1546 1546 1546 1547 1547 1547 1547 1547 1547 1547 1547		1520			F.99.3	7.99-	10		0.1410			
1530		1525			-92.5	-00-	11		0.1100			
TIME MATE CHS		1530			-65.5	-89.5			0.3070			
1235 2604 6 -90.0 -90.6 15 20 1246 -93.7 -93.7 19 27 1256 -93.6 -93.8 -93.5 26 1300 -90.7 -90.2 27 1300 -90.7 -90.2 26 1310 -90.7 -90.7 20 1310 -90.7 -90.7 20 1310 -90.7 -90.7 20 1310 -90.7 -90.7 20 1310 -90.7 -90.7 20 1310 -90.7 -90.7 20 1310 -90.7 -90.7 20 1310 -90.8 -90.0 20 1310 -90.0 20 1310 -90.0 20 1310 -90.0 20 1310 -90.0 20 1310 -90.0 20 1310 -90.0 20 131	,	TIME	KATE	CHS	HEUI	ANS	AN CROSSING	TYPE	FRROR	TYPE	FDROB	PFWARKS
1245 1245 1255 1256 1305 1305 1305 1305 1305 1305 1305 1305	_	1235	2604	•	0.00-	9006-	15 20	FRED	0.0770	HON		
1255 1256 1257 1258 1305 1305 1305 1305 1305 1305 1305 1305		1240			-43.2	1.66-			0.0610			
1255 1255 1255 1255 1255 1255 1255 1255		1245			-03.0	-93.3			0.0330			
1255 1255 1300 1300 1300 1300 1300 1300 1310 131		1250			-03.R	-93.5			0.0670			
1300 1300 1300 1300 1300 1300 1300 1300		1255			-91.5	-91.2			0.0149			
1305 1305 1316 1317 1318 1318 1318 1318 1318 1318 1318		1300			-89.0	B. 68-			0.0260			
1325 260+ 12 -90-7 20 26 1330 1340 1345 1345 1345 1345 1346 1345 1346 1345 1346 1346 1346 1346 1347 1346 1347 1347 1348 1348 1348 1349 1349 1349 1349 1349 1349 1349 1349		1001		,	-01.0	-90.5	23 24		0.00%			
1350		1	A A	SE.	MEDI	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REHARKS
1335 1335 1346 1346 1346 1346 1356 1347 1357 1348 1358 1359 1349 1359 1359 1359 1359 1359 1359 1359 135		6761	5007	21	2-00-	-00-		FRED	0.1610	NONE		
1355 1355 1356 1356 1357 1358 1359 1359 1359 1359 1359 1359 1359 1359		355			5.26	6.00			0.1610			
1345 1345 1345 1345 1345 1356 1357 1415 1415 1415 1415 1415 1415 1415 14		1340			2.26	200			0.0810			
1350 1350 1350 1350 1350 1350 1350 1415 1415 1415 1420 1420 1420 1420 1420 1420 1420 1420		1346			7 00				0.2250			
1355 1135 1135 1135 1135 1135 1135 1135		136.0			0.00	5.16			0.0010			
TIME RATE CHS MEDIANS MEDIAN CROSSINGS 1425		1 356			7.00	8.00			0.0000			
1415 2604 24 -96.8 -87.3 35 38 142 1425 1425 1425 1430 1435 1430 1435 1435 1445 1445 1445 1445 1445 1445		TAR	RATE	CHS	TOSM	2	MEDIAN COOSSINGS	1000	0.00	-	9000	-
1420 1425 1430 1430 1435 1440		1415	2604	26	1	-87	35		400		LOVE TO LEGIS	MEMANAS
1425 1430 1430 1435 1445 1445 1445 1445 1445 1445 1445 1445 1445 1445 1445 1445 1445 146.6 146.7		1420		•	4-74-	-88.6			0.220			
1430 1435 1446 1446 1446 1446 1446 1446 1447 1446 1446		1425			-H-1	-85.5			0.2000			
1435 1440 1440 1445 1446 1445 1445 1445 1445 1445 1445		1430			-97.5	-84.7			0.4000			
1440 1445 1445 1445 1445 1445 1445 1445		1435			-83.S	-84.4			0.1070			
1445 ISOS CHS MEDIANS MEDIAN CRASSINGS 1505 2604 24 -44.8 -85.8 36 26 1510 -46.7 -86.9 31 28 1515 -84.5 -86.1 38 30 1520 -85.0 -85.0 24.5 28 1521 -85.0 -85.0 24.5 28		1440			-87.1	-87.4			0.1310			
TIME MATE CHS MEDIANS MEDIAN CROSSINGS 1505 2604 24 -84.8 -85.8 36 26 1510 -86.7 -86.9 31 28 1515 -86.1 38 30 1520 -85.0 -85.0 -85.0 25 22 1530 -86.4 -86.1 29 18		1445			-86.6	-87.1			0.1100			
1505 2604 24 -44.8 -85.8 36 26 1510 1510 -16.7 -86.9 31 28 1515 -16.5 -86.1 38 30 1520 -15.2 -86.1 31 29 1520 -85.0 -85.0 -85.0 24 22 1530	-	114	MATE	CHS	IG3W	Z	AN CROSSING	TYPE	ERROR	TYPE	ERROR	REMARKS
-86.7 -86.9 31 28 -84.5 -86.1 38 30 -83.9 -82.1 31 29 -85.6 24 22	_	1505	2604	\$	-44.8	-85.A		FRED	0.2100	NONE		
-84.5 -86.1 36 -83.9 -82.1 31 -86.0 -85.6 24 -86.1 29		1510			1.98-	-84.9			0.1900	1		
-83.9 -82.1 31 -86.0 -85.6 24 -86.4 -86.1 29		1515			-84.5	-86.1			0.1400			
-70.0 -85.6 24 -116.4 -86.1 29		1520			-R3.9	-82.1			0.1180			
-H6.4 -B6.1 29		1525			-80.0	-85.6	•		0.1060			
		1530			-E6.4	-84.1	•		0.2040			
-81.3 -81.0		1535			-81.3	-81.0	16		0.0800			

PPM DATA

REMARKS	900							PFWARKS	900							REMARKS	000							REMARKS	900	,					
ERROR								FPROP								FBROR								FRROR							
TYPE	MONE							TYPE	NONE							TYPE	NON							TYPE	NON	1					
ERROR	0.0070	0.0200	0.0150	0.0200	0.0048	0.0144	0.0012	ERROR	0.1570	0.0214	0.0530	0.0640	0.0230	0.0370	0.0270	FRROR	0.1970	0.0820	0.01	0.0830	0.0600	0.1240	0.0770	ERROR	0.1776	0.1040	0.0480	0.0580	0.0410	0.0570	0.3850
TYPE	FRED							TYPE	FRED							TYPE	FRED							TYPE	FRED						
MENIAN CROSSINGS	29 28	34 38	33 31	32 37	32 24	35 42	75 27	N CROSSINGS	18 5	13 7	14 13	11 9	17 10	19 14	18	MFDIAN CROSSINGS	•	13 6	11 13	12 6	10 8	• • • • • • • • • • • • • • • • • • • •	S.	MEDIAN CROSSINGS	10 11	9 +1	9	13 8	6 91	15 9	6 +1
MENIA								MEDIAN								MFDIA								MEDIA							
MEDIANS	6.06-	-88.1	-89.3	-88.1	-86.5	-86.3	-82.5	Z	-78.4	-77-2	-79.5	-81.1	-78.4	-78.9	-7A.+	Z	6.19-	-81.3	-80.5	-96.1	-82.0	-83.3	-85.0	Z	-87.4	-80.7	-77.	-82.1	-85.9	-65.1	-84.5
HED	-49.1	-84.0	-RB-2	-AB.0	-87.0	-A6.9	-85.0	MEUI	-HO.5	-81.3	-83.5	-H5.4	-80.7	-A3.4	-84.3	ME01	-H6.0	-A5.6	-A4.4	-A8.8	-H6.4	-A5.1	-88.2	MEUI	0.06-	-83.5	-82.0	-84.1	-85.7	-A4.9	-85.0
CHS	12							CHS	54							CHS	2							CHS	\$2						
HATE	2604							HATE	2604							MATE	2604							KATE	2604						
TIME	1615	1620	1625	1630	1635	1640	1645	TIME	1355	1400	1405	1410	1415	1420	1425	TIME	1445	1450	1455	1500	1505	1510	1515	114	1535	1540	1545	1550	1555	1600	1605
5	154							S	155							Ş	156							Ş	157						

HEDIAN CROSSI 54 53 54 64 55 55 10 10 10 10 10 10 10 10 10 10		
CHS HEDTANS HEDTAN CROSSINGS TYPE 2 - AR.5 - 91.5 54 21 - AR.5 - 92.6 48 28 - 40.1 - 93.7 49 28 - 40.2 - 93.7 49 28 - 40.2 - 93.7 49 28 - 40.5 - 93.7 49 28 - 40.5 - 93.7 49 28 - 40.5 - 93.7 49 28 - 40.5 - 90.9 5 24 -		
CHS MEDIANS HEDIAN CROSSINGS 24 -AR.5 -92.5 53 31 -84.9 -92.6 48 28 -93.1 -93.1 56 31 -84.9 -93.4 55 38 -84.5 -93.2 55 38 -84.5 -93.2 55 38 -84.5 -93.2 55 38 -84.5 -84.5 55 38 -85.2 -85.2 52 -85.3 -85.2 52 -85.3 -85.3 52 -85.3 52	0.3690 0.1730 0.20108 0.1740	.1.
CHS		
CHS	25 13 16 10 23 7 14 9	-
CHS	199.7	
	10011 10011 10011 10011	•
44 44 4 44 44 44 44 44 44 44 44 44 44 4		
156 1510 1515 1510 1515 1510 1515 1510 1515 1510 1515 1510 1515 1510 1515 1510 1515 1510 1515 1510 1515 1510 15	1105 1110 1115 1115	,

2	TIME	HATE	CHS	SNTIGH	SNA	MEDIAN CROSSINGS	SSINGS	TYPE	FRROA	TYPE	ERROR	REMARKS
101	1250	2400	54	-03.2	-95.5	92	•	FRED	0.6930	NONE		
	1255			-43.5	-95.5	E	10		1.2500			
	1300			6.40-	5.96-	3	0.		1.6000			
	1305			2050-	-96.5	32	11		1.4300			
	1310			6.40-	9.96-	82	15		2.1400			
	1315			-93.7	0-96-	20	12		1.0800			
	1320			4.46-	0.46-	12	11		1.3400			
2	114E	HATE	CHS	MEUI	SHY	MEDIAN CROSSING	SSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS
165	1350	2+00	54	2.46-	-93.0	52	10	FAED	0.9240	NONE		
	1355			-43.6	-92.8	\$ 2	1		0.5750			
	1400			-03.0	-93.7	1.9	16		0-1190			
	1405			-63.0	-92.5	22	1.9		0.2630			
	1410			-06.0	7.40-	ž	=		0000			
	1415			0.40-	-05	0	. <u>.</u>		0.305.0			
	1420			A 40-	- 40-							
252	11	MATE	CHO	HELL	Z	MEDIAN CROSSING	SENISSO	TVDE	F0000	TVDE		DELLOR
166	1520	2400	es.	-89.0	1	30	3.3	S IN LES	0.2220	1000		
	15.25			00-	5.00	36				1		
	1530			P. 08-	X . 04	2 2	76		0640			
	1535			900	9	**	200					
	1640			4 0 4	000	? ?	3 6		170.0			
	448			***	7.00	5 6	7		0.1410			
7	1040	27.40	977	4.681	-69-0	25	212					
		MAIL	2	MEDIAN	PNS	MEDIAN CHOSSING	SONTOS	LADE	ERROR	TYPE	ERROR	REMARKS
101	1235			4.90-	-103.3	15		NONE		NONE		
	0421			-96-3	-103.7	35	_					
	1245			6.96-	-103.5	* 2	12					
	1250			-98.0	-104.2	58	13					
	1255			-47.5	-103.2	35	*					
	1300			+.96-	-101-6	23	15					
	1305			-04.1	-102.9	23	12					
5	TIME	MATE	CHS	MED TA	ANS	MEDIAN CROSSING	OSSINGS	TYPE	FREDR	TYPE	FPROP	RFWARKS
166	1335			1-20-	-96-7	23	Œ	NONE		NON		
	1340			4.40-		1.8						
	1350			-03.4		58						
	1355			-94.5	-98.5	27	13					
	1400			4-26-	-98.2	28	15					
	504		9	2.46-	- 68 · ·	35	13			į	1	
	E 1	X Y	S	MEDIANS	ANS	MEDIAN CROSSINGS	SSINGS	TYPE	ERROR	TYPE	ERROR	REHARKS
707	0001			E .	1-06-	35	17	NONE		NONE		
	1555			5.88-	-91.0	*	2					
	1600			-89.0	-92.0	9	S.					
	1605			-60-1	-95.6	38	25					
	1619			-89.9	8.06-	04	34					
	1615			-89.4	-91.4	33	23					
	1620			-A9.1	-90.3	31	16					
2	TIME	MATE	CHS	ME ID I	Z	MEDIAN CROSSING	SSINGS	TYPE	FRROR	TYPE	ERROR	REMARKS
170	1650	2400	54	-89.2	-91.0	22	15	FRED	0.0515	NONE		
	1655			+.06-	0.06-	22	23		0.2850			
	1700			-43.5	-84.3	17	ç		0.0076			
	1705			-45.A	-87.3	36	92		0.2630			
	1710			-85.5	-86.6	33	23		0.1050			

REILARKS	REMARKS REMARKS	REH ARKS	REHARKS REC PAKS
FROR	EARO OR	n n n n n n n n n n n n n n n n n n n	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
TYPE NONE	NOVE NOVE	NOVE OVE	14 PE NON P NON P NON P
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1√PE FRED	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	779E 779 779 7860	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
CROSSI	MEDIAN CROSSINGS 18 9 18 16 17 15 19 15 19 15 29 26 28 27 28 27 28 27 25 25 26 26 25 25	36 CROSSING 227 19 22 19 22 19 23 20 20 23 20 20 24 CROSSING 26 17 24 13 31 24 25 31 22 13	CROSS SROSS
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111111 1111111111111111111111111111111	# # # # # # # # # # # # # # # # # # #		# 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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2400	HATE 2400 RATE 2400	244 24 400 24 40	7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
73 1955 173 1955 2000 2000 2000 2000 2000 2000 2000 2	70 2005 174 2105 2110 2110 176 1120 1130 1146	179 179 170 170 100 100 100 100 100 100 100 100	RUN 11155 11550 11550 1250 1250 1250 1250 1350 1350 1350 1350

28 12 7 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	CROSSINGS TYPE ERROR TYPE CROSSINGS TYPE ERROR TYPE ERR
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11 0.0026 NOME 11 10.0003 11 0.0003 11 0.00046 11 0.0003 12 12 0.0017 12 12 0.0017 13 17 0.0001 21 18 0.0001 22 14 0.0001 23 14 0.0001 24 18 18 0.0002 34 18 0.0002 43 33 22 FRED 0.0002 44 31 32 0.0002 44 31 32 0.0002 44 31 31 FRED 1.4900 35 26 0.2800 36 26 0.2800 37 27 0.0002 38 20 0.0002 44 38 FRED 0.4640 NOME ERROR 27 0.0002 38 20 0.0002 39 28 0.0002 30 20 0.0002 31 22 0.0003 32 21 22 0.0003 33 21 22 0.0003 34 28 0.0002 35 20 0.0003 36 20 0.0003 37 21 22 0.0003 38 21 22 0.0003 39 22 0.0003 30 0.0003	16 FRED 0.0226 NONE 11 0.0003 11 0.0003 11 1 0.0003 12 12 0.0001 23 1 17 0.0001 25 20 0.0010 25 20 0.0010 27 23 FRED 0.0001 29 19 0.0023 34 27 0.0004 43 33 0.0004 43 33 0.0004 44 32 6 0.0004 44 32 6 0.0004 45 38 77PE ERROR TYPE 28 18 0.0002 40 27 0.0003 41 32 6 0.0002 42 28 17PE ERROR TYPE 29 29 0.0002 41 32 FRED 1.2300 42 28 1.4000 39 28 1.4000 39 28 1.4000 30 2.20 0.0002 42 28 20 0.0002 43 32 20 0.0002 44 38 46 16 0.0002 45 20 0.0002 52 20 0.0003 52 20 0.0003 52 20 0.0003 52 20 0.0003 52 20 0.0003
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14 0.0136 15 0.00046 18 0.00046 19 0.0003 11 17 0.00010 21 2 2 0.0010 22 2 0.0010 23 17 0.00021 25 14 0.00025 29 19 0.00025 34 22 FRED 0.0004 34 18 0.00024 41 32 0.0002 44 33 FRED 1.2300 AN CROSSINGS TYPE ERROR TYPE ERROR 24 13 FRED 1.2300 AN CROSSINGS TYPE ERROR TYPE ERROR 24 13 FRED 1.2300 AN CROSSINGS TYPE ERROR TYPE ERROR 25 26 0.3220 36 26 0.3220 37 21 22 FRED 0.4640 38 20 0.4640 39 22 0.4640 39 22 0.4640 30 23 21 23 FRED 0.4640 30 22 0.4640 31 23 FRED 0.4640 32 22 17 0.4980 32 21 23 FRED 0.4640	14 0.0136 18 10.0003 18 0.00003 18 0.00003 27 23 FRED 0.00001 28 14 0.0002 29 19 0.0002 29 19 0.0002 29 19 0.0002 34 18 0.0002 41 32 27 0.0002 41 32 27 0.0002 41 32 28 FRED 0.0002 41 32 28 1.4000 39 28 1.4000 30 2
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32 26 0.2870 32 26 0.3220 44 38 3.1300 42 25 6.5200 48 28 6.5200 48 28 6.1990 27 22 6.1990 27 21 0.0351 22 17 0.4980 38 16 0.0022	32 26 0.3220 33 21 3.1300 44 38 3.4300 42 25 6.5200 43 21 2.3400 44 38 4.4300 45 25 6.5200 4660 NONE 47 22 27 21 0.4980 48 30 30 33 50 50 33 50 50 50 50 50 50 50 50 50 50 50 50 50
33 21 3300 44 38 3.6300 42 25 6.5200 AN CROSSINGS TYPE ERROR 31 23 FRED 0.4660 NONE 27 22 0.1990 27 21 0.0351 22 17 0.4980 33 16 0.0022	33 21 3.1300 44 38 3.6300 42 25 6.5200 AN CROSSINGS TYPE ERROQ TYPE 31 23 FRED 0.4640 NONE 27 22 0.0035 22 17 0.4980
44 38 3.6.5200 42 25 6.5200 TYPE ERROR 31 23 FRED 0.4660 NONE 27 22 0.1990 27 21 0.0351 27 21 0.0351 27 21 0.0351 27 21 0.0351	44 38 3.6500 42 25 6.5200 TYPE ERROR TYPE 31 23 FRED 0.4660 NONE 27 22 0.0351 22 22 17 0.4980
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AN CROSSINGS TYPE ERROR 31 23 FRED 0.4640 NONE 27 22 0.1940 28 20 0.0351 27 21 0.035 37 16 0.0022	AN CROSSINGS TYPE ERROR TYPE 31 23 FRED 0.4660 NONE 27 22 0.1990 28 20 0.0351 22 17 0.4980
22 7 850 20 0.0351 21 0.4980 17 0.4980	22 7450 20 0.1990 21 21 0.0351
171120	7 5 6 7
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MEDIAN CROSSINGS TYPE									
A	RAT	MEDIANS		MEDIAN CROSSINGS	TYPE	ERROR	TYPE	FRROR	REMARKS
Automotive Aut	240		9.5		FRED	0.2030	PNON		
A			5.5						
Automotive cut	1330		5.3			1.1800			
A	1335		7.7			0.4710			
Animal	1340		7.2			0.0335			
### RATE CAS AFIDIANS REDIAN CROSSINGS TYPE ERROR TYPE ERROR FOR CASINGS AFIDIANS AFIDIANS REDIAN CROSSINGS TYPE ERROR TYPE ERROR FOR CASINGS AFIDIANS AFIDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE ERROR FATE CAS AFIDIAN CROSSINGS TYPE ERROR TYPE ERROR FATE CAS AFIDIANS AFIDIAN CROSSINGS TYPE ERROR AFIDIANS AFIDIAN CROSSINGS TYPE ERROR AFIDIANS AFIDIAN CROSSINGS TYPE ERROR AFIDIANS AFIDIAN			2.9	24 18		0.2040			
RATE CHS WEDIAN CROSSINGS TYPE CRROR TY	RAT	=		AN CROSSING	TYPE	ERROR	TYPE	ERROR	REMARKS
RATE CHS WEDIANS 199.2 19 0.0001 RATE CHS WEDIANS 100.2 29 19 0.0001 RATE CHS WEDIANS 100.2 29 19 0.0001 RATE CHS WEDIANS 100.2 29 19 0.0001 RATE CHS WEDIANS 100.2 19 19 0.0001 RATE CHS WEDIAN CROSSINGS 17PE ERROR 17PE ERROR 100.0001 RATE CHS WEDIANS 100.2 19 0.0001 RATE CHS WEDIANS 100.2 19 0	240		2.0	-	FRED	0.1860	NONE		
RATE CHS WELLIAMS AND Z4 CHS	1525		2.6	_		0.0961			
RATE CHS HEDIANS RATE CHS HEDIAN RATE CHS HERDA RATE CHS HEDIAN RATE CHS HEDIAN RATE CHS HEDIAN RATE CHS	1530		2.0	_		0.0638			
RATE CHS	1535		2-0	51 +2		0.0742			
RATE CHS WEDLANS 19 16 00000 17VPE ERROR 1VPE CARON 1VP	1540		1.1			0.1350			
RATE CHS WEDLANG ROSSINGS TYPE ERROR TYPE ERROR FOR SINGS TYPE CHRON CROSSINGS TYPE ERROR TYPE ERROR FOR SINGS TYPE CHRON CROSSINGS TYPE ERROR TYPE ERROR FOR SINGS TYPE ERROR FOR SINGS TYPE ERROR FOR SINGS TYPE ERROR TYPE ERROR FOR SINGS TYPE	1545		0.0			E040-0			
RATE CHS WEDLANS HEDLAN CROSSINGS TYPE ERROR TYPE EAROR 2400 24 -04.8 -04.4 -0 24 -0 1130 -09.1 -09.4 -0 24 -0 1130 -09.1 -09.4 -0 24 -0 1130 -09.1 -09.4 -0 24 -0 1130 -09.2 -09.2 -09.2 -09.4 -0 1130 -09.5 -09.2 -09.4 -0 12 -09.6 -09.4 -09			1.1			0.0100			
## CHAIR CHS CHAIR	RAT	AIO		AN CROSSING	TYPE	ERROR	TYPE	FDROB	PFHADRS
RATE CHS HEUIANS HEDIAN CROSSINGS TYPE ERROR TYPE CAS POLIS PROPERTY CHS PARTY CAS POLIS PROPERTY CAS POLIS POLIS PROPERTY PROP	240		6.4	24 21	FRED	0.1710	NONE		
RATE CHS HEULANS HEDIAN CROSSINGS TYPE ERROR TYPE TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE			+.+			0.0663			
RATE CHS HEUIANS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1000		3.5			0.1130			
RATE CHS HEUIANS 16 0.177 PATE CHS HEUIANS 22 12 0.0011 TYPE ERROR PATE CHS HEUIANS 21 12 0.0010 HOVE ERROR PATE CHS HEUIANS 190.2 19 19 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 11 11 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 FRED 0.0010 HOVE ERROR PATE CHS HEUIANS 10 10 HOUT HOUT ERROR PATE CHS HEUIANS 10 10 HOUT HOUT HOUT HOUT HOUT HOUT HOUT HOUT	1005		4.4	~~		0.2120			
RATE CHS HEUJANS HEDIAN CROSSINGS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1015		+.+			0.1730			
RATE CHS MEDIANS MEDIAN CROSSINGS TYPE FROM TYPE ERROR TYPE FROM CHOSSINGS TYPE FROM CROSSINGS TYPE FROM CROSSINGS TYPE FROM NONE FROM CHOSSINGS TYPE FROM CHOSSINGS TYPE FROM TYPE FROM CHOSSINGS TYPE FROM TYPE FROM TYPE FROM CHOSSINGS TYPE FROM TYPE FROM CHOSSINGS TYPE FROM TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE		6	6.3	19		0.0181			
2400 24 -95.5 -92.1 24 12 FRED 0.0007 10006 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		JIAN		MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
## FATE CHS			15.1	_	FRED	0.0007	NONE		
HATE CHS HEIDIANS 21 12 0,0000 HATE CHS HEIDIAN CROSSINGS TYPE EHROR TYPE ERROR 2400 24 - 90.2	1055		8.0	_		£640.0			
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HATE CHS HEDIAN CROSSINGS TYPE EMPOR TYPE ERROR CHS	1110		2.5	•		00000			
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2400 24 -96.3 -90.4 11 10 FRED 0.0119 NONE CANONE C	RAT	MEDIAN		Z	TYDE	0000	1404	9000	940440
RATE CHS #EDIANS #EDIAN CROSSINGS TYPE ERROR TYPE FROR 10 10 10 10 10 10 10 10 10 10 10 10 10	240		V	-			1	ENTON I	REMEMBER
RATE CHS #EDIANS #EDIAN CROSSINGS TYPE FROM TYPE TYPE FROM TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1			•	LACO	1000	MONE		
RATE CHS — 69.8 16 12 0.0000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 0.00000 9 9 9 0.00000 9 9 9 9 9 9 9 9	1245			•					
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RATE CHS — 69.5 11 11 0.0033 RATE CHS — 60.5 14 8 0.0039 2400 24 - 91.5 -93.2 9 10 FRED 0.024 -91.5 -93.5 13 10 0.0004 -91.9 -94.7 13 12 9 0.0004 -91.9 -94.7 15 19 FRED 0.0003 RATE CHS — 60.4 92.5 12 19 FRED 0.0003 -92.9 -92.5 17 23 0.0014 -92.7 -92.8 15 10 0.0017 -92.1 99.2 17 23 0.0175	1255		0.0			0.000			
RATE CHS #EDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE CHS #EDIANS CHOSSINGS TYPE ERROR TYPE ERROR TYPE ERROR TYPE ERROR NONE CHOSSINGS TYPE ERROR TYPE ERROR TYPE ERROR TYPE CHS #EDIAN CROSSINGS TYPE CHS #EDIAN CROSSINGS TYPE CHS #EDIAN CROSSINGS TYPE ERROR TYPE CHS #EDIAN CROSSINGS TYPE #EDIAN CR	1300		6.6	_		0.0033			
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HATE CHS -95.5 10 FRED 0.024 NONE -91.3 -95.3 10 10 0.000 -91.9 -94.7 13 12 9 0.0004 -91.9 -94.7 13 12 0.0004 -91.9 -94.7 15 10 0.0012 Z400 Z4 -92.5 17 23 0.0018 -92.0 -92.2 17 23 0.0175		N N		AN CROSSING	TYPE	FRROR	TYPE	ERROR	REMARKS
HATE CHS HEUIANS HEDIAN CROSSINGS TYPE ERROR TYPE CHS HEUIANS HEUIANS TYPE FRED 0.0001 2400 24 -92.5 12 19 FRED 0.0003 NONE 10 19 FRED 0.0003 -92.6 -92.7 10 0.0011 -92.7 18 12 23 0.0175			2.5		FRED	8520°0	MONE		
HATE CHS HEUIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE CHS HEUIANS HEDIAN CROSSINGS TYPE FRED 0.0003 NONE CAS 17 19 FRED 0.0013 NONE CAS 17 19 FRED 0.0013 NONE CAS 17 10 10 10 10 10 10 10 10 10 10 10 10 10	1405			•		0000			
PATE CHS HEUIANS HEDIAN CROSSINGS TYPE FROM TY	1410		*			4000			
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RATE CHS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 2400 24 -92.5 12 19 FRED 0.0003 NONE -92.4 -92.7 10 0.0011 -92.9 -92.8 12 23 0.0175 -92.1 -93.7 18 19 0.0214			4.7	15		0.0012			
2400 24 -92.5 12 19 FRED 0.0003 NONE -41.5 -92.7 10 19 0.0011 -92.6 -92.8 17 23 0.0008 -92.1 -92.8 12 23 0.0175		LIAN		AN CROSSING	TYPE	FRROR	TYPE	ERROR	REMARKS
-92.6 -94.8 15 10 19 -92.6 17 23 -92.8 12 23 -92.8 12 23 -92.9 19 19			20		FRED	0.0003	NONE		
-02.0 -92.2 17 23 -02.0 -92.8 17 23 -02.1 -93.7 18 19	0101		1.20			0.0124			
-92.0 -92.8 17 23 -92.1 -93.7 18 19	6101		E (0.0011			
92.1 -93.7 18 19	1426		7.0			0.000			
16 16 16	6201		8.0	٠		0.0175			
	1630		3.7			0.0214			

PELLPRS	REHARKS	RELARKS	PELLEKS	RELARKS	RELEASES
ERROR	ENROR	ERROR	EAROR	ERROR	FROR
TYPE	N ON	NONE	NONE	NONE	NONE
M	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.000000000000000000000000000000000000			6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000
FAED	FRED	FAED	7 Y P E O	7 7 7 7 7 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0	FRED
MEDIAN CROSSINGS 28 15 21 14 22 16 21 17 16 14 9 9	MEDIAN CROSSINGS 25 24 25 24 26 26 26 26 26 26 26 26 26 26 26 26 26	SSOS	CROSS	CROSS	MEDIAN CROSSINGS 13 10 14 16 16 16 15 16 16 16 16 16 16 16 16 16 16 16 16 16
MEDIANS -91.7 .90.2 -91.6 .92.0 -92.0 .92.6 -94.5 .92.6 -91.9 .91.9	AIO		30000000 30000000	NOID	NATIO
S &	CHS 24	CHS SA	SAS SAS	SAS SAS	S *
	2400 2400	RATE 2400	2400 2400	2400 2400	2400 2400
20 TIME 20 TIM	201 TIME 201 1415 1420 1430 1440 1440	202 1518 1520 1518 1525 1535 1535 1535	200 200 100 100 100 100 100 100 100 100	200 100	200 11145 11145 11155 11200 1200

DATA RATE CHS		OIAN	CROSS	T 40 E	ERROR	1	ERROR	REHARKS
24 -93.8 -93.9 -93.9 -90.6 -90.6 -91.0 -91.0	66666 		6 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	FRED	0.1630 0.1630 0.01430 0.01430	NON		
DIA		HED]	12 22 22 15 15 15 15 15 15 15 15 15 15 15 15 15	TYPE PED PED	0.000000000000000000000000000000000000	TYPE	EROR	FEFF
# C	1 ANS 6 ANS	MEDI.	18 CROSSINGS 26 22 22 22 22 22 23 24 26 26 26 26 26 26 26 26 26 26 26 26 26	14 PE		HONE	2980	REMARKS
1 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	MEDIAN NUMBER	CROSSILES SE 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	TAPE		NONE	EPROP	REHARKS
101.5 MEDIAN 101.5 MEDIAN 102.3 102.0 101.9	101.5 MEDIAN 101.5 MEDIAN 102.3 102.0 101.9	MEDIAN	CROSSINGS 1 0 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	FRED		NOME	ERROR	REHARKS
MEDIAN SECTION	11ANS 198.4 PEDIAN 199.0 28 197.0 28 197.0 19		CROS	77 77 0		TYPE	2308	RELEGIC

		REMARKS	RENARKS	RELARKS	REMARKS REC PAD	RENARKS
	M K O	CR BOR	CRROR	FROR	ROUN	ERBOR
	NON	NOVE	NONE	TVP	TYPE	TVP E
	1 NED	74PE	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	TYPE	FRED	FACO
3071.3000	37 55 55 55 55 55 55 55 55 55 55 55 55 55	CROSS 176	CROSSING CRO	CROSSINGS 11 11 11 13	CROSSINGS	CROSSINGS 112 104 109
	21 22 19 3 1 2 3 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3 4	MEDIAN 13 13 13 13 13 13 13 13 13 13 13 13 13	MEDIAN 13 13 15 15 15 15 15 15 15 15 15 15 15 15 15	MEDIAN 100 100 100 100 100	MEDIAN 104	MEDIAN 194
			M. 04111111111111111111111111111111111111	NA 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	NS	ANS 172.0 175.0 185.0 180.0
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4	§ ≈	S * S	## *	S *	CHS ST	24 24
97.40	2400	RATE 2400	RATE 2400	2400 2400	RATE 2400	2400 2400
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1	212	25 2 2 3 2 5 2 5 2 5 2 5 5 5 5 5 5 5 5 5	214 214	215 215	216 216	217

132 240 24 241												
Automotive color		MATE	CHS	MEDI	ANS	MEDIAN	CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
AATE CHS		2400	54	-78.3	-75.8	in (in (FRED	0.0549	NON		
AATE CHS	326			7.00	100		ID (2100.0			
HATE CHS TOTAL TOT	330			-81.7	4000	-						
AATE CHS FF6	1335			-77-1	-75.1	12	-		00000			
AATE CHS WEDIANS WEDIAN GROSSINGS TYPE FROM TYPE TY	1340			-76-1	-74.6		12		0.000			
### Color			4110	-79.2		•	16		0.000			
AATE CHS		KAIL	SES	MEDI	₹	Z	CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
RATE CHS		2400	5	176.2	-72.7	_	n č	FRED	0000	NONE		
### CHS CHS ##DIANS ##DIANS TYPE ###################################				-77-8	-74.0				90000			
RATE CHS HEDIANS FRED 0.1260 0.1260		RATE	CHS	MEDI	ANS	MEDIAN	CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
RATE CHS WEDLIANS CROSSINGS TYPE ERROR TYPE ERROR CHS		2400	2	-92.2	-01.7	S	en ·	FRED	0.0030	NONE		
HATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ER	1540			93.0	-03.4	•	• •		0.1260			
RATE CHS #EDIAN CROSSINGS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1550			-01.7	4.00	• •	•		0210-0			
RATE CHS HEDIANS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1555			-94.3	-92.6	· in	P		00000			
RATE CHS HEDIANS HEDIANS TYPE ERROR TYPE FRROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1600			6.96-	-97.0	•	•		0.3220			
RATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR TYPE ERROR CHS			9			"	9		0.0000			
Z400 Z4 -996.2 -995.7 Z9 18 6SC4 4.6680 FRED Z2.2800 10.9180 1		RATE	CHS	0	₹	Z	CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
HATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1.250 RATE CHS HEDIAN CROSSINGS TYPE ERROR 1.250 POSS POSS POSS POSS POSS POSS POSS POS		2400	5	-98.5	-95.7	0	91	6SC4	4.6680	FRED	2.9280	
HATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1.0250 1.0	940			2.66-	2.96-	72	25		8.0130		2.2680	
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE FROM TYPE PROPERTY OF 1910 049180	980			***	100	7 6	6 3		2.0640		1.6990	
HATE CHS	955			0.70	04.0	1	e e		3.3360		0.0160	
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 10-10-10-10-10-10-10-10-10-10-10-10-10-1	1000			-97.4	-95.0	38	9		19.0650		2.4480	
HATE CHS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE FROM 10.9180 1.00000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.000000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.000000 1.00000 1.00000 1.00000 1.00000 1.000000 1.000000 1.000000 1.00000000				24.4		86	30		7.2650		2.3240	
### CHS 14 6 65C4 5.4080 FRED 0.9180 -100.0		RATE	CHS	MEDI	•	MEDIAN	CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
RATE CHS MEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE		2400	*	7-201-	-101-0	45	• ;	6804	5.4080	FRED	0.9100	
RATE CHS	115			1000	-08	200			04770		1.7690	
RATE CHS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1.2070 -97.9 -96.4 39 47 6.4010 0.1960 -97.9 -97.4 36 37 3.1110 0.1960 -97.5 -96.5 48 33 28 4.3030 -98.3 -97.5 22 23 10.7640 -98.5 -97.5 22 23 10.7640 -98.5 -97.5 22 23 10.7640 1.0250 -98.6 -97.5 24 17 7.2220 1.0250 -98.6 -97.5 24 17 7.2220 1.0250 -97.5 -96.8 24 17 7.2220 1.0250 -97.5 -96.8 24 17 7.2220 1.0250 -97.5 -96.8 17 19 0.5400 0.0020 -97.7 -96.6 19 16 0.5400 0.0020 -97.7 -96.6 19 21 0.3430 0.0020 -97.7 -99.7 20 19 21 0.5420 0.0020	120			-98.9	-98.2	23			3.6520		0.7000	
RATE CHS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1.6430 1.6	1125			6.66-	+-86-	39			6.4010		0.2320	
RATE CHS WEDLAN CROSSINGS TYPE ERROR TYPE ERROR 1.6430 240 24 -95.4 -96.5 +8 33 28 4.3030 FRED 1.6430 -96.3 -97.5 23 26 5.3170 FRED 1.2070 -98.4 -97.5 22 23 10.7640 1.2070 -98.5 -97.5 22 23 10.7640 1.0250 -98.5 -97.5 22 23 10.7640 1.0250 -98.5 -97.5 22 23 10.7640 1.0250 -98.5 -97.5 22 23 10.7640 1.0250 -98.5 -97.5 22 23 10.7640 1.0250 -98.5 -97.5 22 23 10.7640 1.0250 -98.5 -98.6 17 19 16 0.3430 0.0520 -92.7 -93.7 20 19 21 0.3430 0.0500	1130			198.0	-97.0	36			3-1110		0.1980	
2400 24 -96.1 37 26 95C4 3.5390 FRED 1.6430 0.7590 -97.5 -96.6 48 33 28 4.3030 FRED 1.6430 0.7590 0.		RATE	CHS		ANS	MEDIAN	SPUZZENAS	TVDE		TVDF		DELLON
PATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 19850 1985		2400	24			37	26	9SC4	3.6300	204	1.6430	
-96.3 -97.2 33 28 4.3030 0.7590 1.2070 -96.4 -97.5 22 22 10.7640 1.0250 1.0250 -97.5 22 22 23 10.7640 1.0250 1.0250 -97.5 -97.2 24 24 6.4420 1.0250 1				-97.5	-96.6	4	93		3.5170		0.5650	
-98.4 -97.5 23 26 5.6510 1.2070 -98.5 -97.5 22 23 10.7640 1.0250 -98.6 -97.2 24 24 6.4420 1.0250 24 -93.5 -96.6 17 19 0.5560 0.0020 -93.7 -95.6 19 21 0.3430 0.0020 -92.7 -93.7 20 19 21 0.0290	1215			-98.3	-97.2	33	82		4.3030		0.7590	
HATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 19000000000000000000000000000000000000	0221			-98-	-97.5	23	92		5.6530		1.2070	
PATE CHS HEDIANS HEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1.629 C	522			0.80-	-97.5	25	53		10.7640		1.0250	
RATE CHS MEDIANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR -93.6 -95.3 -96.6 17 19 36 0.5400 0.0020 0.0	1235			196	900	2	2 2		7.2220		1.0000	
2400 24 -93.6 -95.5 21 18 GSC4 0.3190 FRED 0.0021 -93.7 -96.6 17 19 16 0.5561 0.0020 -94.3 -96.2 19 21 0.3430 0.000 -92.7 -93.7 20 19 0.0590 0.000		RATE	CHS	MEDI	NS	MEDIAN	CROSSINGS	TYPE	FREDO	TYPE		DELLOKE
-95.3 -96.6 17 19 0.550 -93.7 -96.2 19 21 0.3540 -97.7 -93.7 20 19 0.0590 -92.1 -94.9 23 21 0.2520		2400	24	-93.6	-95	21	1.0	43C6	0-1190	FRED	0.001	
-93.7 -96.6 19 16 0.5560 -94.3 -96.2 19 21 0.3430 -92.7 -93.7 20 19 0.0590 -92.1 -94.9 23 21 0.2420				-95.3	-96.6	17	6	Ų	0.5400		0.0020	
-94.3 -96.2 19 21 0.3430 0 0.25.7 -93.7 20 19 0.0590 0 0.	1345			-93.7	9.96-	19	16		0.5560		0.0020	
23 21 0.05420	980			E-40#	-96.5	19	21		0.3430		0.0040	
0.02000 12 52 5.55 1.255	000			1-26-	-63.7	02	6.		.050		0.000	
	004			1-26-	0.00	23	21		-245		0.0002	

DENABLE					•		-		DENABUR	MEMBERS								REMARKS								PENABUR	MEMARKS						MEMAMKS							REMARKS	REC PAD						Charles Maria	REMARKS	REC PAD						
repor			0.000	0.0370	0.00.0	0000		1000	Copye	TOWARD OF THE PERSON OF THE PE	0.0030	0.00.0	0.000	0.00.0	0.0000	0.0020	0.0030	FRADE	0.2130								2000	00000			0.00		ENTOR					0.00	1000	ERROR	00000	0.000	0.000	0.0010	0.000	0.000	0.000	ERROR	000	9	8	:	:	0.000	0.1160
1404		LACO							1404		FRED							TYPE	2000							1485		FRED						LACO						TYPE	FRED							TYPE	FRED						
60000	2000		0664.0	0.4700	0.1470	4200	0767	0.4470	50000	TO LA COLON	0.0670	0.0330	0.0340	0.0100	0.0560	0.0460	0.0550	ERROR	0.2330	0.70		0.000	0.0440		0.04.50	60000 60000	Course of	0120-0	00100		00000	0.0130	FREE				9000	0.00.0	0.000	ERROR	0.0001	0.0000	0.0010	0.0850	0.000	0.0030	0.0000	ERROR		8	0.0010	0.0060	0.0001	0.0060	0.00%
TYPE	1000	1000							TVDE	3000	6504							TYPE	4088							TVDE	1000	4269				407	344	430						TYPE	65C4							TYPE	6504						
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SNA	4.00-	100 3	5.001-	-1001-		0.001-	3,101	-100.5	-	10.	5.46	-63.7	0.00	-91.9	-91.2	-93.A	-93.4	ANS	-91.B	4050	63.7	646	-03	9	100	3	,	7 66	77.0	4	73.7	2	- 18-	-76.6	-77.2	A2. E	30	-81.0	-79.7	Z	4.88-	-84.0	-86.6	-91.0	-87.1	-87.A	-88 · B	ANS	9.69	7.00	1.00-	-60.7	-90.0	5°16-	91.6
MEDIANS	9 10			+ · 86-	-98-2	-040-	1.00		2	•		8-26-	-89.6	06-	-01.5	-43.7		4F.01	-92.1	-03.7	0.50	-63	9.60-	0	3.60	5	- 12		76.5	446	4.5.4	2	1000	-77-8	-77.	2		-R9.9	-79.6	5	9.00-	-88.6	-H2.0	4.6H-	-85.8	-87.1	-18.3	5	E	6.84	-85.3	-44-7	-88.7	-91.5	0.00-
CHS	20	;							CHO	10	*							CHS	54							CHS	10	ţ				917	4	ì						CHS	5				٠			SEC	*						
MATE	2400								RATE	2000	2							RATE	2400							RATE	2400					at	2400							RATE	0						4	KALE	6400						
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\$	225								25	226	2							\$	227							200	228					3	000							Ž	231						1		252						

PATE	CHS	MELITANS		MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
240	54		2.06-	15 11	68C4	0.0140	FRED	0.000	REC PAD
		4.10-	4.16-			0.0120		0.000	
_		-89.2	+-68-			0.0460		012	
6		-91.0	-91.6			0.000		0.000	
•		-910.E	-91.4			0-1180		0	
ıo.		-95.1	4.46-	11 9		0.0010		0.0010	
			-97.0	15 10		0.2670		1000	1
E WAIE	2	5	ANS	CROSSI	TYPE	ERROR	TYPE	SOL E	REMARKS
	*2	1.64-	1.06-	15 16	920	.00	FRED	0.000	REC PAD
n e		1.00	0 7			0.0003			
.		0.00	0.70-	•		*0000		000	
n (200	2.88	~ .		0.0007		0.0380	
		- 10	0.00			0.0030		0000	
		4.74	1 200	11 21		1000			
	CHS	EDI	ANS	CROSSI	TYPE	ERROR	TVDE		DFWARKS
5 2400	77	-80.1	-91.6	15 15	4359	0010-0	6060	0000	OLIAN DIV
340		-89.5	-91.2			00.00		0	
En.		4-66-	916-	_		0.0040		0.00.0	
•		-BO.6	-90-5			00.00			
· NO		0.68-	-90-2			0.00.0		0000	
•		7.78-	-90.5			0.0140		9000	
		-89.5	-92.3	17 14		0.0120		0000	
E RATE	CHS	10	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
	54		-95.6	12	65C4	0.0140	FRED	0.0000	QUAD DIV
		-88.0	-91.0			0.0130		0.000	
••		-84.7	-91.0	_		0.0020		.000	
	970	-AB-7	_	5	8	0.0150		0000	197
MAIL	2	=	ANS	CROSSI	TYPE	ERROR	TYPE	ENROR	
	\$	0 1	E - 68-	01	9204	0.0140	FRED	0.000	OUAD DIV
		0.00	200	-		0.000			
		86.8	- BO. 3			0.00			
		-87.3	200			0100-0			
		-R5.6	-89.3	14 12		0.000		0000	
		-45.3	68			0.0003		0000	
E RATE	CHS	=	ANS	MEDIAN CROSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
240	5	4.78-	-89.4	•	65C4	0.0010	FRED	0.000	QUAD DIV
•		-H7.1	-89.1			0.0150		0.000	
.		600	200	0,1		0.0003		0.000	
		200				0.0030		0.000	
.		9.0		_		0.000		0.000	
•		0.66		21 51		90000		0000.0	
	977	-		A 2000 M	4	0.00.0		00000	
1000	5	1103h	SNS SNS	CHOSS	1000	A COL	TYPE	ERMOR	REMARKS
	+	6.69	000		4765	•	FRED	0.020.0	SOAD DIV
.			000			0.0000		0620.0	
			0 0			0.0030		0.0120	
- ·		5	4.00	ie *2		3£04.0		0.0010	
0		6.04-	6			100.		90000	
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5	TIME	RATE	CHS	MEUIANS	ANS	MEDIAN CROSSINGS	TYPE	EBBOA	TYPE	FRROR	REMARKS
246	1240	2400	54	2.20-	7-64-	13	65C4	0.0770	6063	0.0087	ATO OFF
	1245			9-10-	-63.	-		0.1660		0.0847	
	1250			A.00-	-05.7	53		0.00 A		0.0017	
	1255			4.[5.	-04.2			0.0100		0.00.0	
	1300			-03.9	2.46-			0.0157		0.0045	
	1305			-43.0	-03.H	14 12		0.0164		0.0038	
	1310			1.00-	-93.2	0		0.0164		0.0043	
2	11FE	MATE	CHS	SWY I (13W	ANS	MEDIAN CRUSSINGS	TYPE	ERROR	TYPE	ERROR	REMARKS
247	1340	2400	54		-92.0	30	69C4	0.0115	FRED	0.0026	OUAD DIV
	1345				-91.3	16		0.0019		0.000	
	1350				1.16-	12		0.0003		0.0000	
	1355				-92.5	12		0.0019		0.0085	
	1400				-94.0	e .		0.0196		0.0077	
	1410					91		*000*0		2000.0	
3	1111	DA TE	1	PACITANCE AND	4N5	SOUTSSORD INTROSP	2	# L D O O	2	0.0010	4
2	144	3400	66	ć	2 CO -	MILITAN CROSSINGS	100	EMROR		ERMOR	MEMARKS
	1445		· W	7 7 7 7	1000	- 1	9259	0.130	PRED	0.0000	OUAD DIV
	1450				1000	•		6.00		11000	
	1455			-92.6	-92.9	6 11		0.000		2000	
	1500			4.20-	-93.0	-		41000		0.0003	
	1505			H-00-	-90.4	~		0.0030		000000	
	1510	010		-41.3	-92.0	6		0.0111		0.000	
3	TIME	KATE	SI S	MEDI	Ž	CROSSI	TYPE	ERROR	TYPE	ERROR	REMARKS
546	1240	2400	54	-63-3	36-		6504	0.0114	FRED	0.0075	QUAD DIV
	1545			-45.1	-94.4			0.0620		0.0270	
	1550			-42.5	-63-3			0.0012		0.0000	
	1555			-92.6	-93.5			0.0800		0.0057	
	1606			E-6-6-	6.46	•		0.0570		0.0066	
	1610			4.60	693			0.000		0.0314	
200	TIME	RATE	CHS	46117	3	COUCK	TVDC		702		9700000
250	1640	0	24	-93.6	-95.6	16.	GSCA	0.0780		5410 C	STATE OF THE PARTY
	1645			-43.9	-95.5			0.1840		0.0683	
	1650			1.25-1	T. 76-	•		0.1540		0.0503	
	1020			0.50	-620	0		0.0300		0.0143	
	1406			0 0 0		71 C		0.0430		0.0178	
	1710				200			50000		20000	
Ş	TIME	HATE	CHS	MEDI	Z	CROSSI	TYPE	FRECE	TYPE	F0000	DENABRA
251	1405	2460	\$2	-85.5	-87.0	8 15	5SC4	0.0074	FRED	0.0264	DUAD DIV
	1410			-43.5	-86.5	10 16		40000		0.0021	
	1415			-45.3	J. CH-	16 10		0.0044		0.0022	
	1420			-R7.4	-87.8	14 14		0.0000		0.0014	
	1425			. x	-87.E	_		0.0001		0.0020	
	1436			4. T.	-82.0	6 t		0.000A		0.0039	
	7			×	689.0	n >		0.0018		0.0026	

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18 14 13 13 13 14 13 28 28 28 28 28
20 20 30 30 24 29 29 29
-84.5 2H 20 ##EDIAN CROSSINGS TYPE 9 -76.0 56 46 1 -74.6 60 50 4 -74.4 47 41 1 -76.7 36 42 40 1 -75.6 42 40
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E 60	MEMAMA	-001							REMARKS	100	1						REMARKS	L00#				RFHARKS	900							REMARKS	1001						REMARKS	-00 -						DELABES	SAKE OCC -	1				
	ENROR	0000	0000	0000.0	0.000.0	0.0001	000000	0.0000	ERROR	0.0007	0.0003	000000	0.000	0.000	0.0000	0.0010	ERROR	0.0007	00000	0000		FERCE	0.0004	1000	0.0007	0.0032	0.0020	0.0027	0.0010	ERROR	0.0135	0.000	0.0115	0.0103	0.0435	0.0246	ERROR	0.0052	0.0013	0.0163	60000	0.000		10000	0.0040	0.0111	0.00	0.0040	0.0036	
	1	A MED							TYPE	FRED							TYPE	FRED				TYPE								TYPE	FRED						TYPE	FRED						TVPF	- 14	1				
-	E MANON	10000	00000	0.0010	0.0021	0.0012	0.0049	0.0051	FRROR	0.0104	0.0007	0.0004	0.000	4100.0	0.0055	0.0044	EBROR	0.0010	0.0026	0.000	1000	FRROR	0.003	E000-0	0.0001	0.0026	0.000	0.0019	000000	ERROR	0.0019	0000	0000	00000	0.000	0.000	FRROR	00000	0.000	00000	0000	0000	0000	FRECE	90000	9.0038	0.0197	0.0001	0.0010	
	3000	475							TYPE	. 6SC4							TYPE	6SC4				TYPE	4289	,						TYPE	6 5C4						TYPE	65C4						TYPE	4085	,				
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	F T T O T U	200		97	0	17	19	2		17	1.9	16	16	21	18	11	MEDIAN	87	2	0 7	0	MEDIAN	-	9	14	16	16	13	-	MEDIAN	4 [13	£ 0	2	12	~	MEDIAN	S.	<u> </u>	- 0		<u> </u>	9.5	HEDIAN	Ñ	* *	28	16	23	-
		7 9 9	200	-91.	-82.7	-83,4	-83.7	-83.4	ANS	-80.c	-80°2	-79.3	-79.3	4.61-	-79.5	-70.4	ANS	-77-2		0.071	-78.	ANS	-74.9	-75.3	-74.4	-78.5	-19.5	-19.8		ANS	-83.0		-83.5	-63-5	-85.5	-45.0	ANS	6.00	7.01	100	4 50	1000	1	ANS	-17.2	-77-1	-77.3	-76.7	-16.4	
	She I Chan		3.6.1		\$ - TE-	1.1.	+.18-	-42.5	=	0.01-	9.4.4	-77.0	-77.7	-77.6	-18.4	-78.8	=	115.0	1.0/-	1.01	-76.9		-73.1	-74.2	-15.7	£77.1	-77.5	-14.5	•	Ŧ	-84.7	- OH-		-85	0-44-0	0 SH	5	* C P			4 601	1000	-H2.2	=	•	0.74	-74.2	-77-8	-10.7	,
01	56	,							CHS	%							SIC	5				CHS	54						•	Š	\$ 2						£	•						CHS	2					
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-82.7 -82.2 17 19 0.00000 0.0001 -82.6 -82.1 17 19 0.00001 -82.1 -82.1 17 19 0.00001 -82.1 -82.1 17 19 0.00001 -82.1 -82.1 17 19 0.00001 -82.1 -82.1 17 19 0.00001 -82.1 -82.1 17 19 0.00001 -82.1 -82.1 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.1 -82.2 18 17 19 0.00001 -82.2 -82.2 18 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	CHS HEDIANS CROSSINGS TYPE ERROR		9	ž	-84.0	-82.4		68C4	0.000	FRFD	0.0056	1000
CHS HEDIANS TYPE CROSS NGS TYPE CROSS CHS CHS CHS CHS CHS CHS CHS CHS CHS C	CHS HEDIANS 17 19 0.0003 0.0005 CHS HEDIANS 12 17 0.0001	۰			-82.¢	-61.0			0.000		0.0019	
CHS HEULANS TYPE ERROR	CHS HEDIANS TYPE ERROR	Ş			-43.7	-82.2			0.0003		0.0051	
CHS HEOLANS HEDLAN CROSSINGS TYPE ERROR TYPE	CHS HEOLANS MEDIAN CROSSINGS TYPE ERROR TYPE ERROR 1991 1991 1991 1991 1991 1991 1991	•			-83.4	-82.1			0.001		0.0052	
CHS HEDIANS TO THE COORDINATE CHS AND TABLE	CHS HEULANS 16 17 17 17 17 17 17 17				-B4.6	-82			2000		0.000	
CHS	CHS HFOLMAS ROTAL CROSSINGS TYPE ERROR TYPE	•			0.62	0.00						
CHS HULLANS THOLANS TYPE ERROR TY	CHS HEULANS TO THE CROSSINGS TYPE CROOK FRED 0.0056 11.7	. 4			42	2000			90000			
CHS Hallans	CHS		a F	77.5		-	TO THE POST OF THE		10000		00000	
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		0			-83.6	1.67-			0.0015		0.0150	
	HALLIANS HEDIANS 10 00010 000010 000001	i.			1.28-	-10.			900000		0.0036	
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CHS HELIANS 179.6 19 21 0.0006 0.0026 24 - 43.6 - 49.5 - 40.5 19 21 0.0007 0.0	CHS HELIANS 19 21 0.0006 0.0006 24 -43.6 -49.4 -40.4 -40.2 SIS 65.4 0.0007 0.0006 -43.6 -49.6 -49.4 -40.4 -40.4 0.0007 0.0007 -43.6 -49.6 -49.6 -40.5 31 21 0.0007 0.0007 -43.6 -49.6 -49.6 15 19 0.0007 0.0007 -43.6 -49.6 -49.6 15 19 0.0007 0.0007 -43.6 -49.6 -49.6 19 19 19 0.0007 -43.6 -49.6 -49.6 19 19 0.0007 -43.6 -49.6 -49.6 19 19 0.0007 -43.6 -49.6 -49.6 19 19 0.0007 -43.6 -49.6 -49.6 19 19 10 0.0007 -43.6 -49.6 -49.6 19 19 10 0.0007 -43.6 -49.6 -49.6 19 19 10 0.0007 -43.6 -49.6 -49.6 19 19 10 0.0007 -43.6 -49.6 -49.6 19 11 12 0.0007 -40.5 -49.6 -49.6 19 11 12 0.0007 -40.5 -49.6 -49.6 19 11 12 0.0007 -40.5 -49.6 -49.6 19 11 12 0.0007 -40.5 -49.6 -49.6 19 11 12 0.0007 -40.5 -49.6 -49.6 19 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 12 0.0007 -40.5 -49.6 -49.6 19 11 11 11 11 11 11 11 11 11 11 11 11	S.			-H1.4	-78.5			0.0001		0.0028	
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DATA	HATE	2400								KATE	2400							MATE	2400							PATE	2400							XAIR	2400						RATE	5400						
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REMARKS	DUAD DIV								DEMARKS	STATE OF THE	10000							MEMAMES	OUAD DIV							RFWARKS								REMARKS								REMARKS	L00P)					
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TYPE	FDED								TVDE	2000									FRED							TYPE	1000							TYPE	FRED							TYPE	FRED						
ERROR	40000	0.000		100000	0.000	0.0001	6000.0	0.001	60000	0.0407	0.0140	0.00.0			5000	00000		NOW N	000000	0.0170	0.00.0	6.000.0	0.0004	F000-0	0.0019	ERROR	0.0012	0.0022	90000	0.0010	0.0017	90000	0.0007	FRROR	0.0003	0.0007	0.0003	0.0010	0.0000	0.0004	0.0012	FRROR	0.0000	0.0053	0.0038	0.0121	0.0044	0.0038	0.0000
TYPE	65C4								TVDE	405E									65C4							TYPE	65C4							TYPE	6504							TYPE	6SC4						
MEDIAN CROSSINGS	5] 43	42 SR	1 4	n	52 49	51 43	52 44	- CE 9E	Sough	9E UE				10 64			Series and Market	2000		38 25		36 34	39 37	39 37		CROSS	57 84		54			42 80	75 76	MEDIAN CROSSINGS	117 93	110 99	91 91		90 87		33 32	CROSS	78 64	62 60				17	75 7R
	-86.6	-87.0		E-CD-	-85.0	-84.7	-83.4	-146.2	ANS	4.26-	-65-1	100	0.10	2 000	100	1 0 0		•	-06-	-93.3		26-	-92.5	-92.1	-93.0		4.06-	-90.3	4.06-	-90.5		-88.0	-88.8		-87.2	-86.4	-85.4	-84.5	-87.0	-85.0	-82.5		-87.5	-86.7	-86.4	-86.9	6.48-	-87.2	-87.6
-EUIANS	-A7.1	-84.7			5.7H-	-86.7	- H5.9	- KA-	7	7-00-	0010-	-00-	4.10-		100		-	-	7	-01.5	0.40-	-05.2	-45.5	-45.4	P-65-	-	9-16-	-93.2	-92.4	-92.4	-63.5	-89.7	-60.3	1034	-84.7	A. 18-	-47.S	-89-3	-88.6	-87.2	-84.3	HEDI	0.68-	-88.4	-86.3	4.84-	-84.6	-89.2	-88.8
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EAROR AEKARKS 0.0003 0.0003 0.0002 0.0002 0.0002	ERROR C.0000 C.0	ERROR REMARKS 23.7519 LOOP 20.8350 12.6399 8.7465 6.6714 5.2504 ERROR REMARKS 0.0236 0.0236 0.0422	0.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010 6.0010	0.0636 ERROR REMARKS 0.1135 GUAD DIV
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TYPE	200									TYPE	FRED								707		1				TVDF		PACO			TYPE	FRED								1 - 1	r well							TYPE	FRED							
FRROR	0.0404	0.081	103016	0.0048	0.0232	0.0056		0.0798	0.1404	ERROR	0.0015	41000	61000	+100-0	00000	0.000	0.0026	900000	50000		20100	1.5091	1.1636	0.7156	2000	2000	54.5103	19.4460	25.5576	ERROR	36.0586	35.4195	42.0867	44.5869	15.1401	11.8645	16 2700		KOKE T	140.00	1001001	17.4597	13.1924	12.5816	16.7652	19.3071	ERROR	0.3939	C.868n	0.4577	0.5652	0.5443	0.5173	0.3432	
TYPE	ACCA									TYPE	6SC4	í							TVDE	1000	1000				TVDE	1000	+ > 0			TYPE	65C4							-	3000	420							TYPE	65C4							
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MEDIANS	-47.3	9.40			-96-1	-95.5	6 10	2016	4.06-	MEDIANS	-92.5	-03.5	-01			-61.3	-91.7	-92.4	MFDIANS						MEDIANS	-0K. 2	3000	-62.		MEDIANS	03.0	-93.2	-93.6	-94.3	8.46-	-91.6	900	2	4.50-	4.60	400	0.00	200	+-26-	-93.5	-93.5	Ž	-95.3	-97.0		-97.4				
¥	-07.0	27		500	-96.0	-92.9	40-		-42.0			5.0-	103.7	4 6 0 1	9.76	4.50	2.26-	-93.1	J.JM		2001	0.191	-102.3	-190.2	HE	4.00	200	5.25	-45.3	ME	-93.6	-43.3	-46.6	-95.3	-63.5	7-10-	-07	MEDI	4.70	9	96.40	103		-03·¢		-46.0	MEOL	-98.1	-66-1	-100.5		4.66-	-100.5	-9A.3	
CHS	24									CHS	54								CHS	40	,				CHS	24	,		1	SHO UHO	54							VHC	24								CHS	54							
RATE	2400									RATE	2400								KATE	2400					KATE	2400			ļ	KATE	2400							PATE	2400								KATE	0							
			1216	0101	1320	1325	1330	200				1510	1515	1520	1000	5267	0541					207	1625					5401				1200	1205	1210	1215	1220	1225				1205	יובו	1	1315	1350				1410	1415	1420	1425	1430	1435	
\$	29									Ž	2								5	200					Š	297			i	2	29							2	290								2	30							

	470	O O O		REMARKS	1000				9700000	PARTY OF THE PARTY					REMARKS	1007																						DELLABORE	STATE OF THE STATE					PENARKS	100					
	9000	NO LANGE		ERROR					0000	-					ERROR																							20000	0.0007	1000.0	00000	0.0057	0.0022	FRROP	1000.0	2000	0000	0000	0000	
	1001	NON		TYPE	NONE				1007	NON C					TYPE	NONE																						1405	FRED					TYPE	6060					
	0000			ERROP	0.9641	1.8470	9.1631	0.0083	10000	0.0361	0.0079	0.1567	0.0634	0,0575	ERROR	0.0001	0.0108	0.0300	0.0063	900000		0.00%																00004	0.0078	0.0179	C 800 0	0.0825	0.0550	ERROS	1500.0	940000	0.0010	0.0130	0.0136	
	100	NONE	C C	TYPE	9 2€				1001	4088	,				TYPE	65C4																						TYPE	6SC4					TYPE	6SC4					
	MEDIAN CONSTINES	53	~	MEDIAN CROSSINGS		22 20		23 26 27	2000	36		27 25		7	CROSS				62		22																	MEDIAN CROSSINGS	99	92 83				CROSS	75 95				78 68	
	MEDIANS	-100.5	A.66-	4EDIANS			m (-42.3 -62.1 -83.0 -82.0	Z	-80.0 -80.4				-80.3	UIANS				1.00/1					01									-76-5 -76-5					DIAN	-A5.7 -90.3					MEDIANS	-A2.4 -89.0					
	CHS			CHS	*2				CHS	54					S S	v																						CHS	54				Ī	CHS	24					
UATA	RATE			RATE	2400				I	2400					7	2007																						RATE	2400					RATE	2400					
DELTA MOD	-	301 1550	_	BUN TIME		1306	6057	1315	_	304 1425	1430	1435	1440		102	7	1261	6261	1636		0+61	1942	1550	1999	0097	6001	0101	1015	707	5201	0501	6601	1645	1650	1655	1700	1705	RUN TIME		1225	1230	1235	~ 1	RUN TIME	_	1310	1315	1320	1325	

LOOP LOOP	REHARKS LOOP REHARKS LOOP	NON	REMARKS NON DIV DOOP RKS
4000M	M-8-9		# 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
TYPE	TYPE TYPF NONE	74 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
ERROR 0.0106 0.0022 0.0014 0.0003	ERROR 0.0740 0.0710 0.0211 0.0034 0.0034 0.0108	FRRD 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000	ERROR 0.7970 0.7740 0.7740 0.1870 0.7710 ERROR 0.1550 0.1310 0.1310
TYPE GSC4	179F 6504 179E 6504	35 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	6 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
MEDIAN CROSSINGS 58 94 96 96 71 84 93 96	MEDIAN CROSSINGS 85 61 121 112 124 110 118 117 109 111 MEDIAN CROSSINGS 106 RT RS 79 96 85 95 85 103 79	#EDIAN CROSSINGS 11H 12B 13A 145 121 119 69 99 99 86 118 113 132 107 HEDIAN CROSSINGS 97 94 94 193 91 87 80 94 90	MEDIAN CROSSINGS 100 73 144 125 123 117 133 118 151 142 177 177 19 61 30 61 56
MEDIAN 58 96 71 71	MEDIAN 121 121 121 1124 1124 1106 1	4EDIAN 13A 11B 11B 11B 11B 11B 11B 11B 11B 11B 11	HEDIAN 100 1123 1133 1133 1151 1151 1151 1177 HEDIAN 29
4FUIANS -66-0 -2 -86-0 -9 -84-9 -9 -83-1	ALAGE SECTION ODOOS PEROSOS ALAGES SECTION ODOOS	2 2	MEDIANS
4F01	1	A A A A A A A A A A A A A A A A A A A	177 6 177 6
CHS S.	N T N	2. 2. 2. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	£ * 5 *
MATE 2400	10 10 44 44 10 Fe	2	24 44 60 64 64 64 64 64 64 64 64 64 64 64 64 64
11 ME 1350 1400 1405	10011111111111111111111111111111111111	11205 12205 12205 12205 12305 12305 13305 13305 13305 13305 13305	10000000000000000000000000000000000000
S C C C C C C C C C C C C C C C C C C C	No Se	10	16 26 36 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4

REMARKS	REMARKS LOOP	REMARKS LOOP	REMARKS LOOP
CRROR	R R R S R R R R R R R R R R R R R R R R	0.00033 0.00033 0.00136	00000 00000 00000 00000
TYPE	NO PE	3 × P P S C +	TYPE 6SC4
ERROR	200 200	6.0120 0.0120 0.0120 0.0120	ERROR 0.0087 0.0065
NONE	Z → Z → Z → Z → Z → Z → Z → Z → Z → Z →	TYPE 6SCA	TYPE GSC4
MEDIAN CROSSINGS 23 34 34 37	HEDIAN CROSSINGS 16 A 31 19 28 23 30 31 31 26 26 25	MEDIAN CROSSINGS 13 15 24 23 25 27 26 24 33 29	MEDIAW CROSSINGS 37 22 33 27 33 36
MEUIANS -72.5 -72.7 -73.0 -75.5	HEDIANS 1144.6 1000.2 1000.4 1000.4 1000.4 1000.7 1000.7 1000.7 1000.5		MEDIANS -41.3 -85.4 -84.7 -86.2 -43.3 -85.7
S. S	CHS	C+S	CHS 24
RATE.	A .	2400 2400	RATE 2400
1105 1110 1110 1130	17-NE 1230 1240 1250 1250	1116 1355 1400 1410	1176 1425 1430 1435
317	318	319	35 25 20 30 30 30 30 30 30 30 30 30 30 30 30 30

Table IV

Run #	Time	Tracks	Fade Rates
36	1425-1430	2, 3	71, 72
42	1005–1010	2, 3	39, 29
	1025-1030	2, 3	22, 23
44	1205-1210	2, 3	20, 12
127	1645–1650	4, 5	106, 76
134	1645-1650	4, 5	63, 57
142	1300–1305	4, 5	8, 9
164	1305-1310	4, 5	18, 14
215	1320–1325	4, 5	16, 19
233	1540-1545	4, 5	17, 23
256	1310-1315	4, 5	52, 43

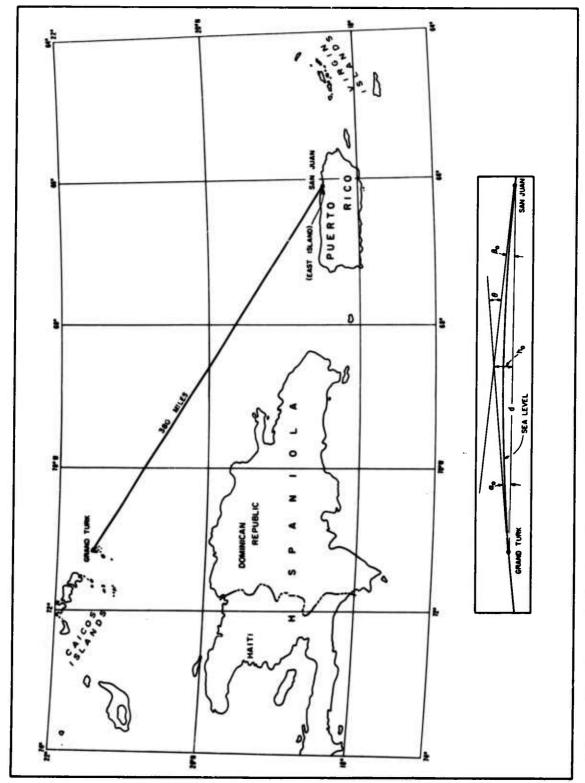


Figure 1. Maps of the Grand Turk - East Island path and side view showing path geometry.

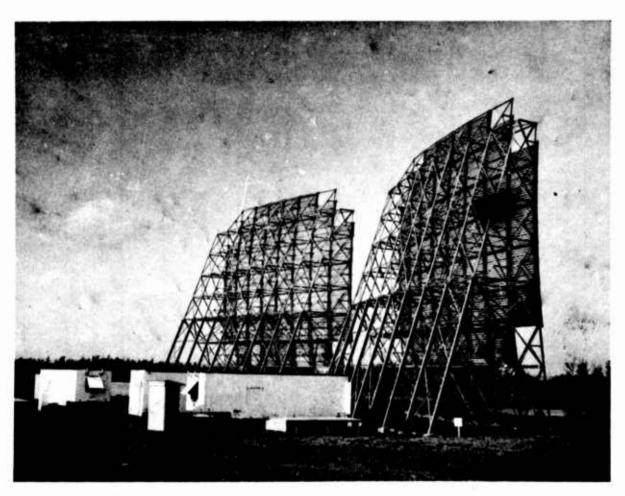


Figure 2. Sixty (60) ft. antennas at East Island site.

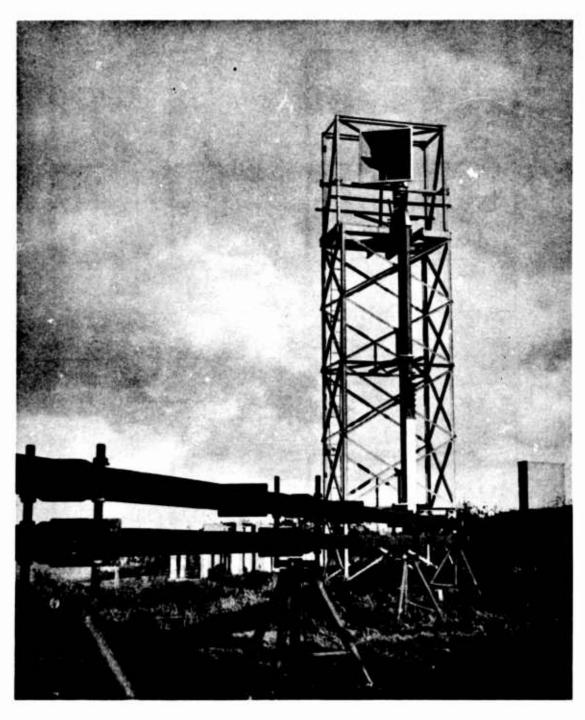


Figure 3. Feed horn and wave guide section at East Island site.

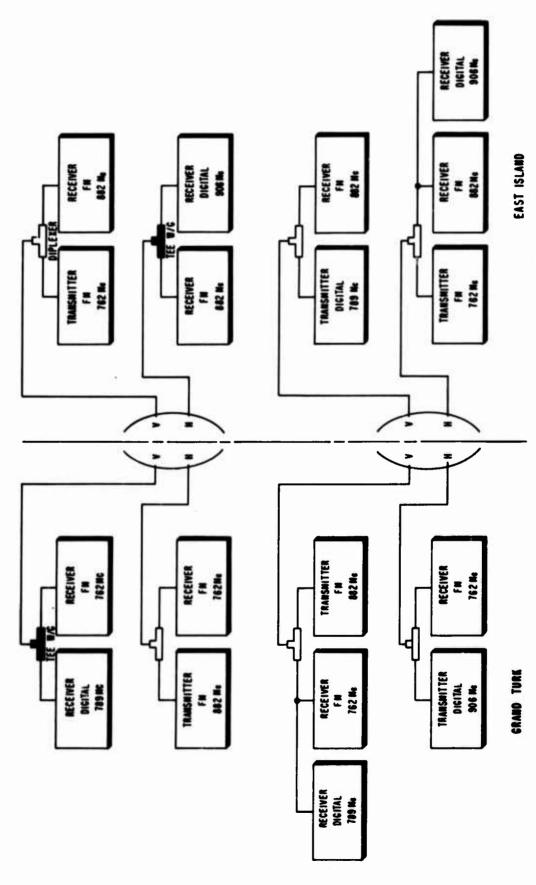
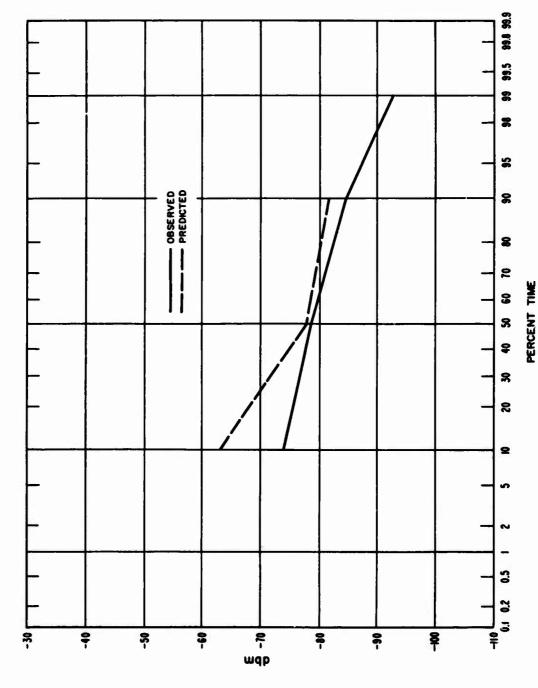
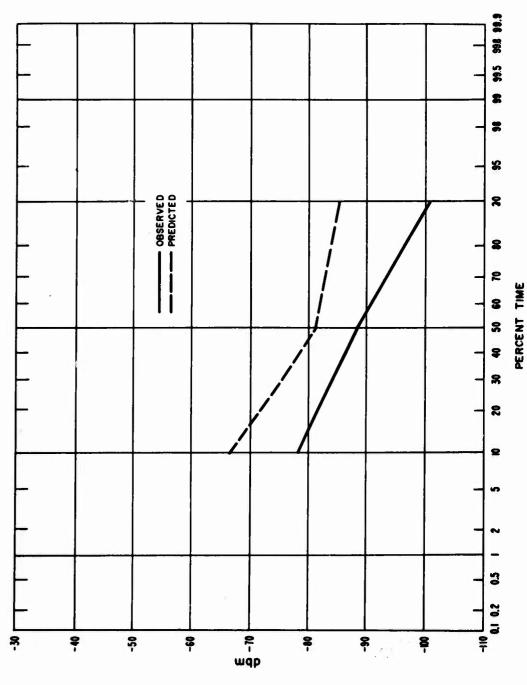


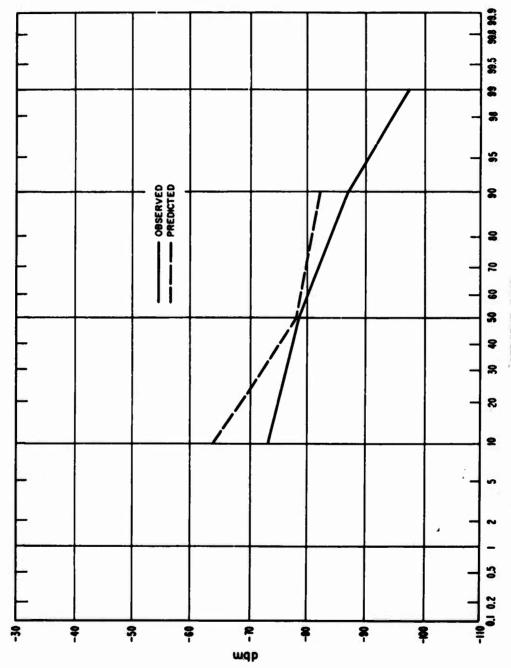
Figure 4. Schematic of available transmitting and receiving facilities.



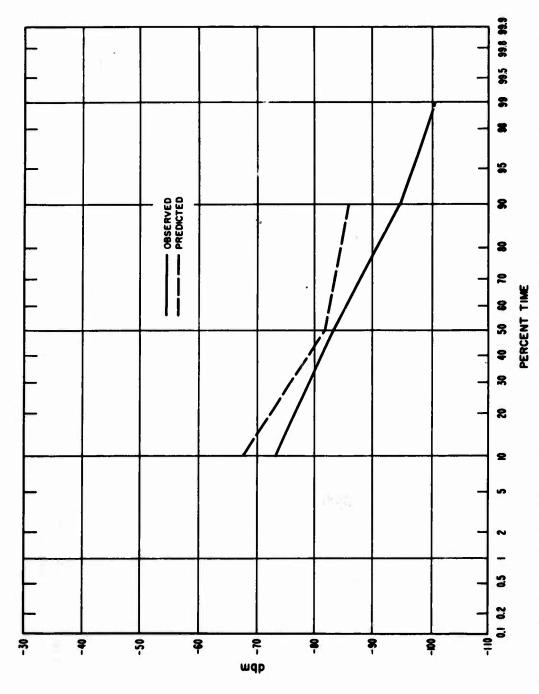
Cumulative distribution of predicted and observed received power for the period August, September and October 1962 at the East Island site. Figure 5.



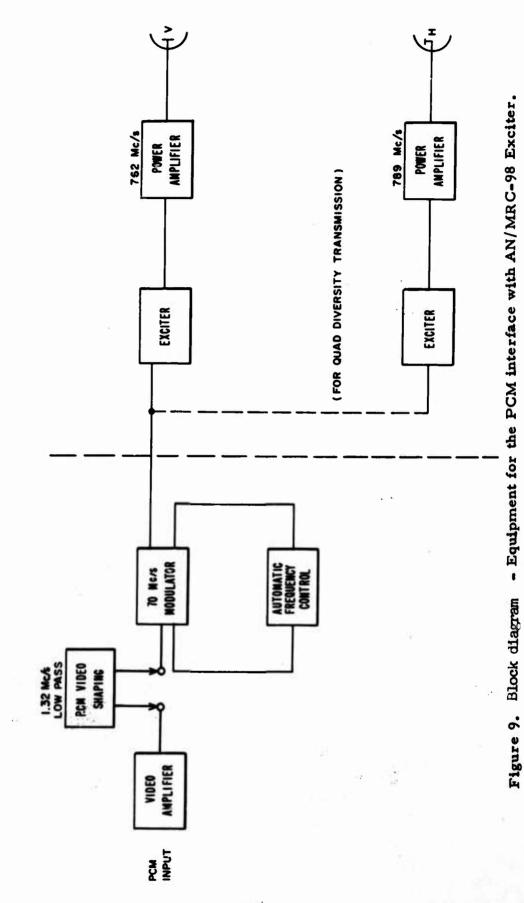
period November and December 1962 - January 1963 at the East Island site, Figure 6. Cumulative distribution of predicted and observed received power for the

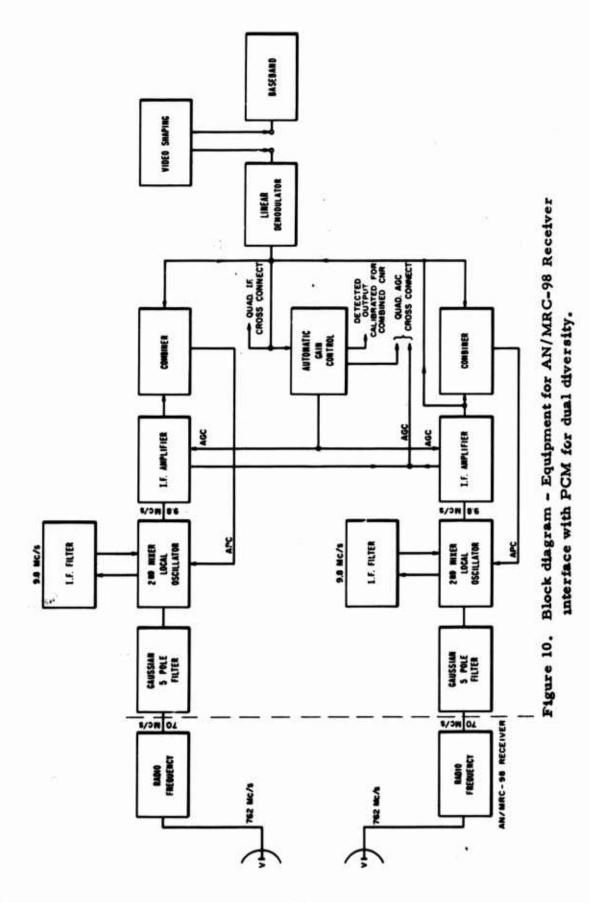


period May, June, July, August and September 1963 at the Grand Turk site, Figure 7. Cumulative distribution of predicted and observed received power for the



Cumulative distribution of predicted and observed received power for the period February, March and April 1963 at the Grand Turk site. Figure 8.





٠,

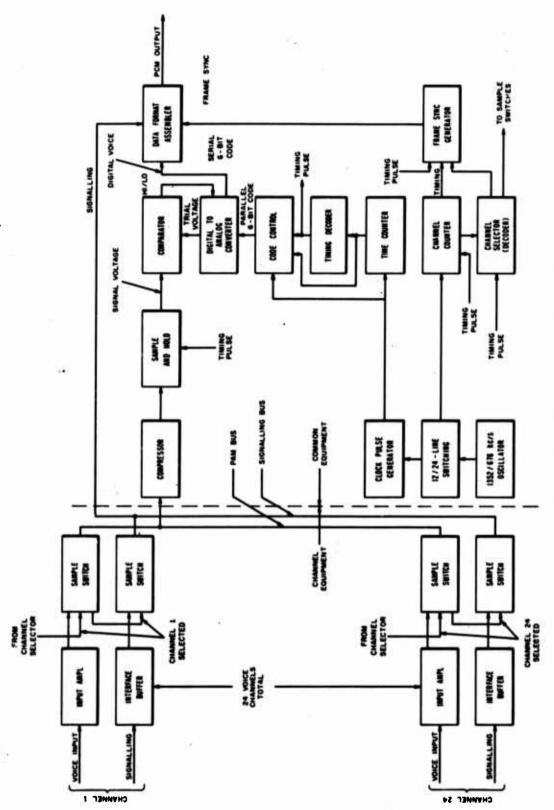


Figure 11. Block diagram - PCM Multiplexer.

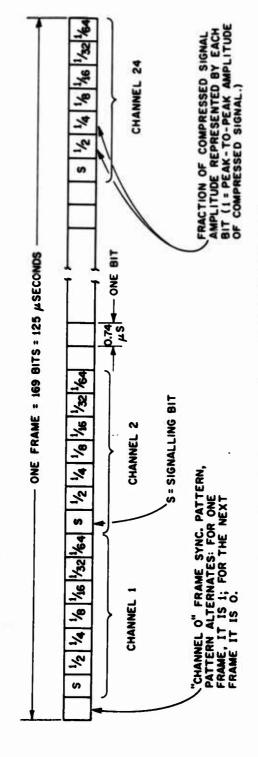
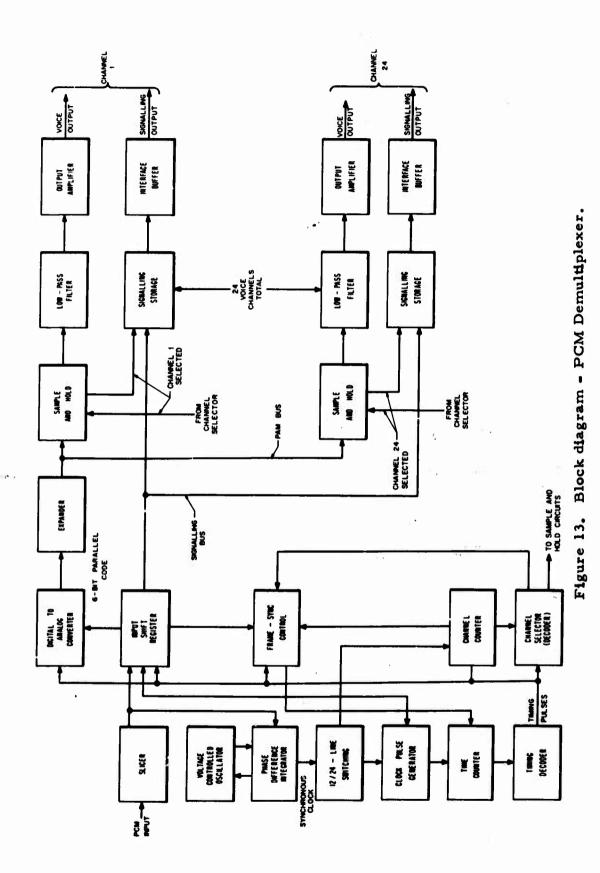
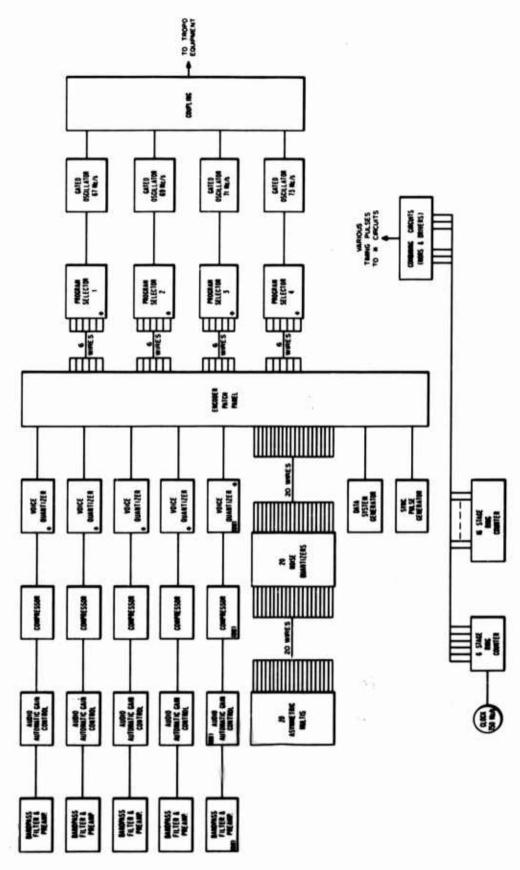
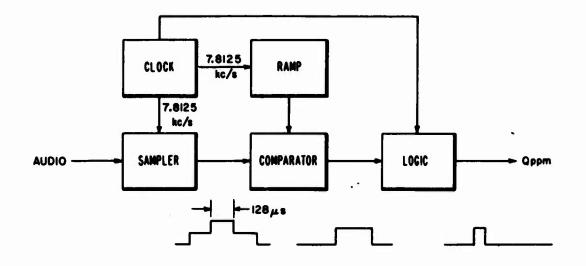


Figure 12. Block diagram - PCM Data format.







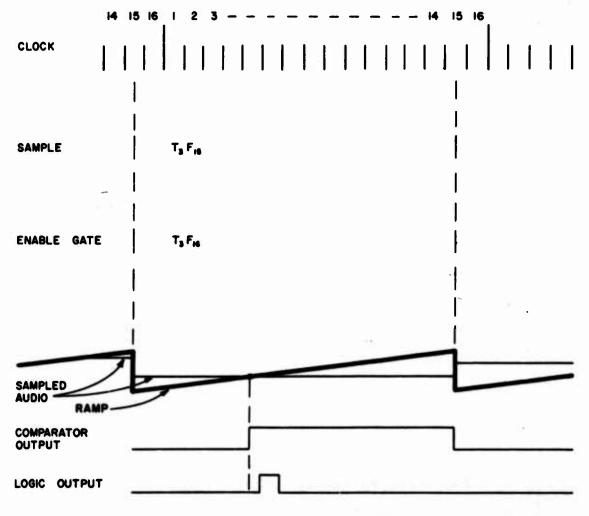


Figure 15. Voice Quantizer Timing Diagram.

```
Time Slot
               123456
               1 - 2 3 4 -
                                Noise Channel 1
               1 - - 2 3 4
               14--23
               1 3 4 - - 2
               2413--
                                             5
               2 - 4 1 3 -
               2 - - 4 1 3
               23--41
               213--4
               3 1 4 2 - -
                                             10
               3 - 1 4 2 -
               3 - - 142
               32 - - 14
               3 4 2 - - 1
               4312 - -
                                             15
               4 - 3 1 2 -
               4 - - 3 1 2
               42 - - 31
               412--3
               - 321-4
                                             20
               --4321
                                Voice Channel 2
               -1-432
                                             3
               -21-43
                                             4
               -4321-
                                             1
               1234 - -
                                Sync and Order Wire
```

Figure 16. Frequency - Time Program

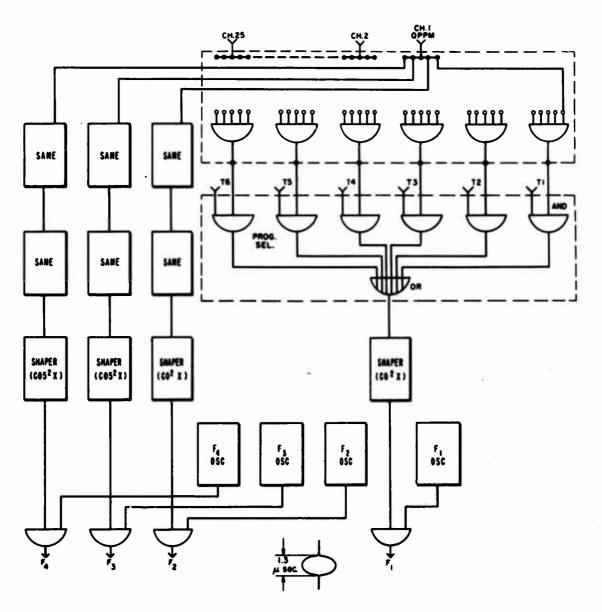
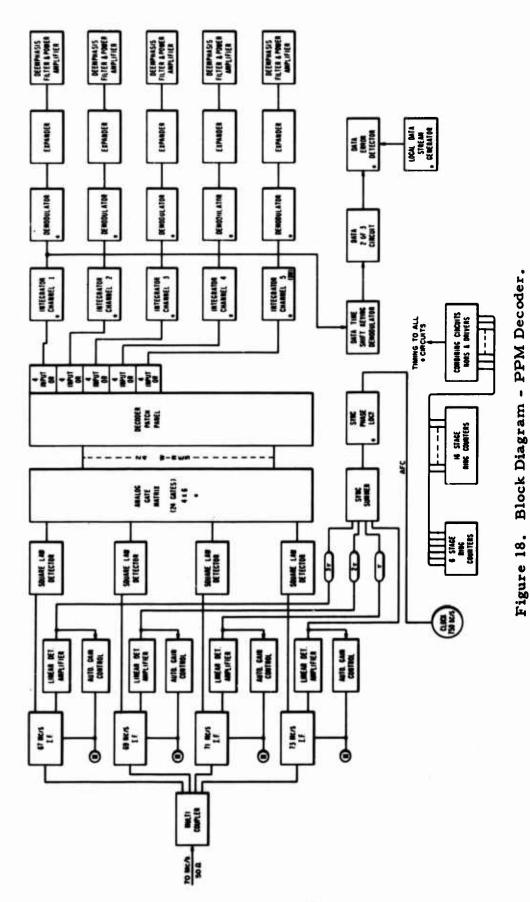


Figure 17. Block diagram - Match panel and program selector.



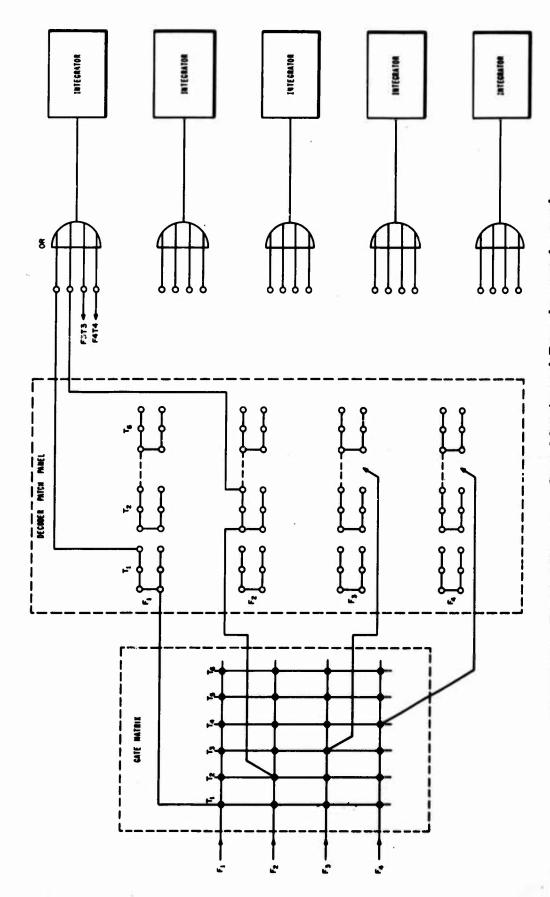
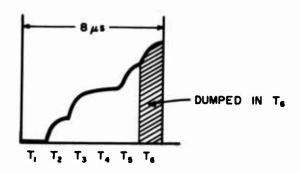
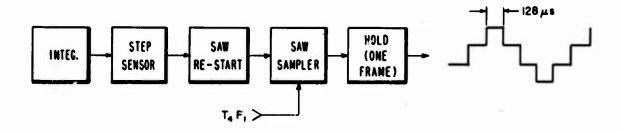


Figure 19. Block Diagram - Gate Matrix and Decoder patch panel.

INTEGRATOR INTEGRATES OVER ONE FRAME (8 μ s). THE OUTPUT OF THE INTEGRATOR IS DUMPED AT THE END OF T₆ IN EACH FRAME.



DEMODULATOR



SAW

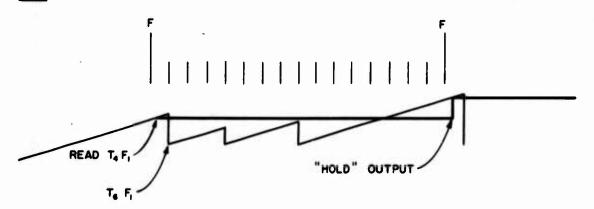


Figure 20. Integrator and Demodulator diagram

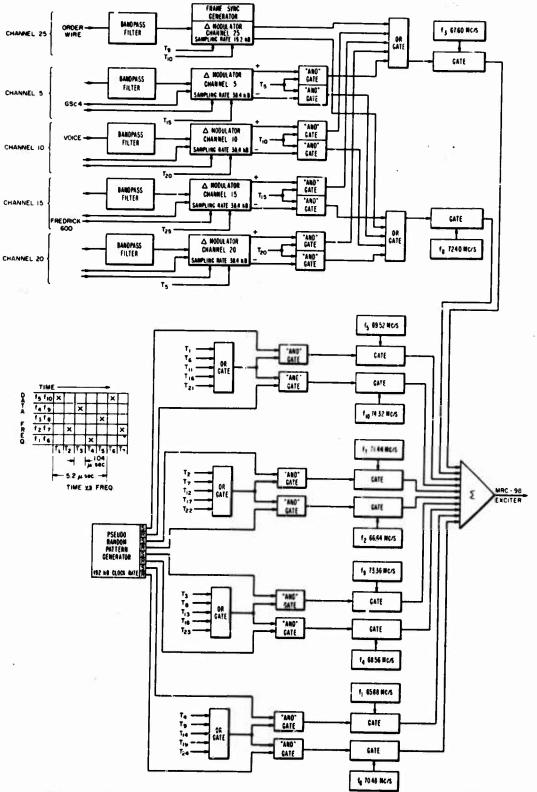


Figure 21.. Block Diagram - Motorola Δ modulator TDM/FDM Multiplexer transmit terminal.

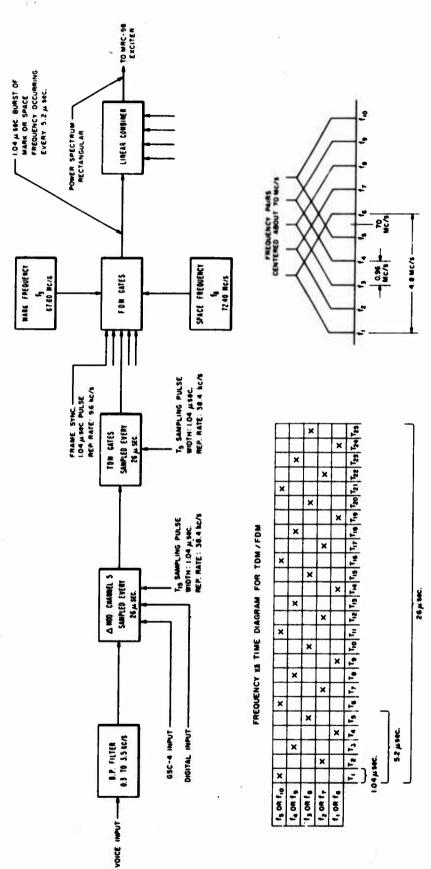
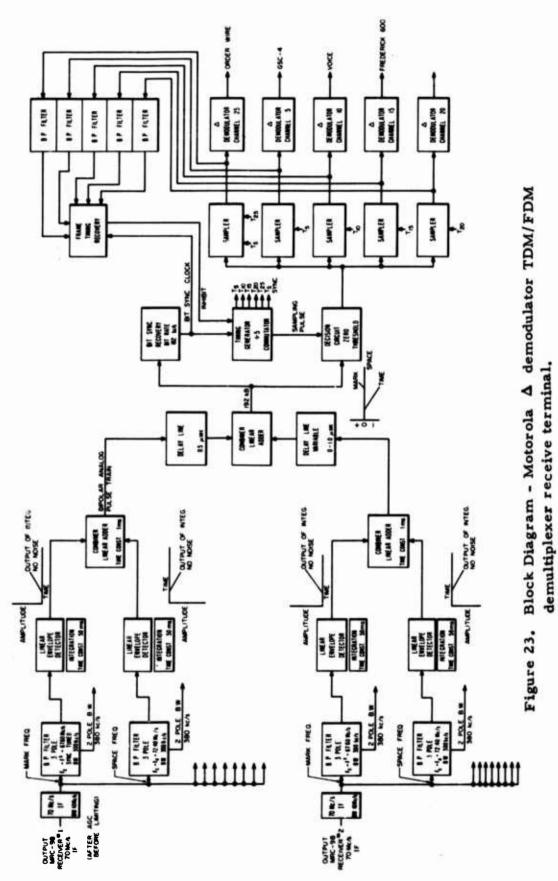
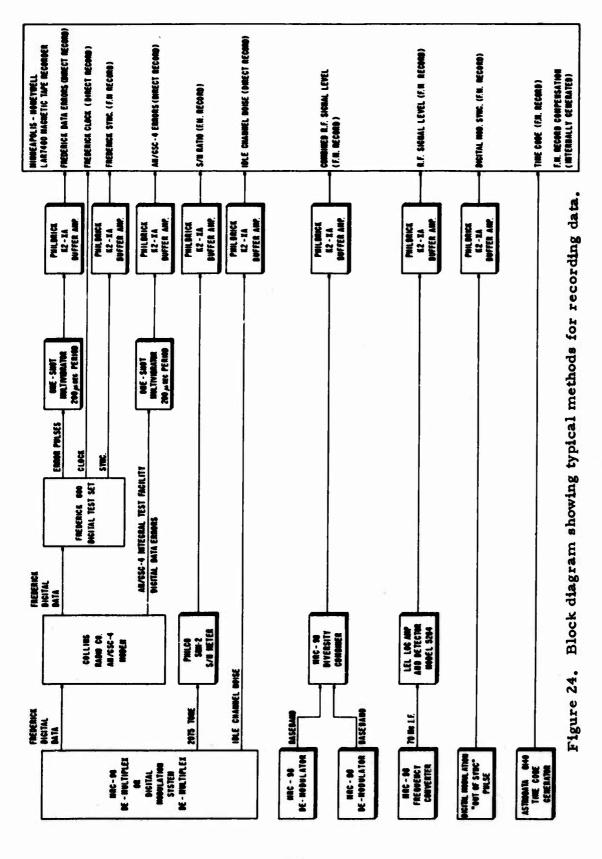
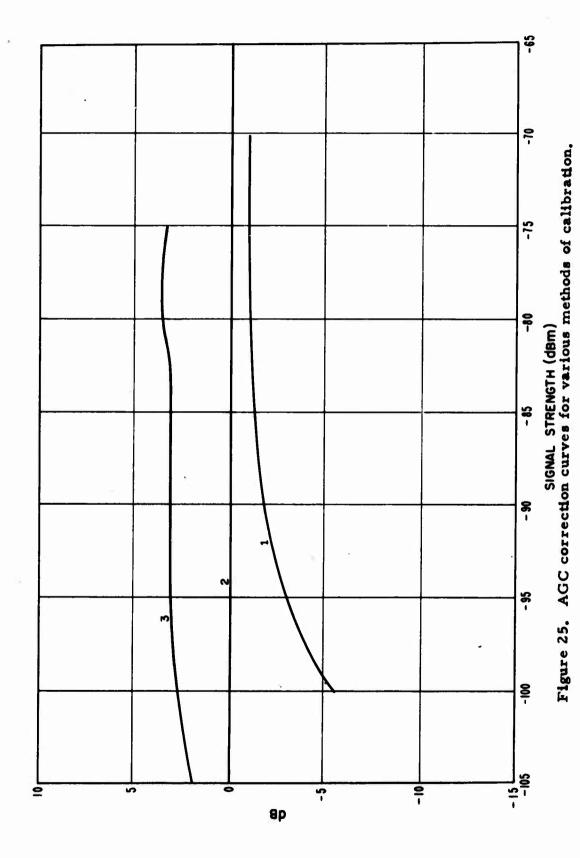
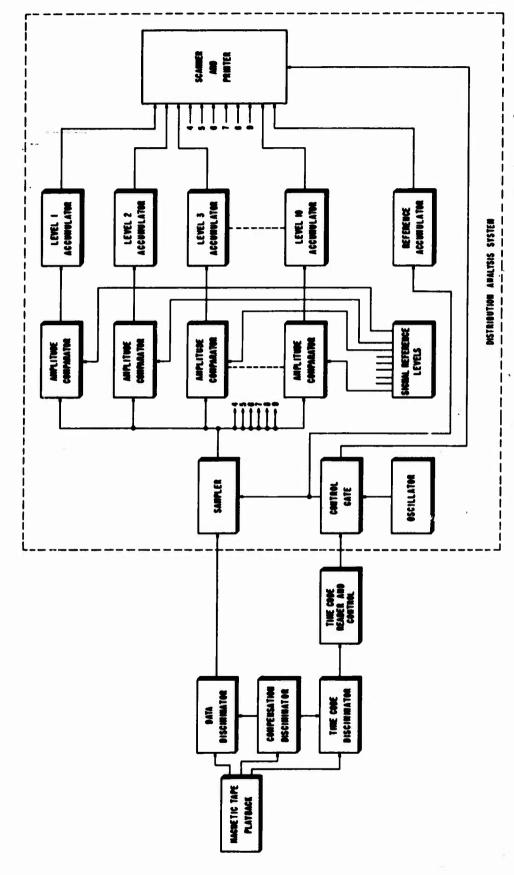


Figure 22. Block Diagram - Single channel Motorola A modulator TDM/FDM multiplexer transmit terminal.

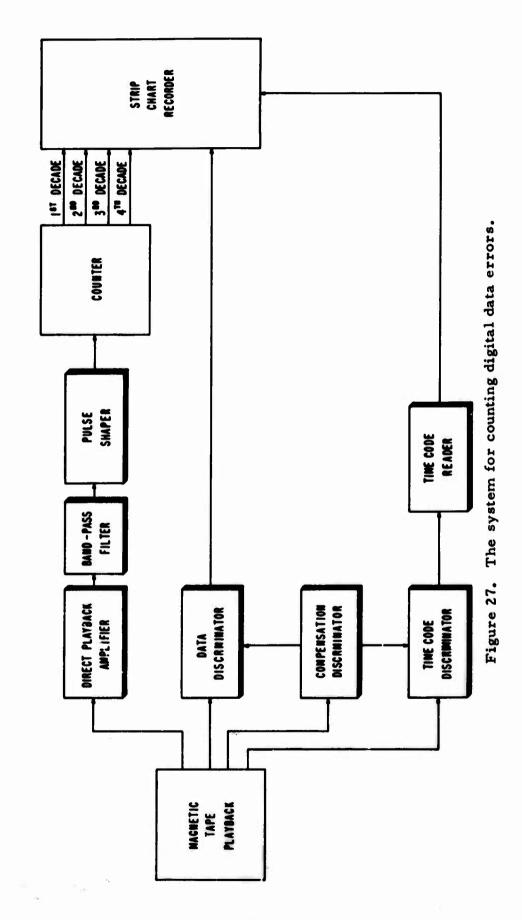








The system for obtaining the cumulative amplitude distribution and a detailed block diagram of the Distribution Analysis System. Figure 26.



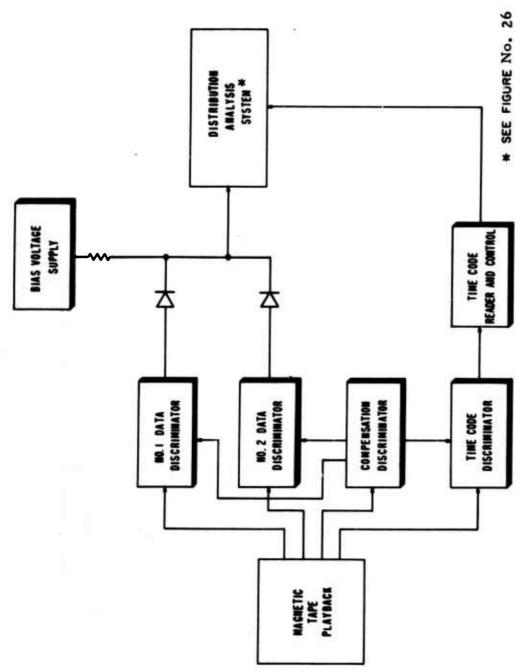


Figure 28. The system used to determine the cumulative amplitude distribution of two "combined" received signal strengths.

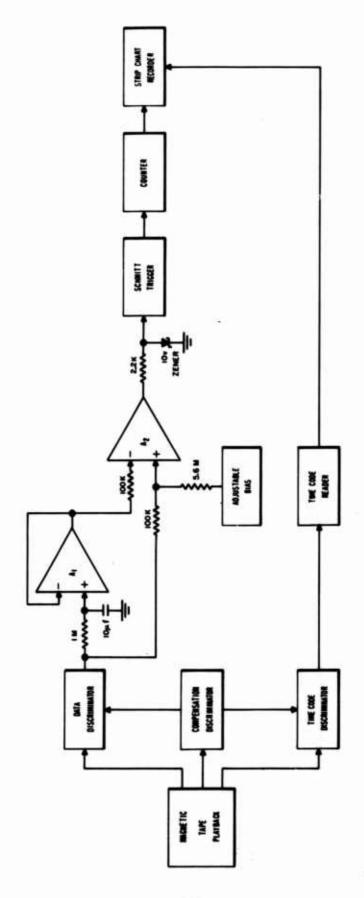


Figure 29. Circuit diagram for median crossings.

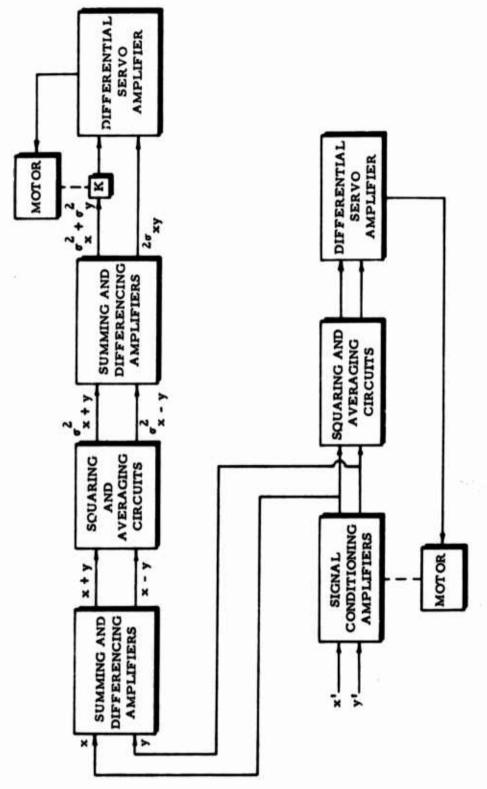
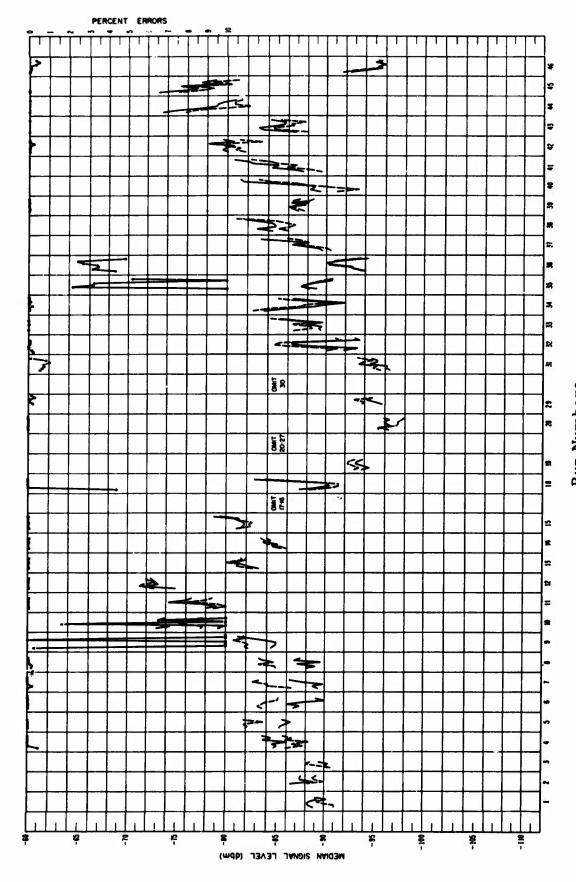
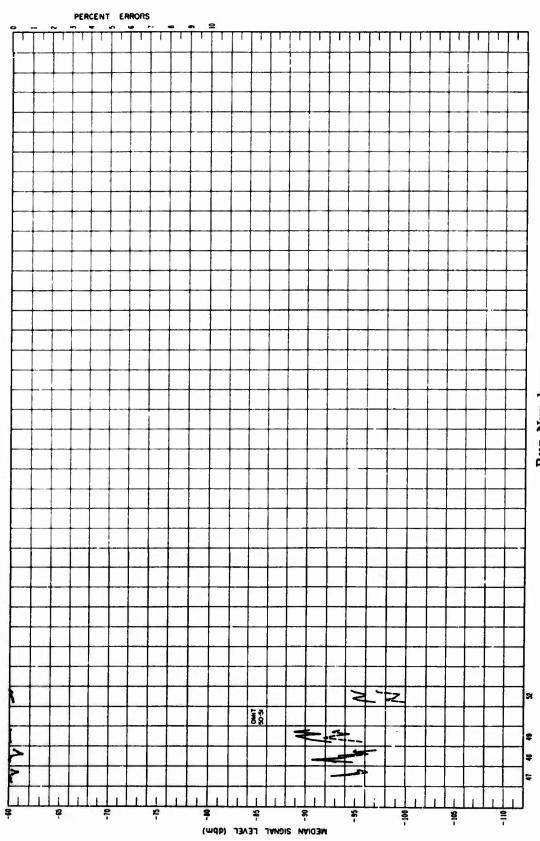


Figure 30. The analog correlation computer used to compute the cross correlation of two parameters.



Run Numbers Figure 31. Medians and error rates for the FDM system.



Run Numbers Figure 32. Medians and error rates for the FDM system.

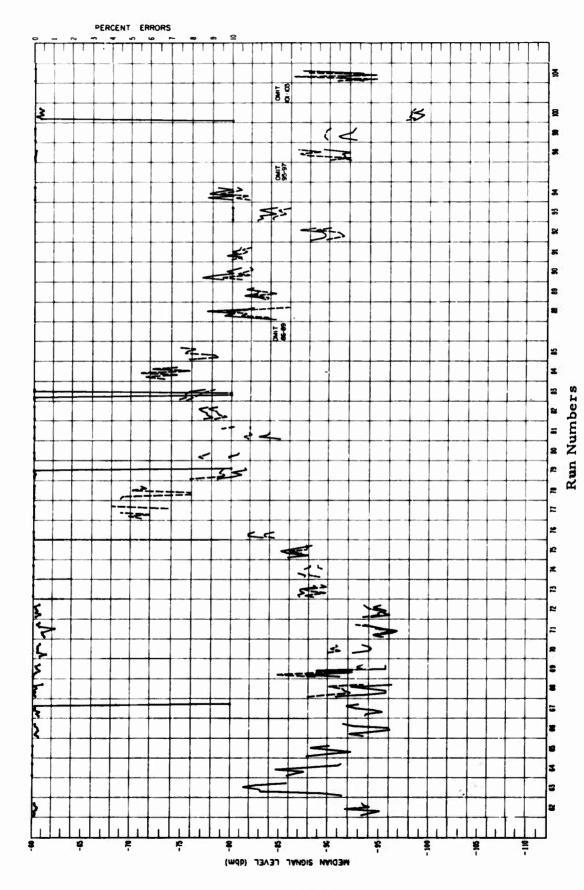
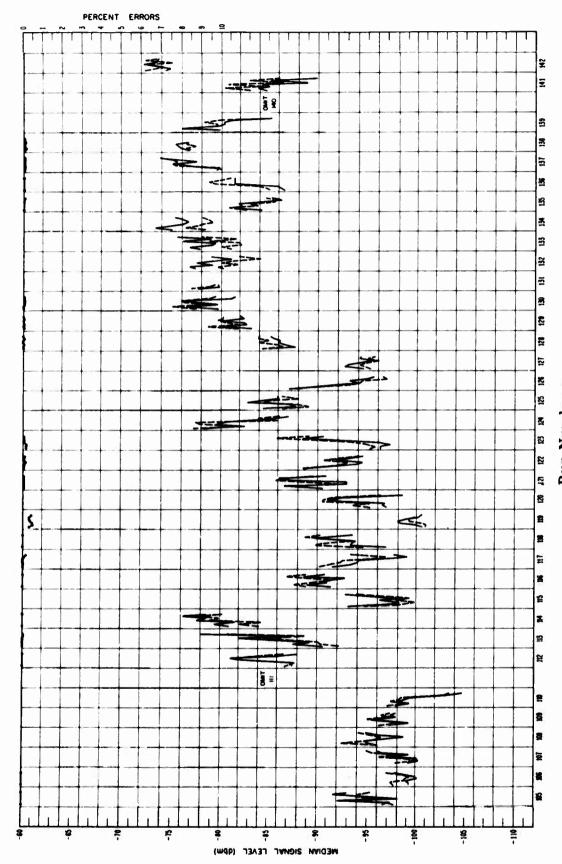


Figure 33. Medians and error rates for the FDM system.

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Run Numbers Figure 34. Medians and error rates for the FDM system.

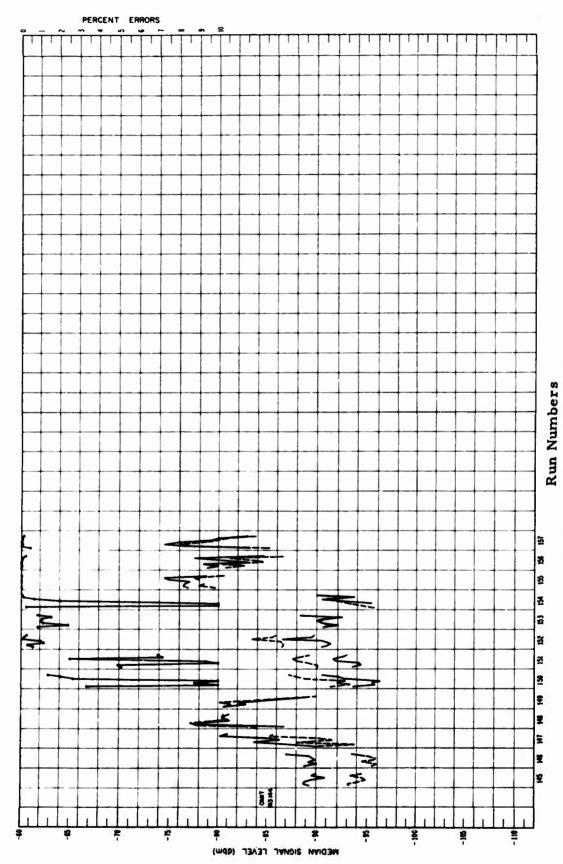


Figure 35. Medians and error rates for the FDM system.

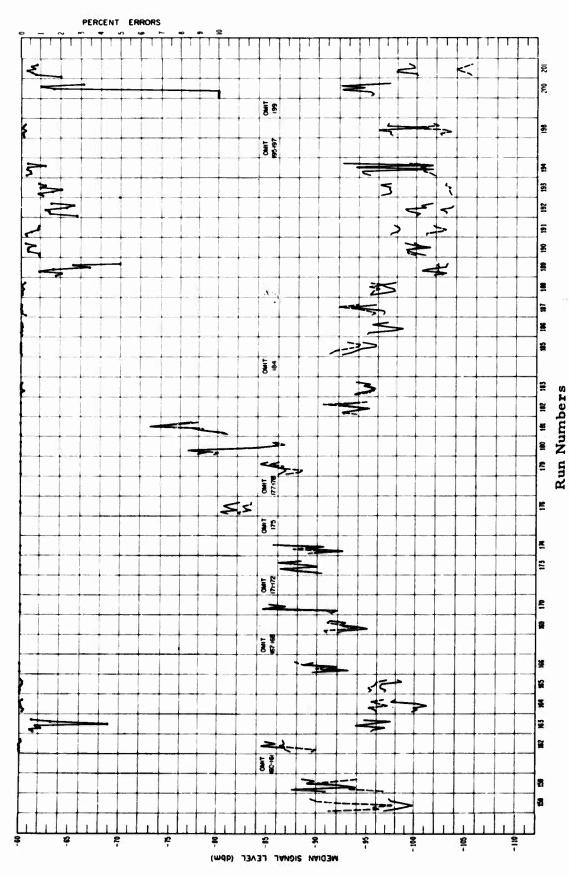


Figure 36. Medians and error rates for the FDM system.

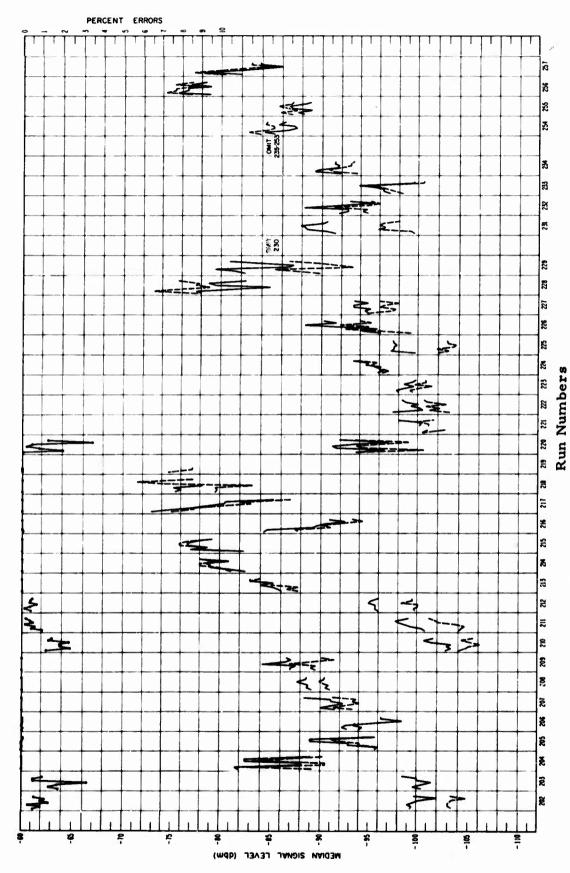
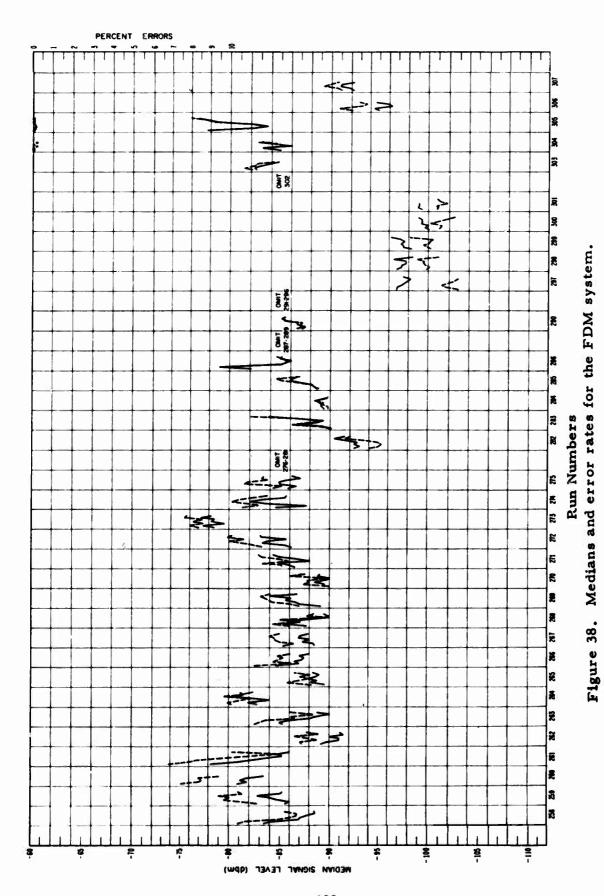
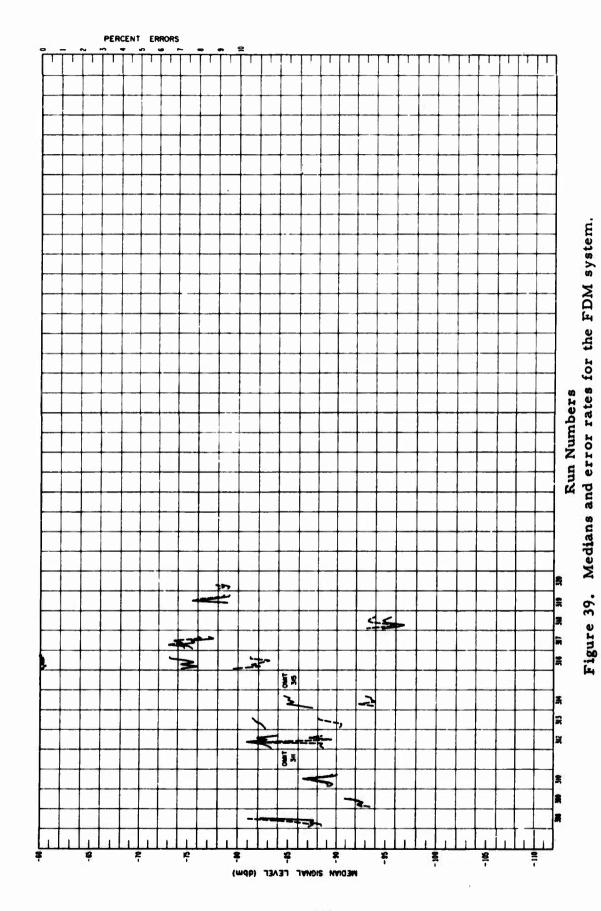


Figure 37. Medians and error rates for the FDM system.

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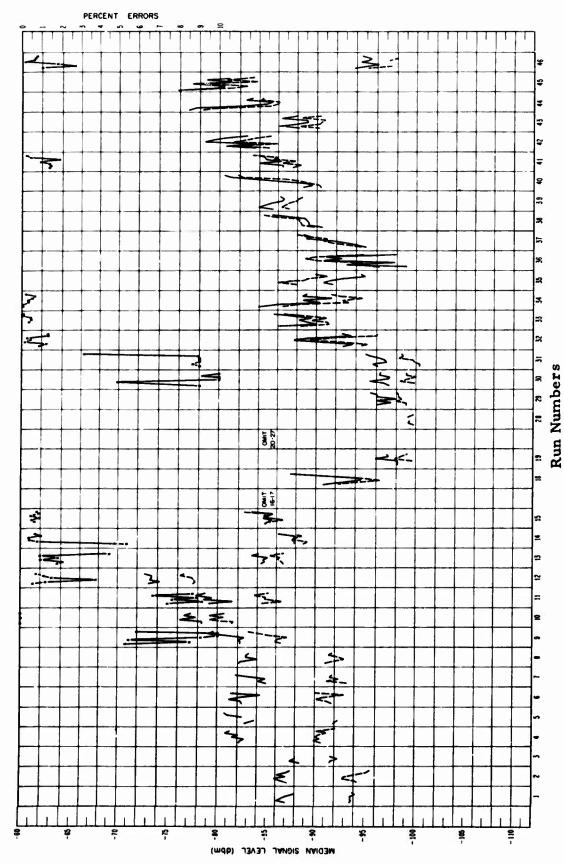
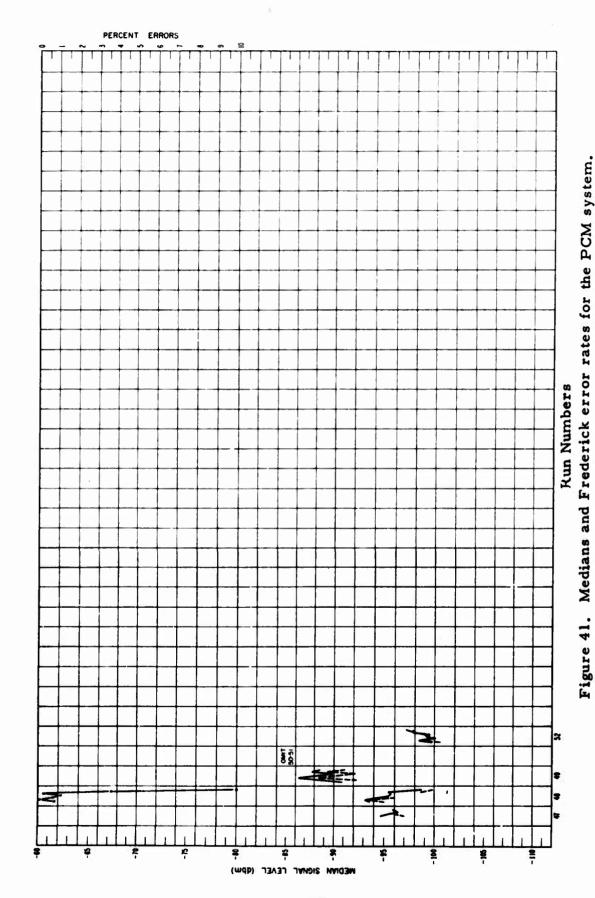


Figure 40. Medians and Frederick error rates for the PCM system.



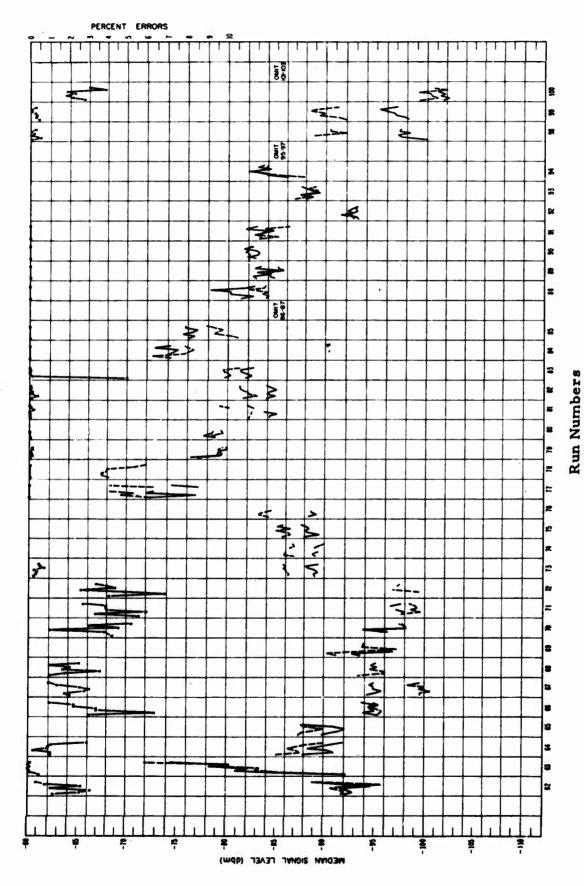
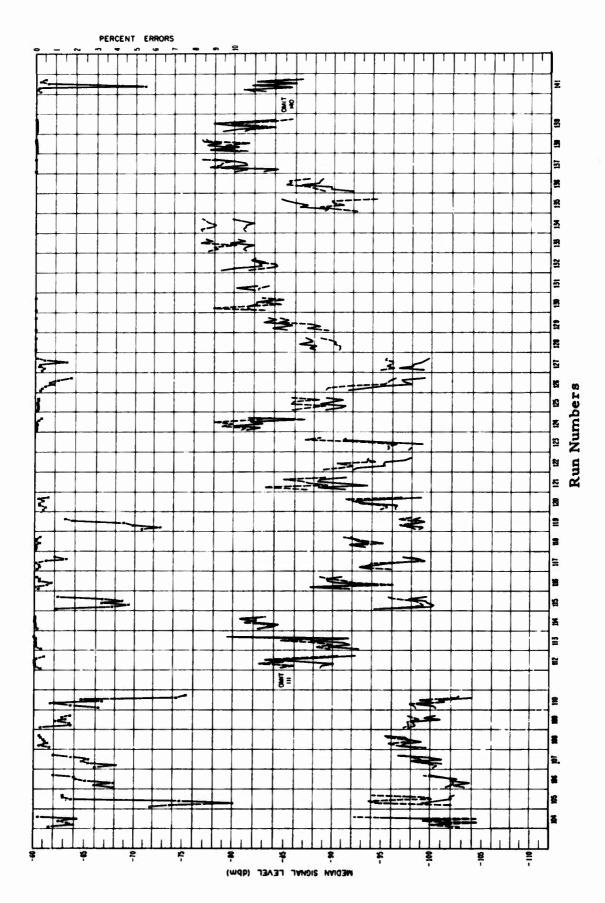
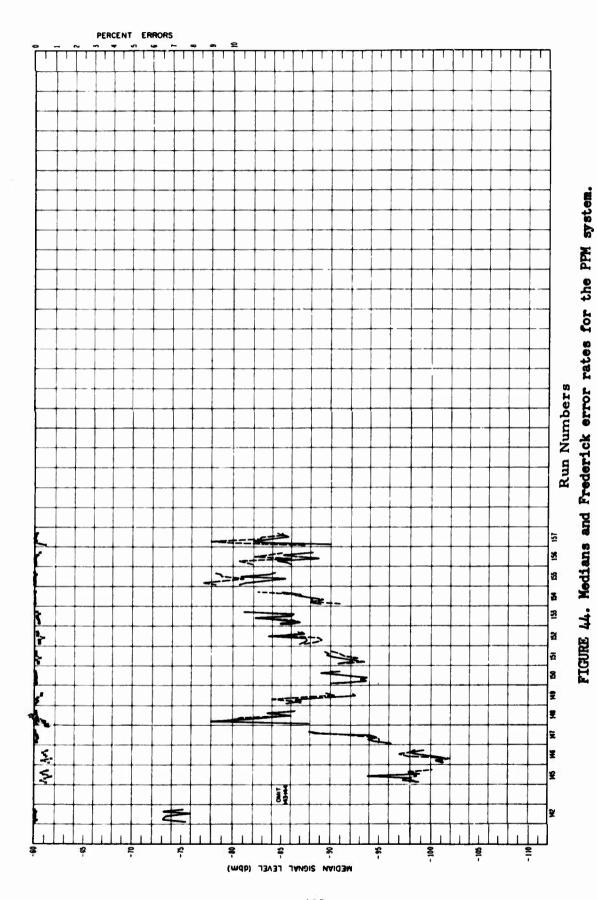


FIGURE 42. Medians and Frederick error rates for the PPM system.









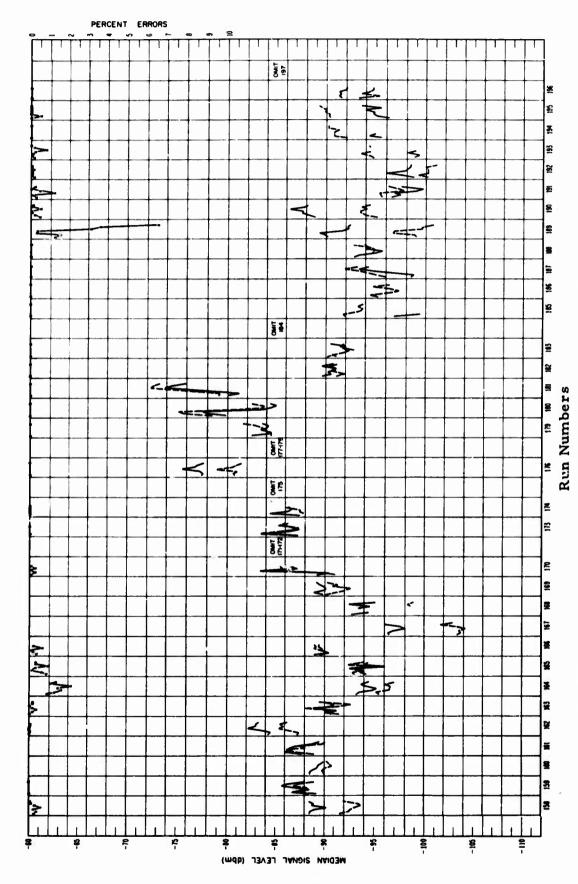


FIGURE 45. Medians and Frederick error rates for the & Mod system

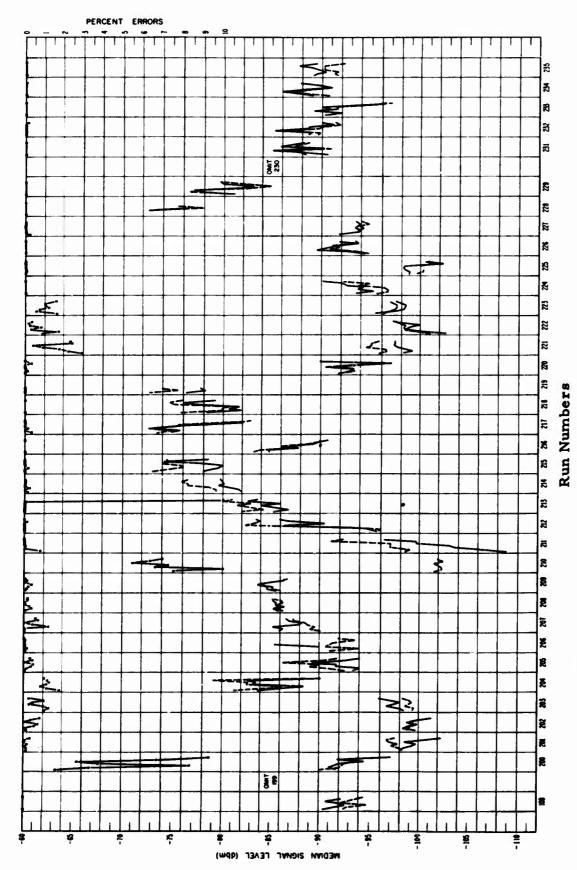


FIGURE 46. Medians and Frederick error rates for the A Mod system.

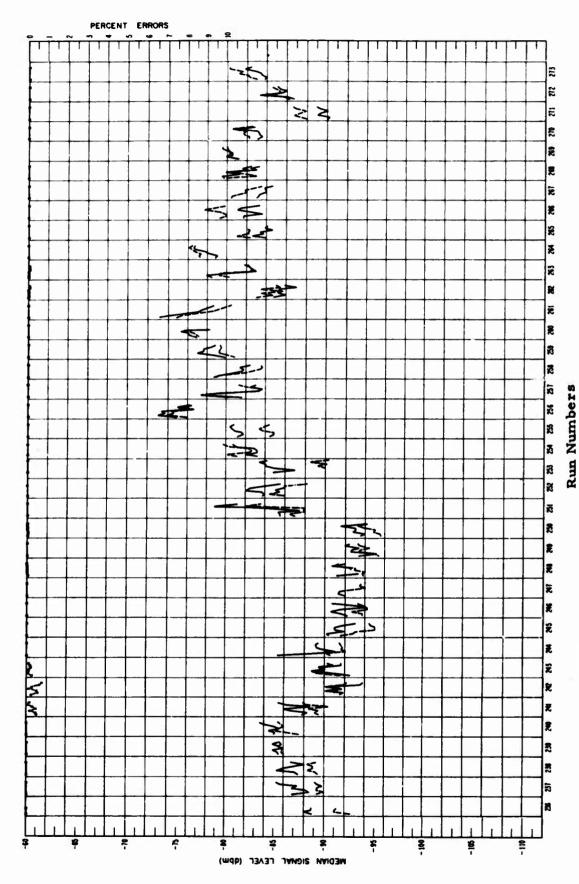


FIGURE 47. Medians and Frederick error rates for the Δ Mod system

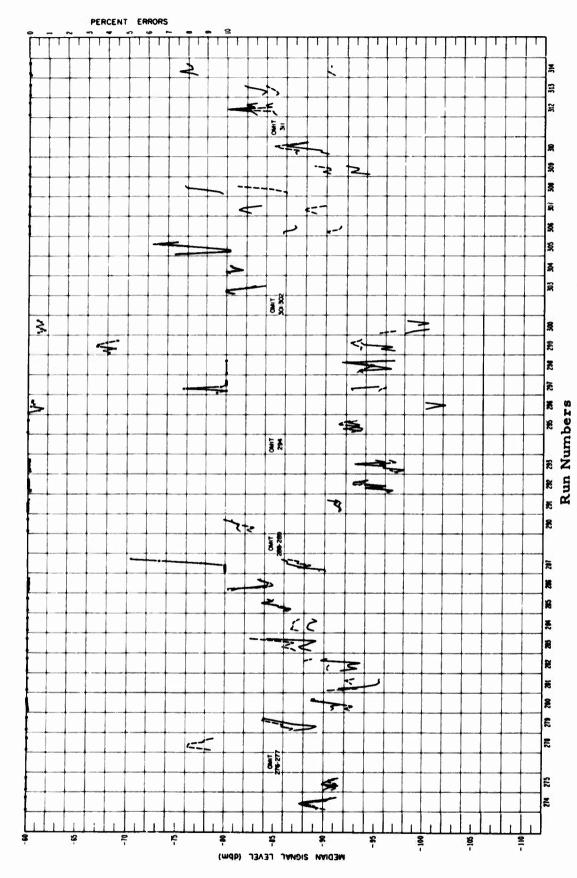


FIGURE 48. Medians and Frederick error rates for the A Mod system.

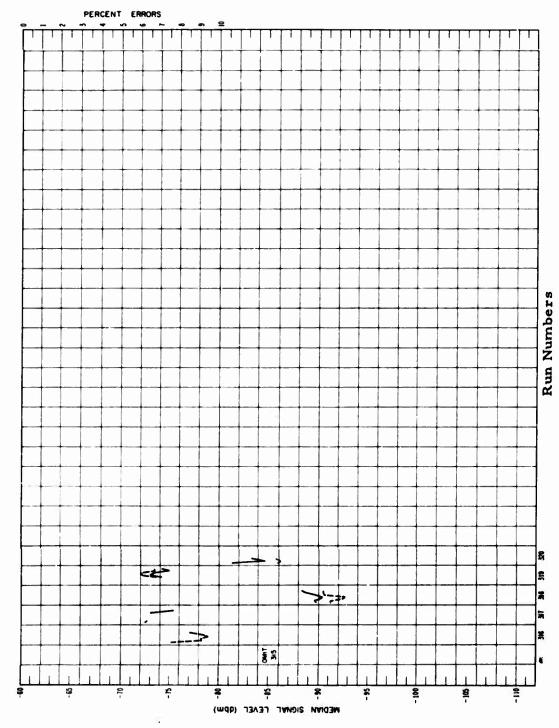


FIGURE 49. Medians and Frederick error rates for the A Mod system.

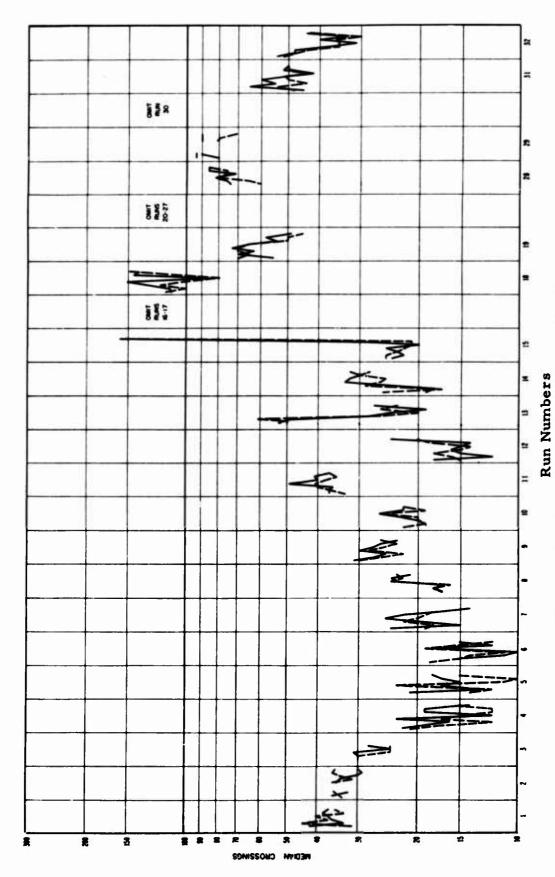
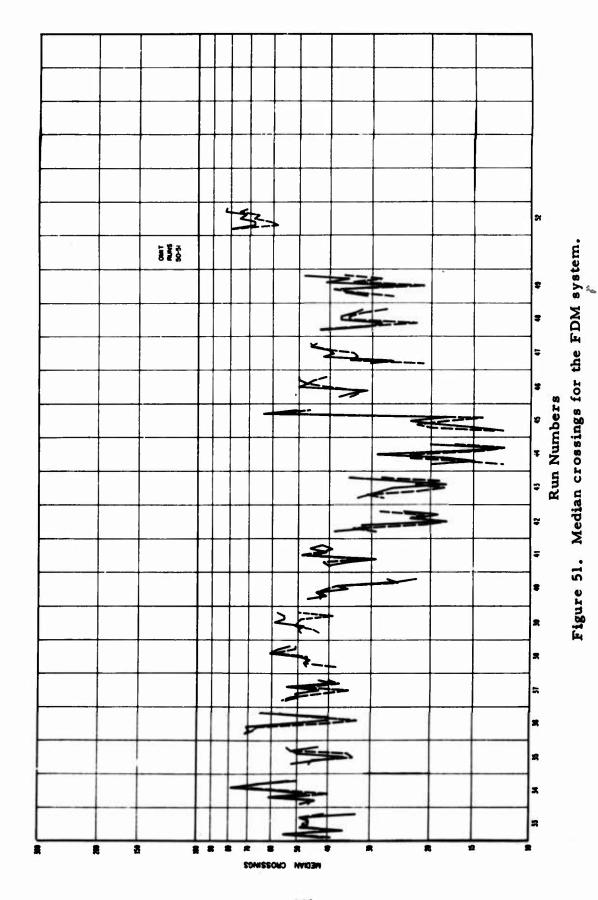


Figure 50. Median crossings for the FDM system.



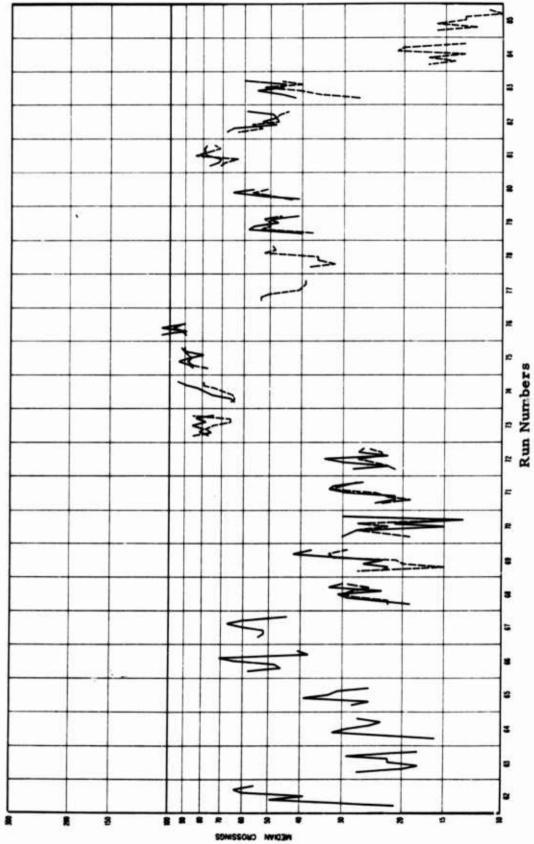


Figure 52. Median crossings for the FDM system.

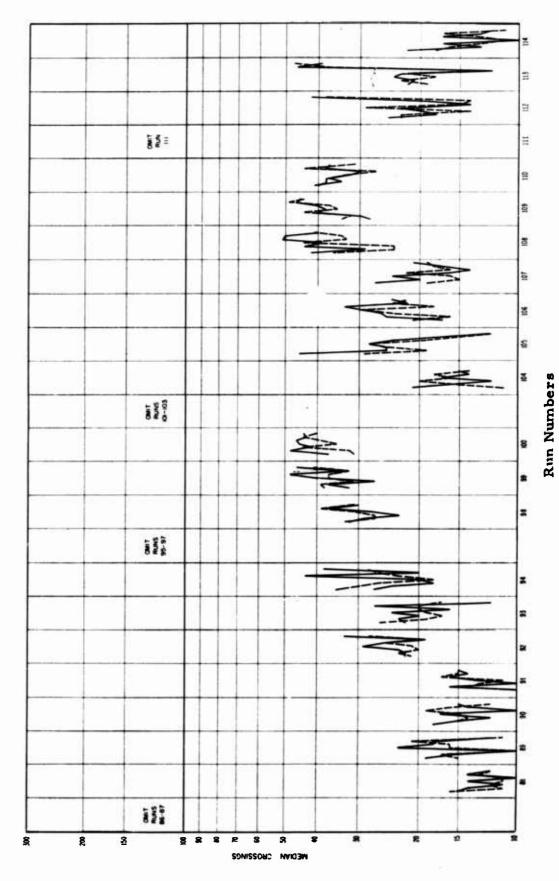


Figure 53. Median crossings for the FDM system.

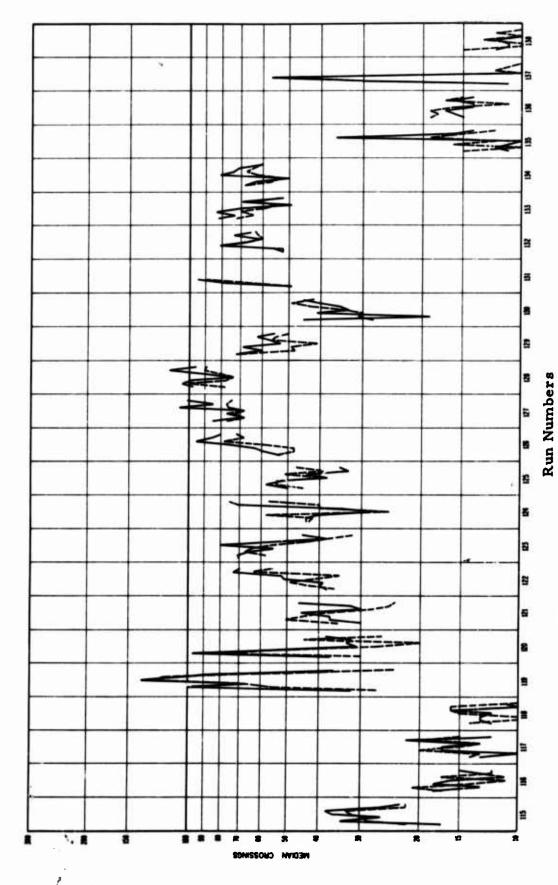
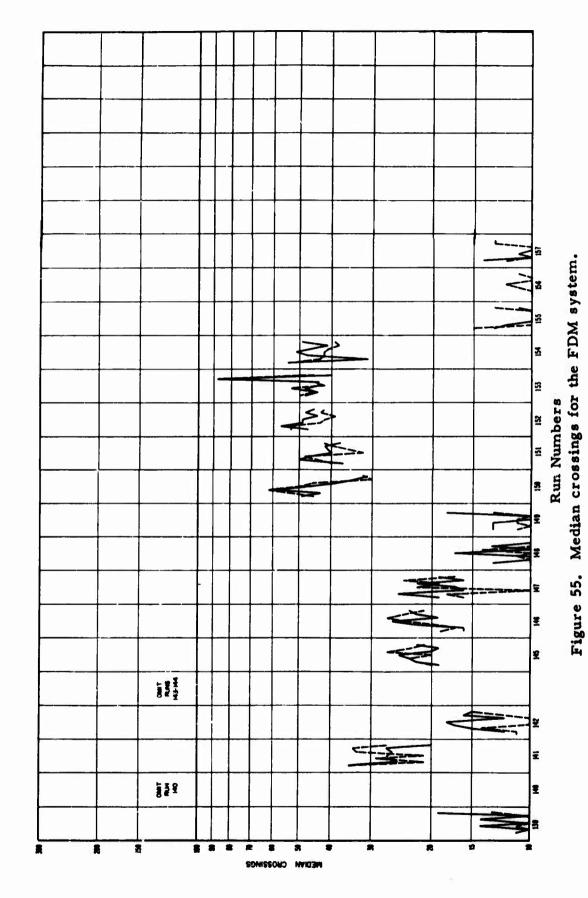


Figure 54. Median crossings for the FDM system.



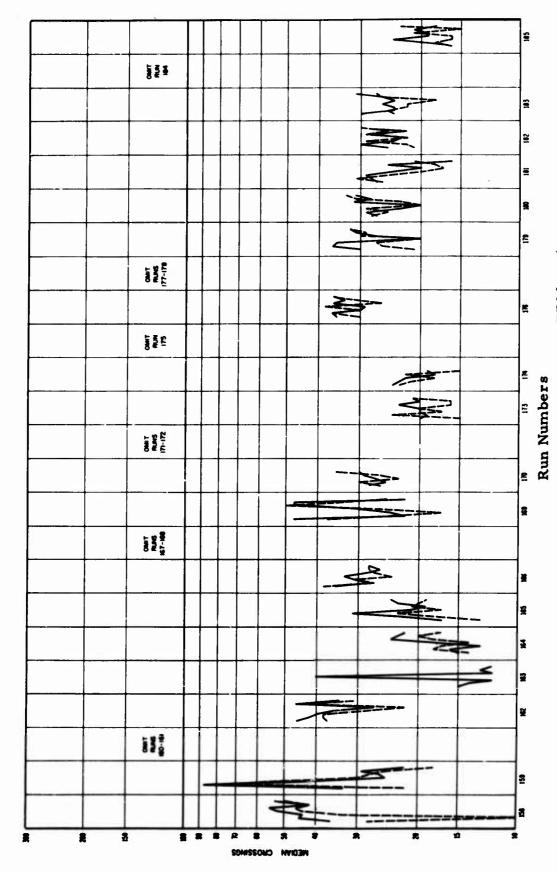
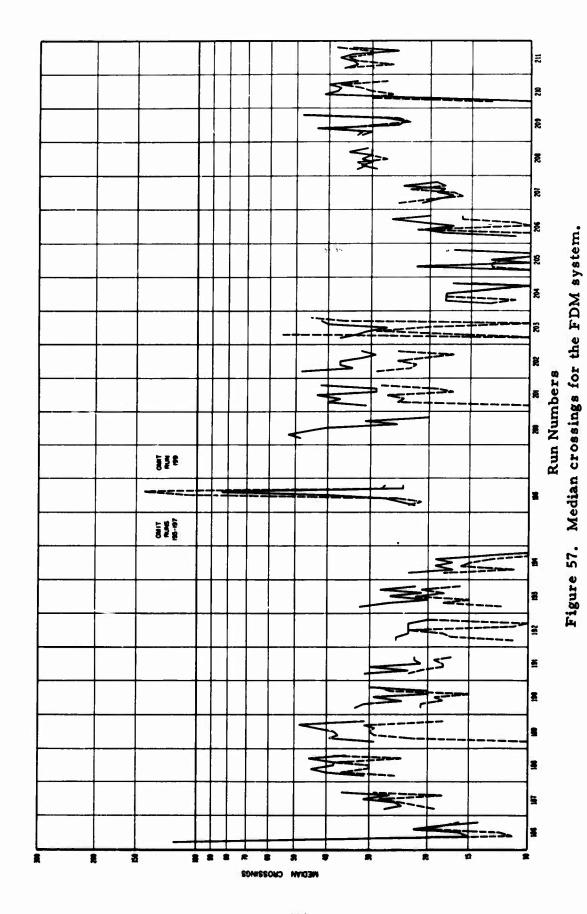


Figure 56. Median crossings for the FDM system.



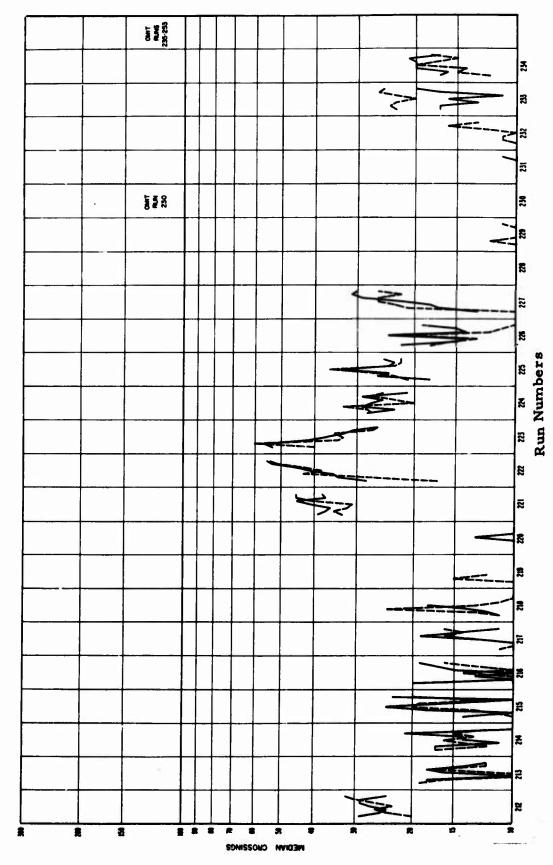
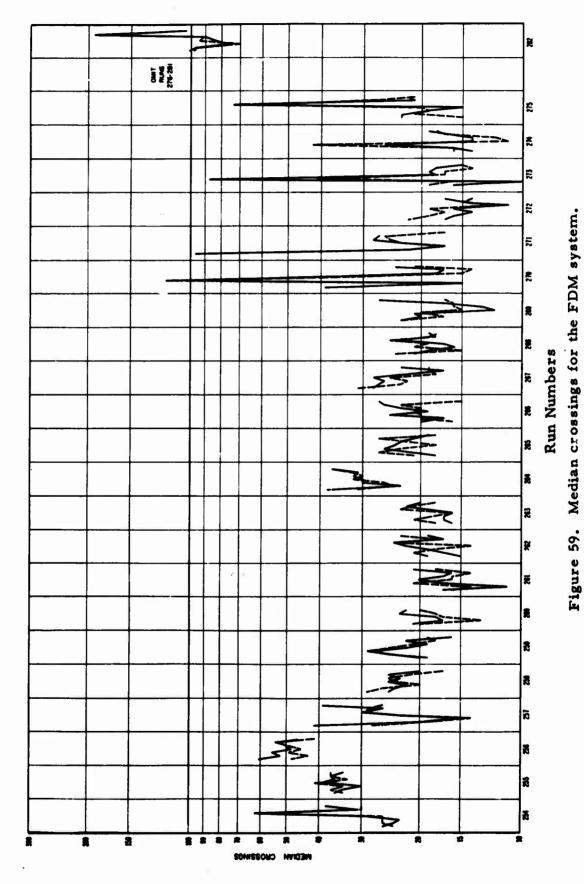
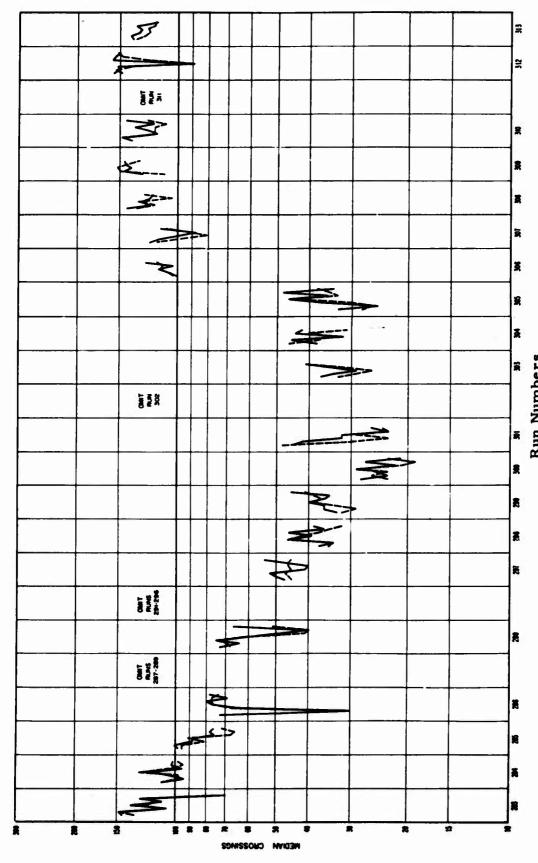


Figure 58. Median crossings for the FDM system.





Run Numbers Figure 60. Median crossings for the FDM system.

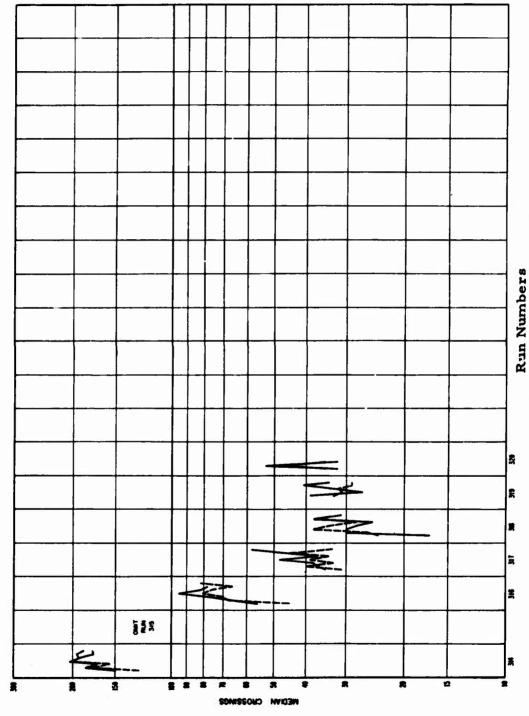


Figure 61. Median crossings for the FDM system.

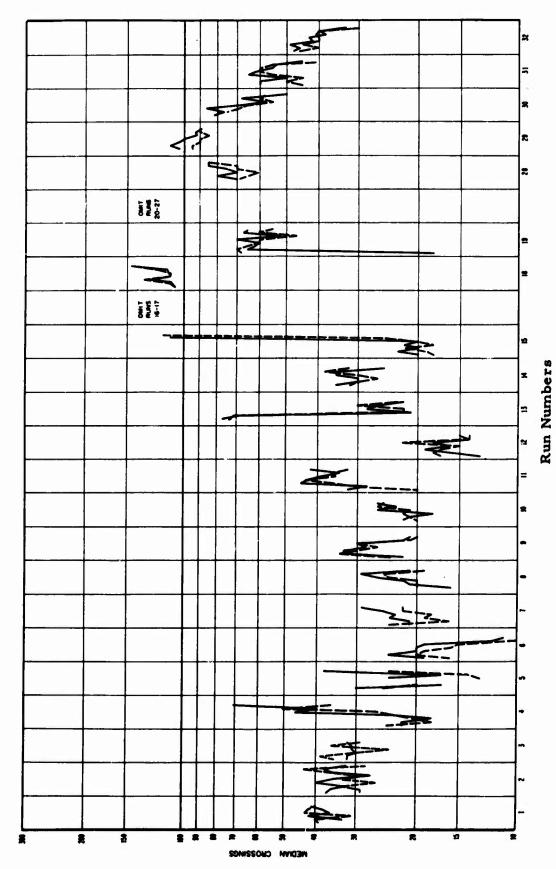
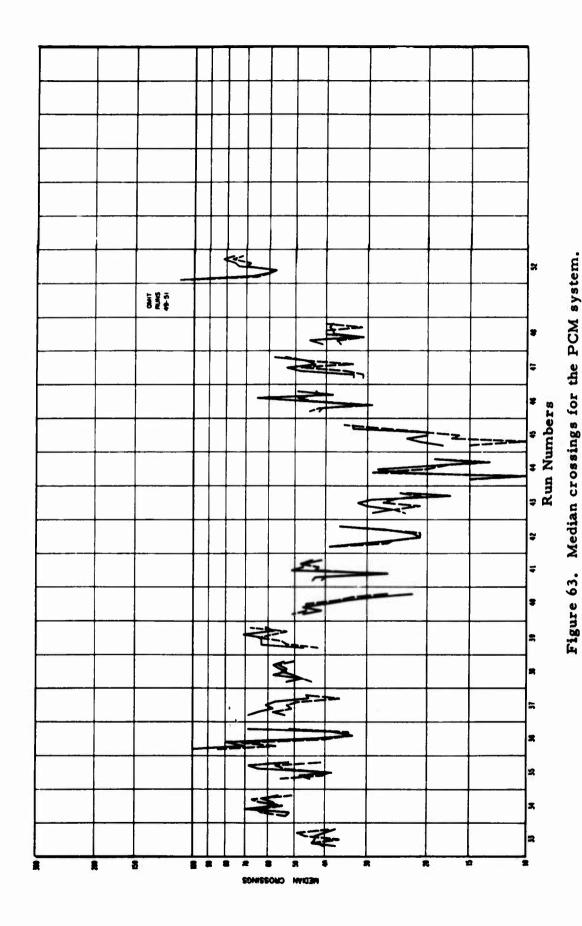


Figure 62. Median crossings for the PCM system.



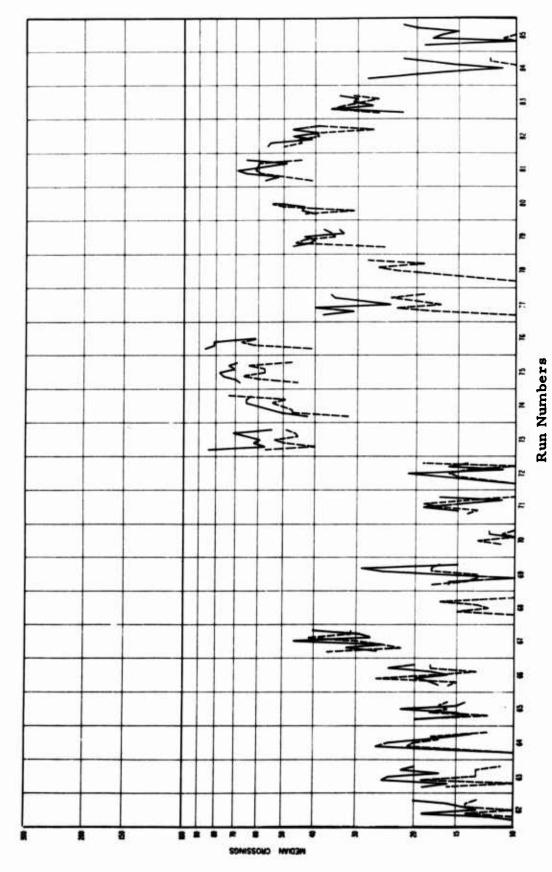


FIGURE 64. Median crossings for the PPM system.

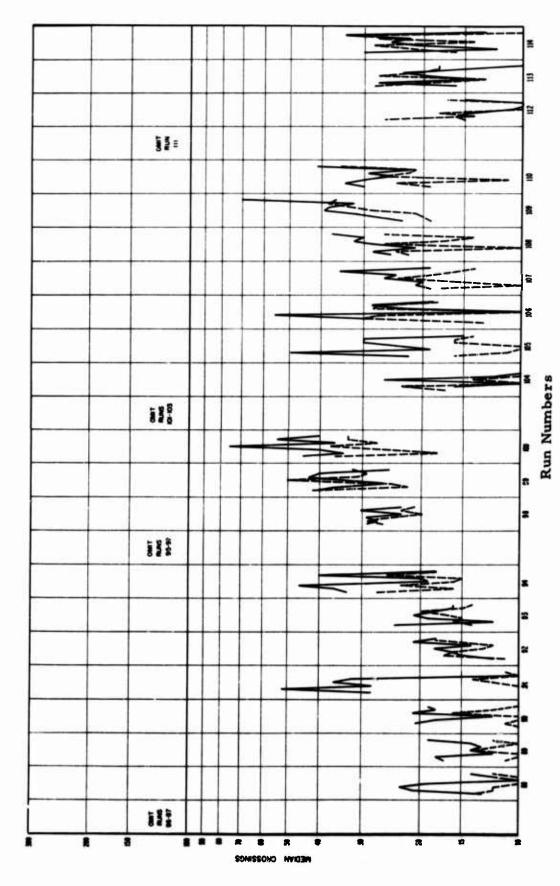


FIGURE 65. Median crossings for the PPM system.

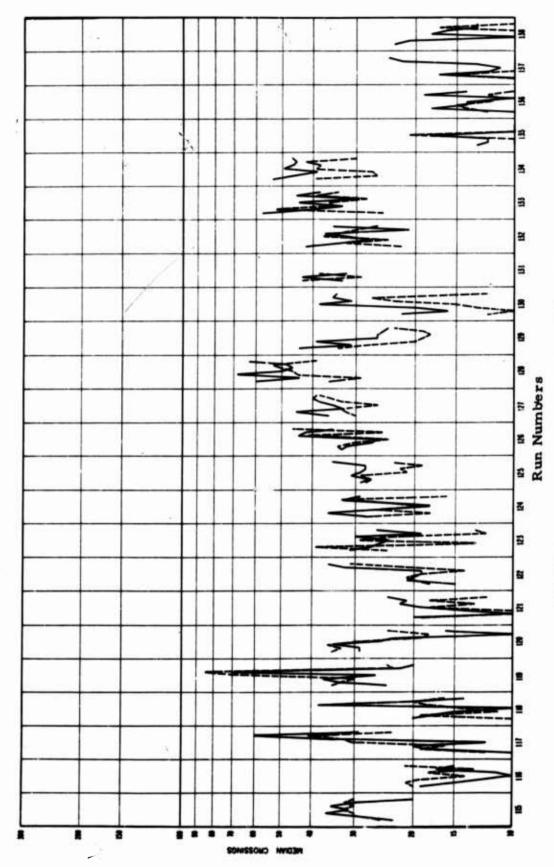
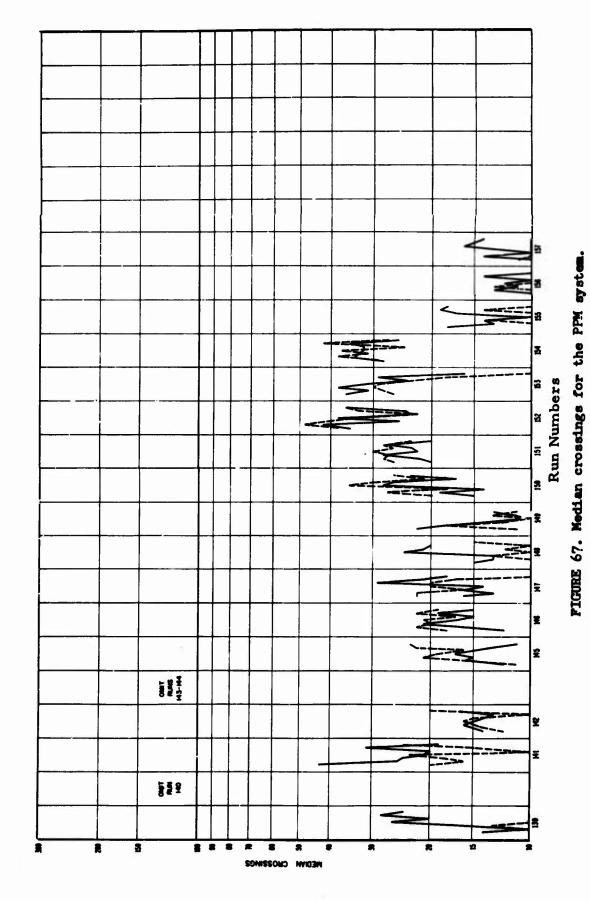


FIGURE 66. Median crossings for the PPM system.



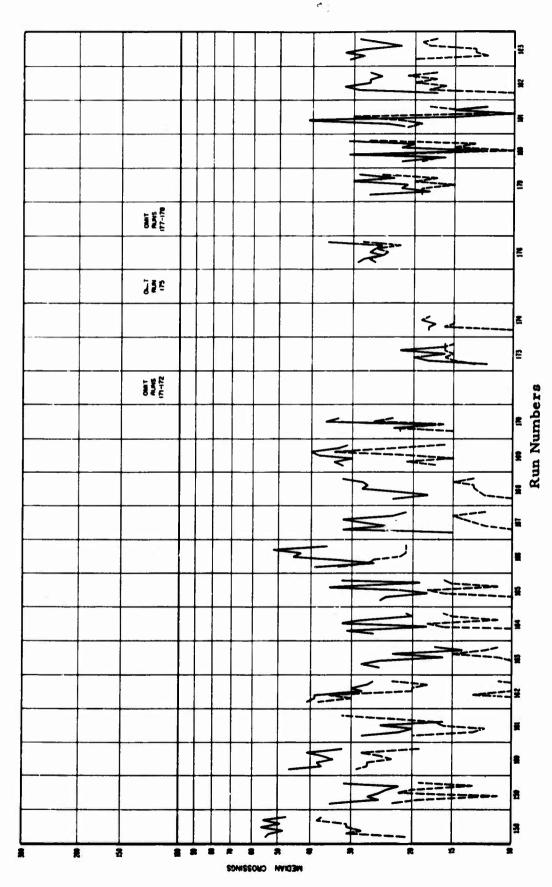
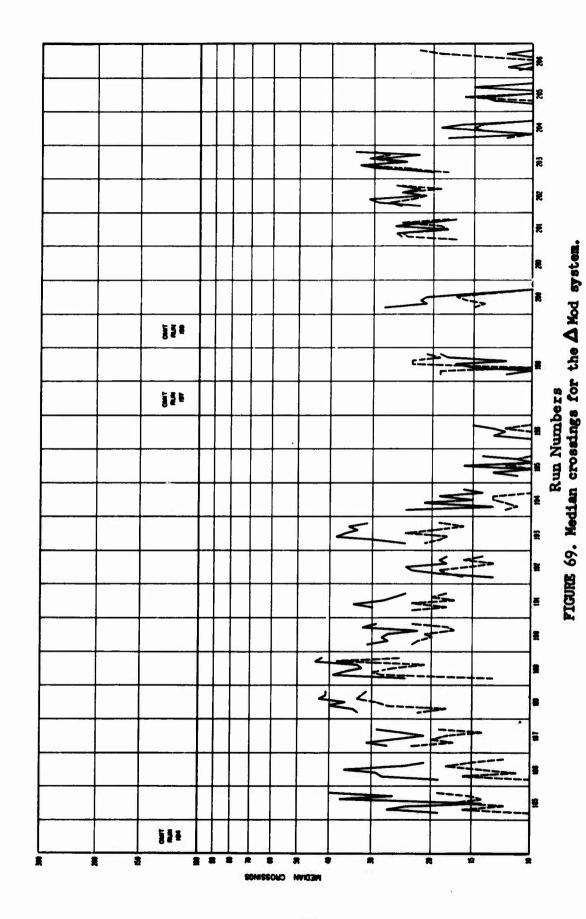


FIGURE 68. Median crossings for the A Mod system.



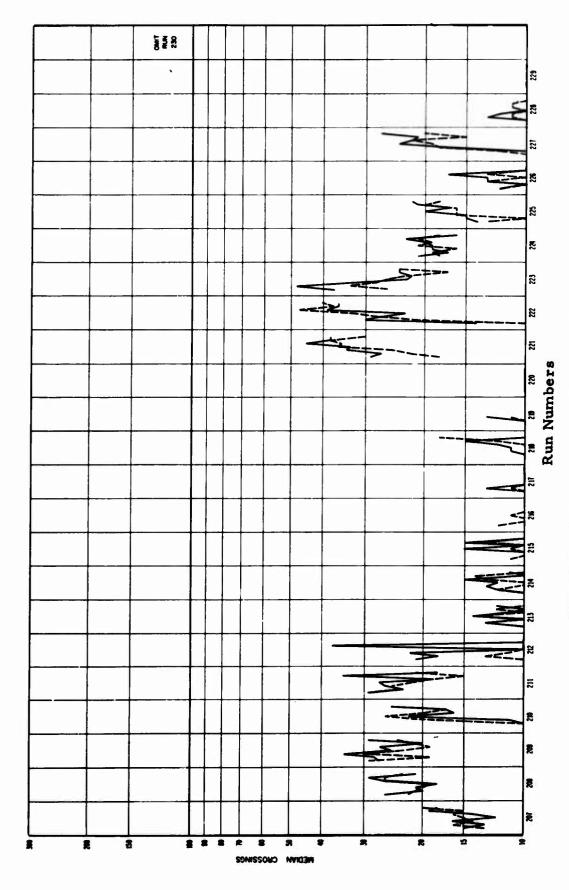


FIGURE 70. Median crossings for the & Mod system.

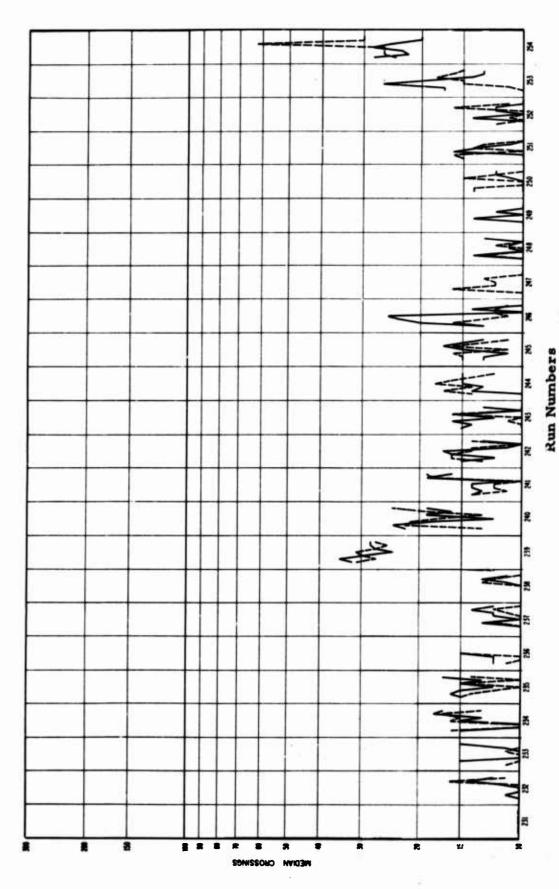


FIGURE 71. Median crossings for the A Mod system.

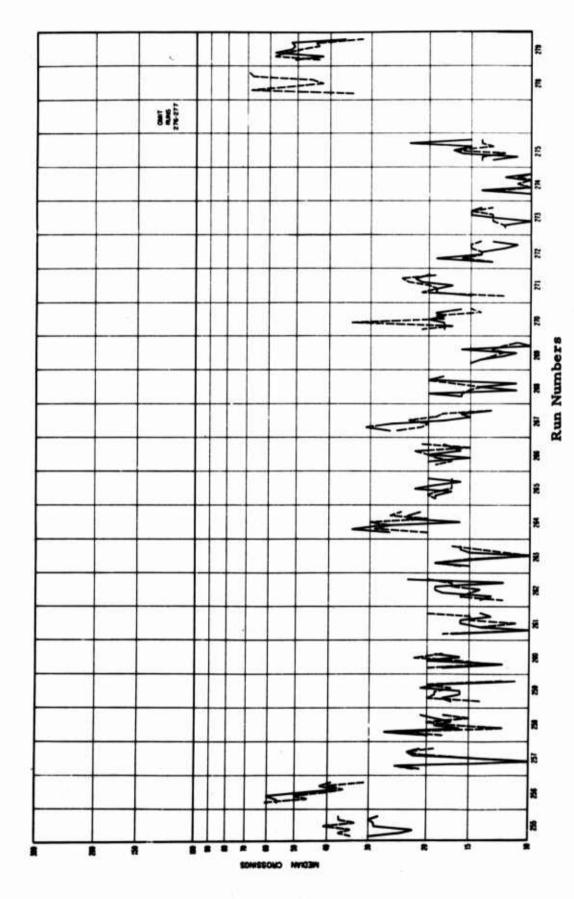


FIGURE 72. Median crossings for the A Mod System.

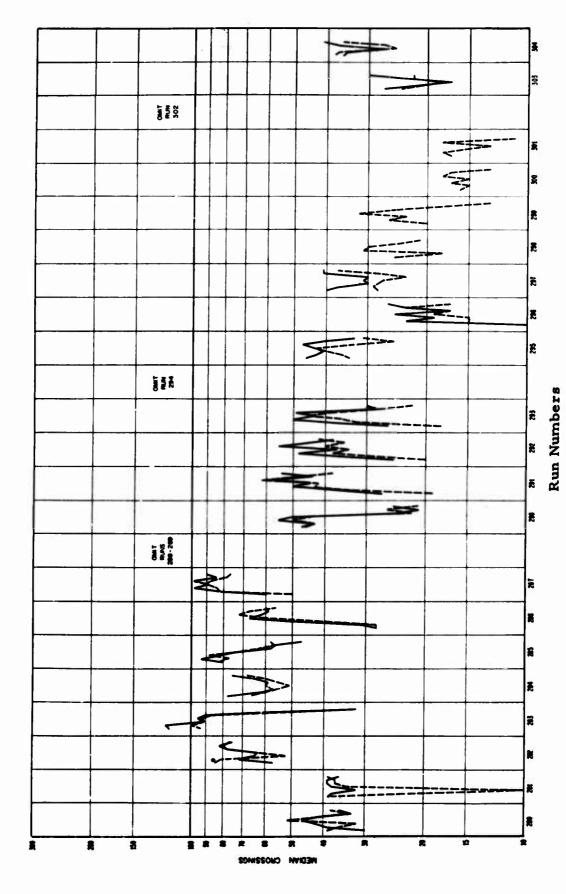


FIGURE 73. Median crossings for the & Mod system.

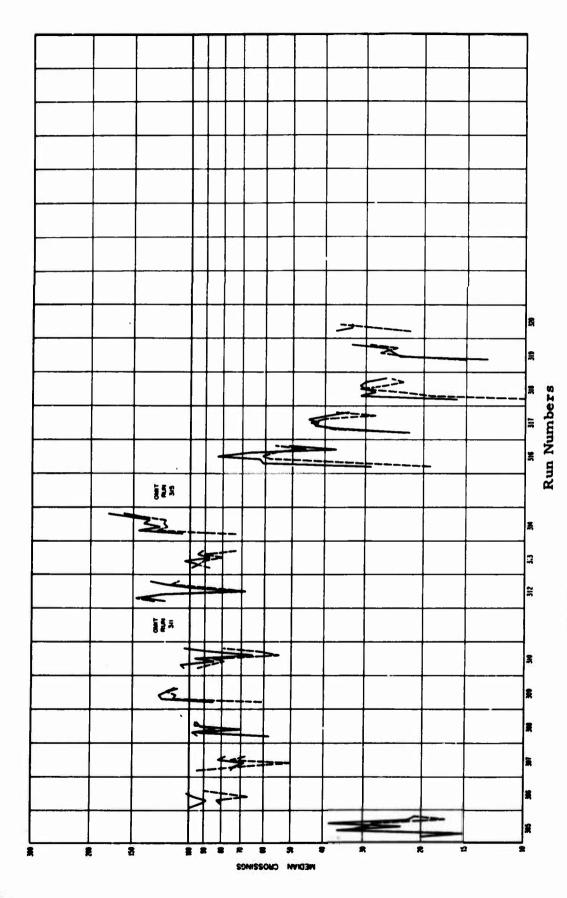


FIGURE 74. Median crossings for the & Mod system.

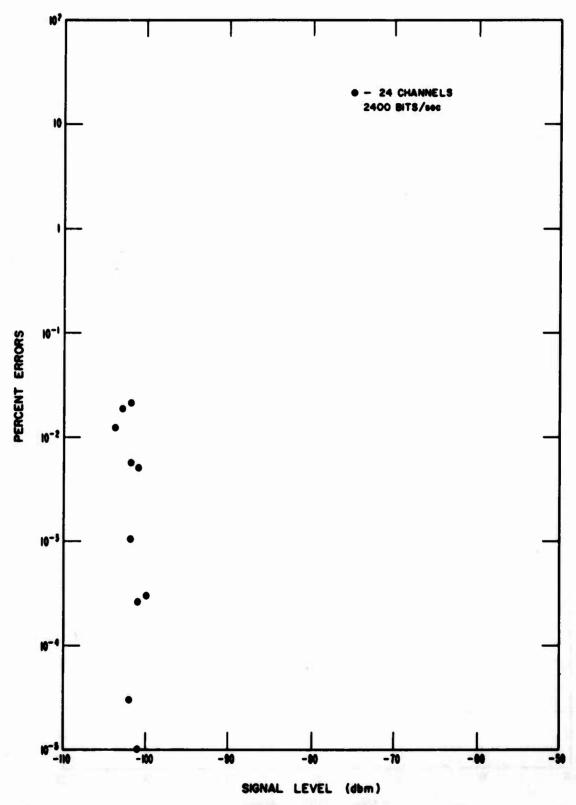
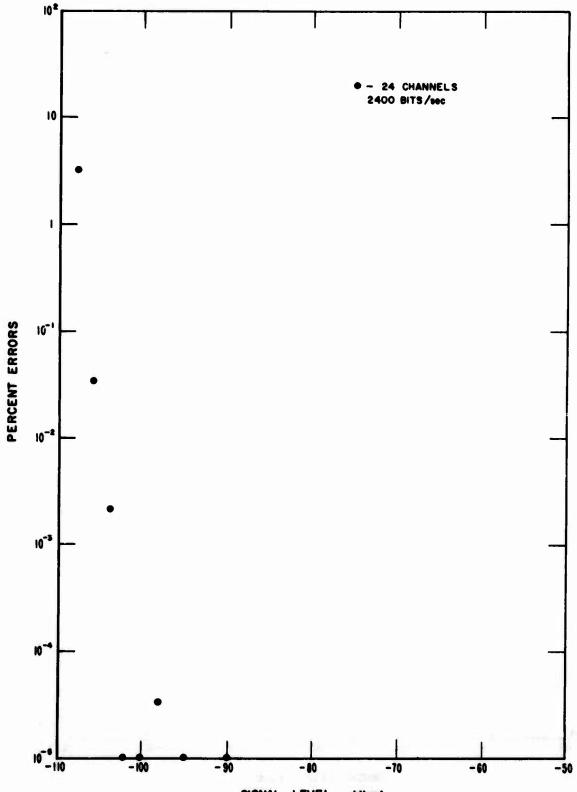


Figure 75. Back-to-back FDM Frederick.



SIGNAL LEVEL (dbm)
Figure 76. Back-to-back FDM GSC-4.

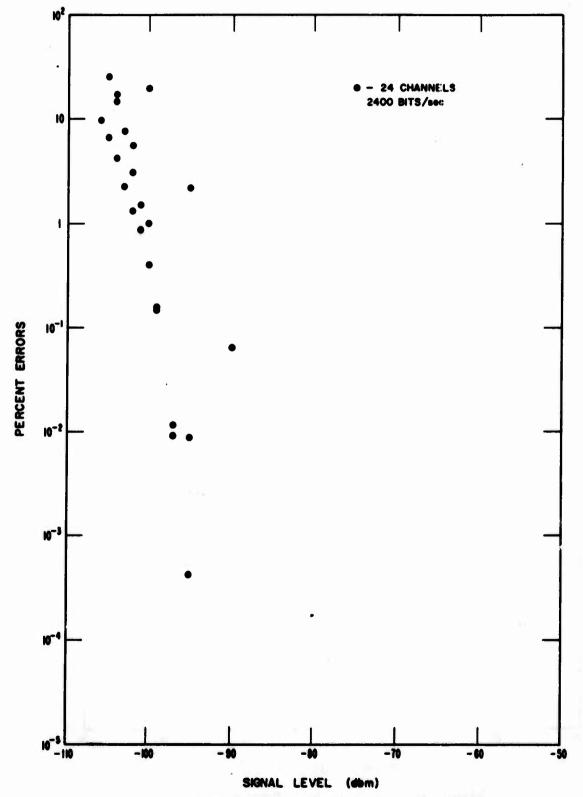


Figure 77. Back-to-back PCM Frederick.

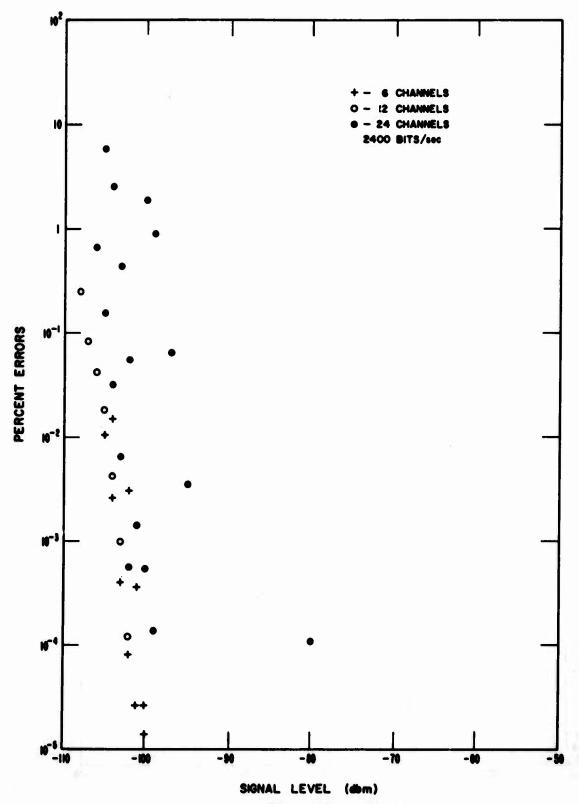


Figure 78. Back-to-back PCM GSC-4.

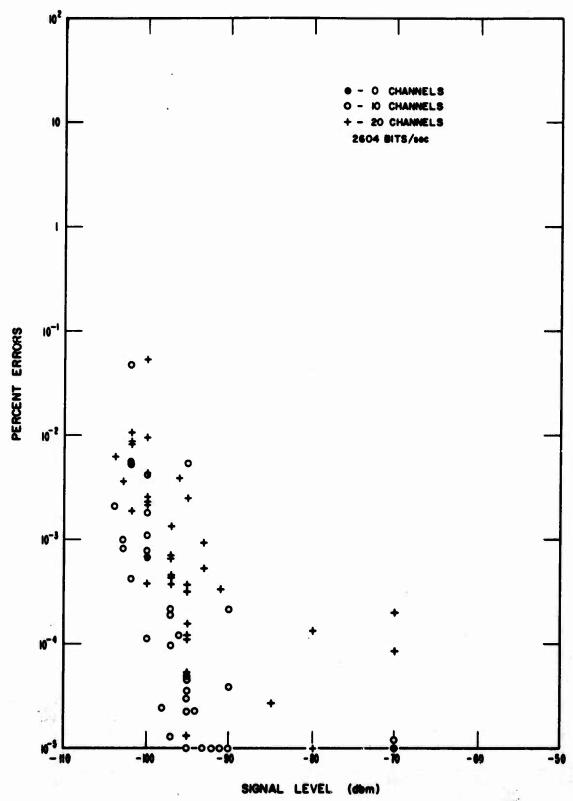


Figure 79. Back-to-back PPM Frederick.

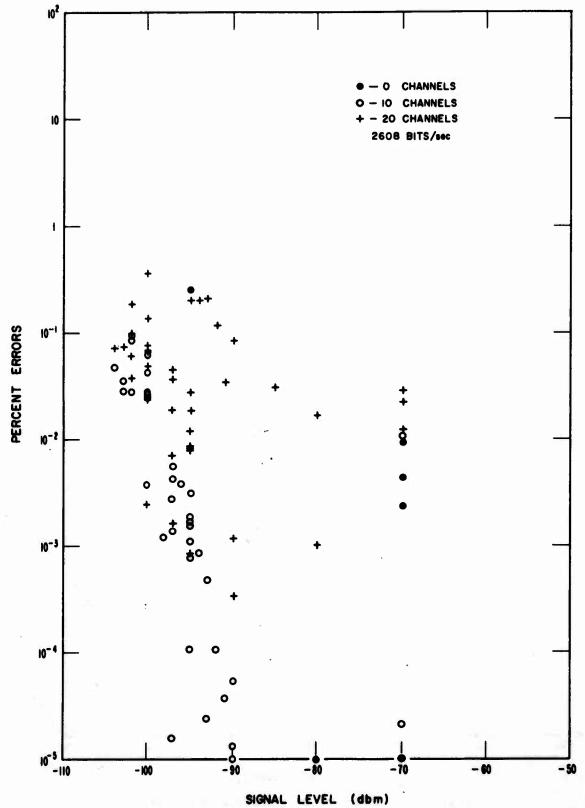


Figure 80. Back-to-back PPM GSC-4.

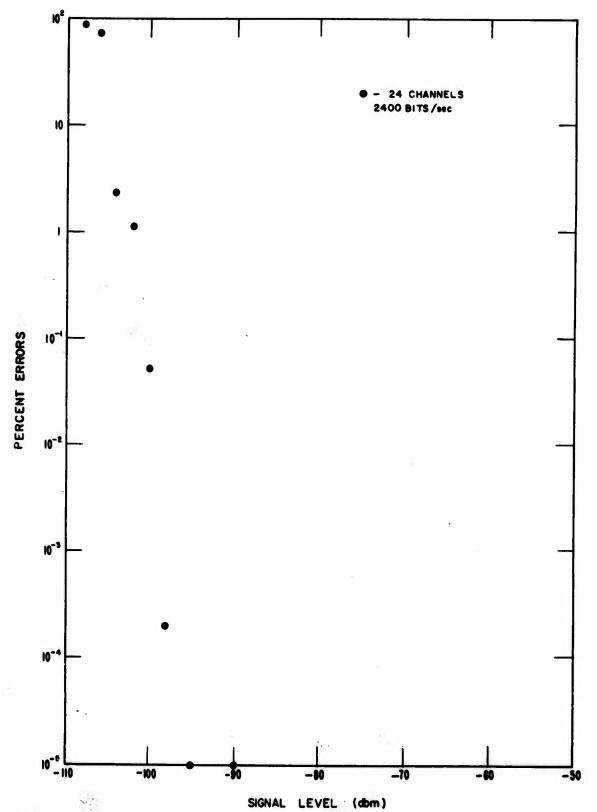


Figure 81. Back-to-back & Mod. Frederick.

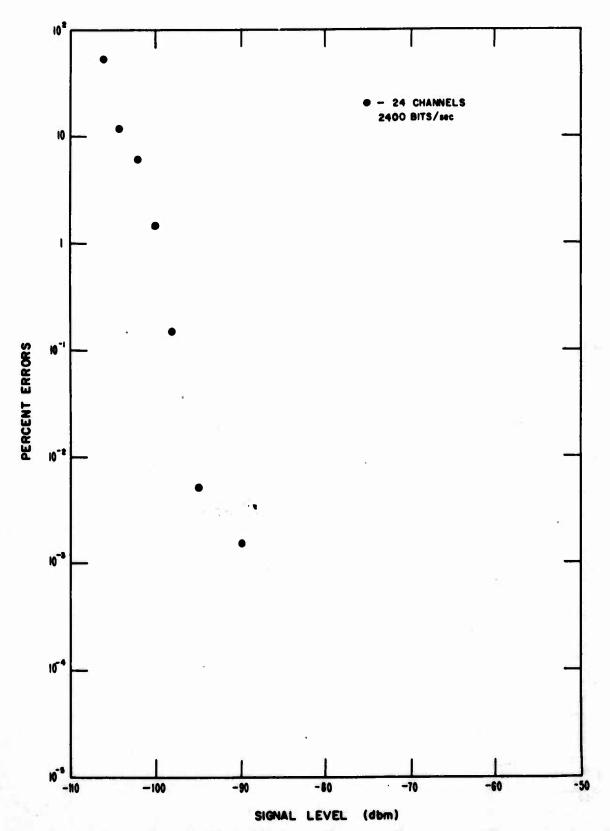


Figure 82. Back-to-back Δ Mod. GSC-4.

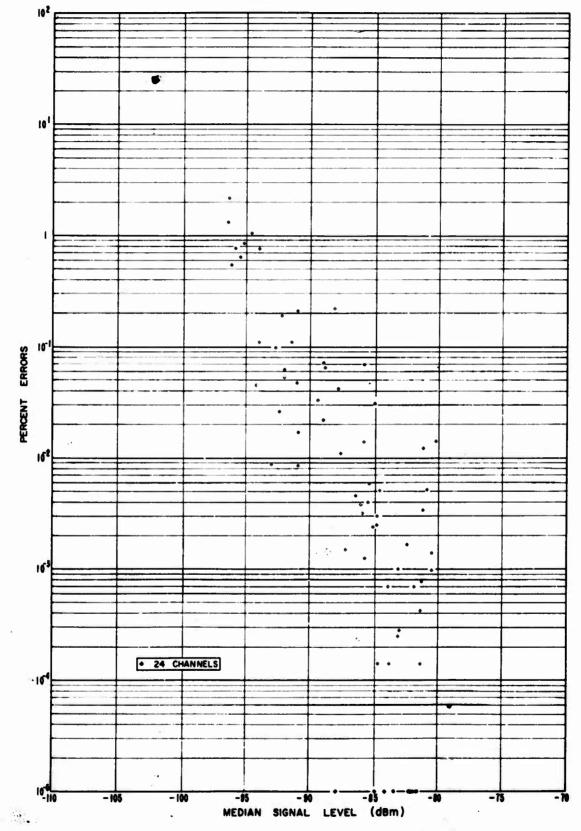
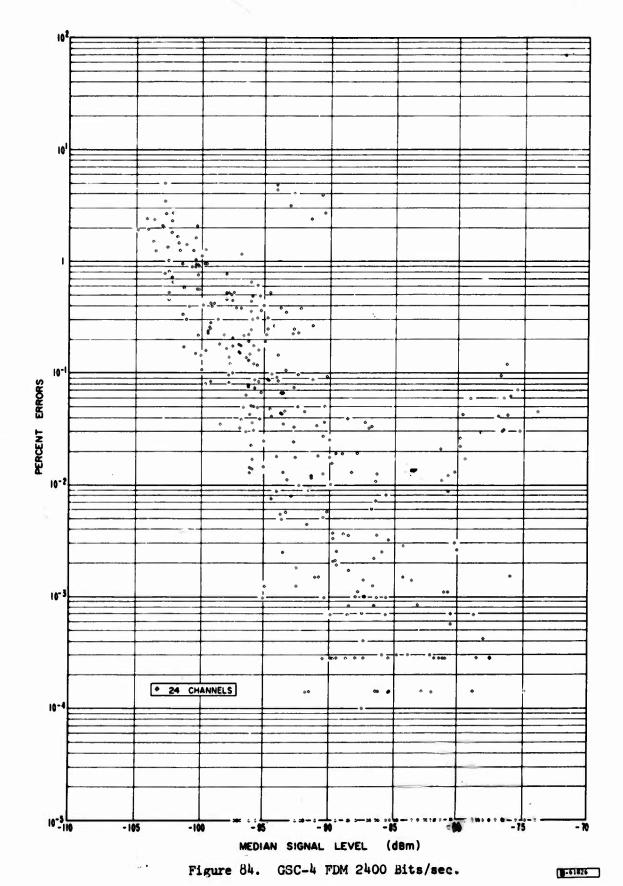
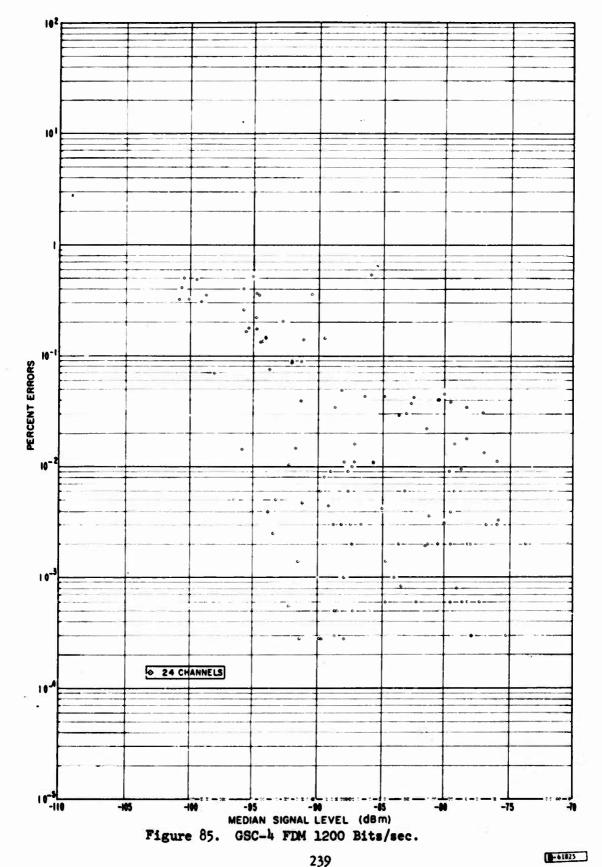
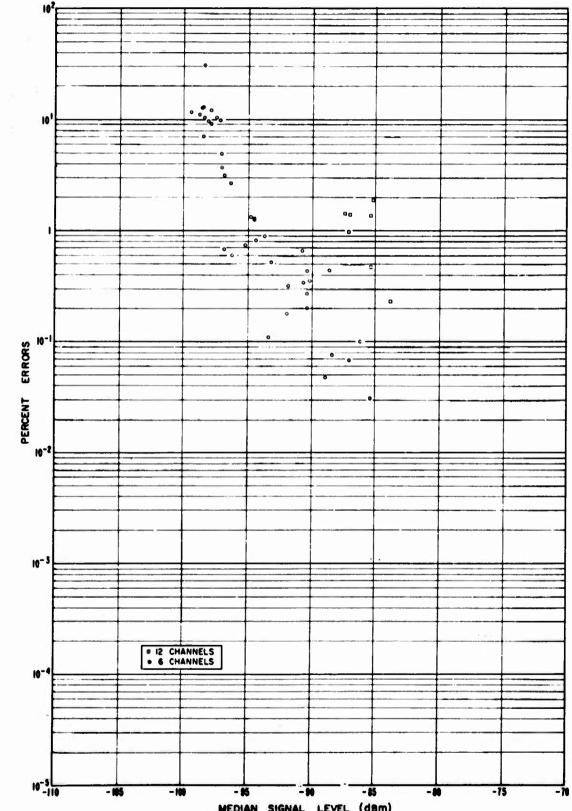


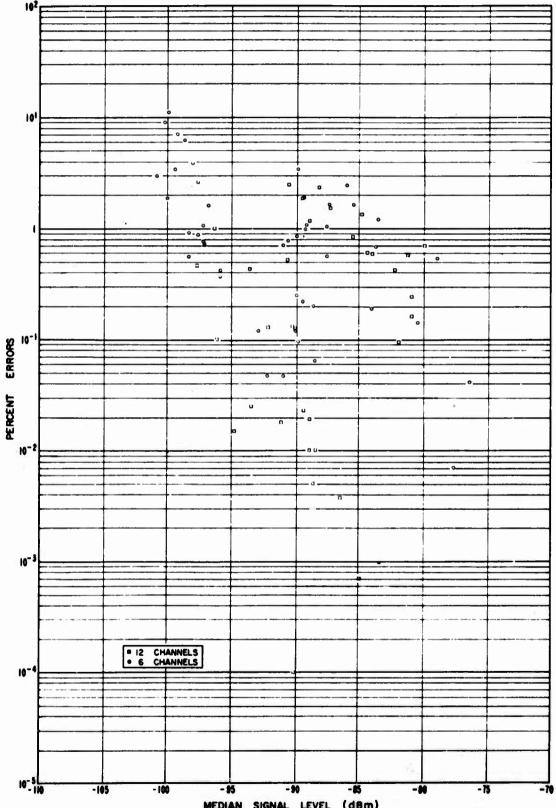
Figure 83. Frederick FDM 2400 Bits/sec. 237



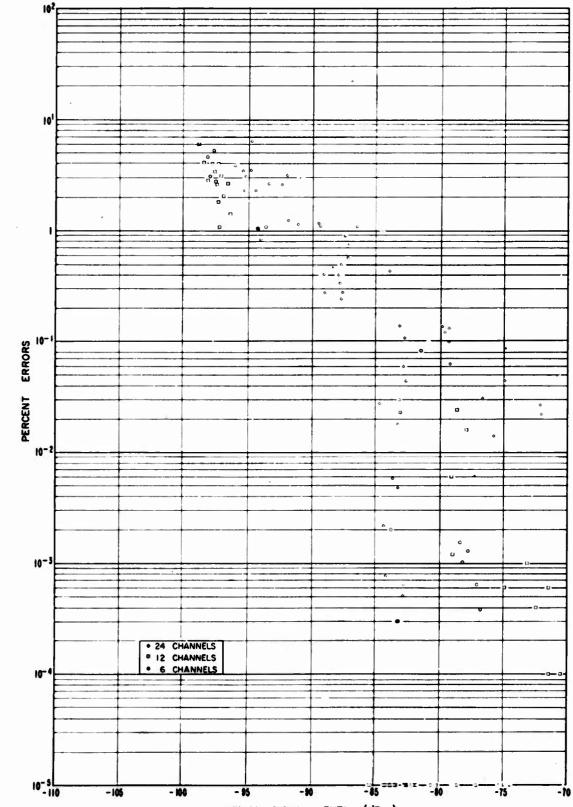




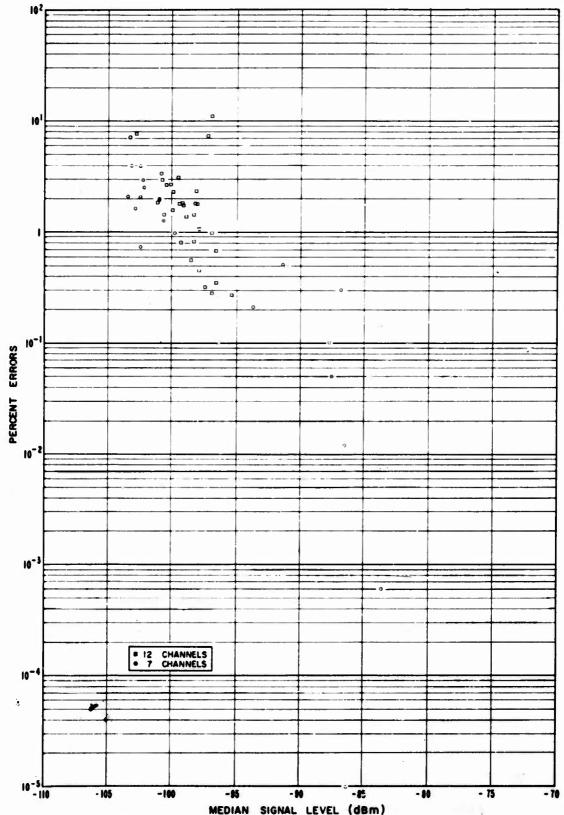
MEDIAN SIGNAL LEVEL (dBm)
Figure 86. Frederick PCM 2400 Bits/sec.



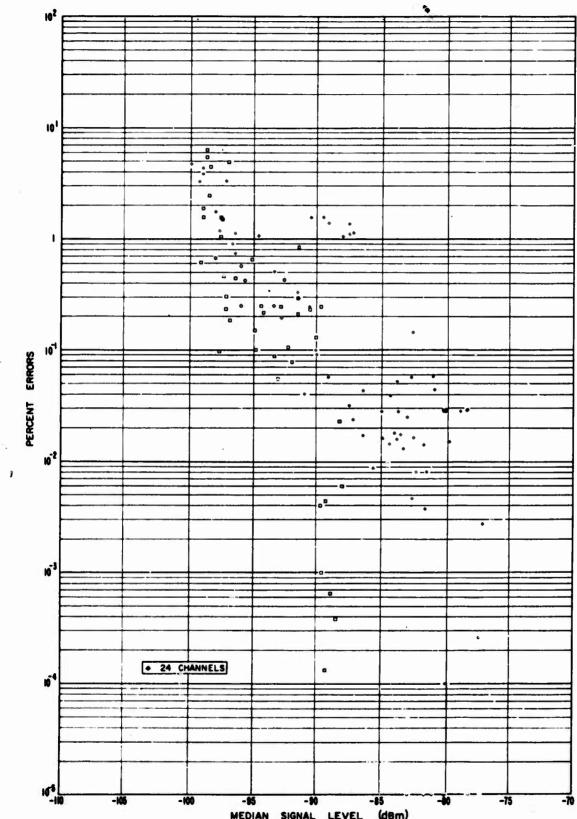
MEDIAN SIGNAL LEVEL (dBm)
Figure 87. GSC-4 PCM 2400 Bits/sec.



MEDIAN SIGNAL LEVEL (dBm)
Figure 88. Frederick PPM 2604 Bits/sec.



MEDIAN SIGNAL LEVEL (d8m)
Figure 89. Frederick PPM 2604 Bits/sec.



MEDIAN SIGNAL LEVEL (dBm)
Figure 90. Frederick PPM 2604 Bits/sec.

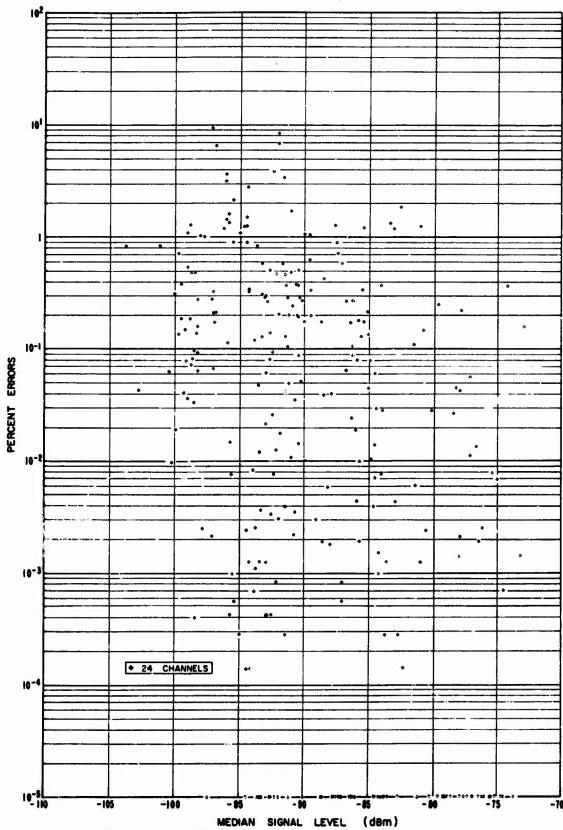
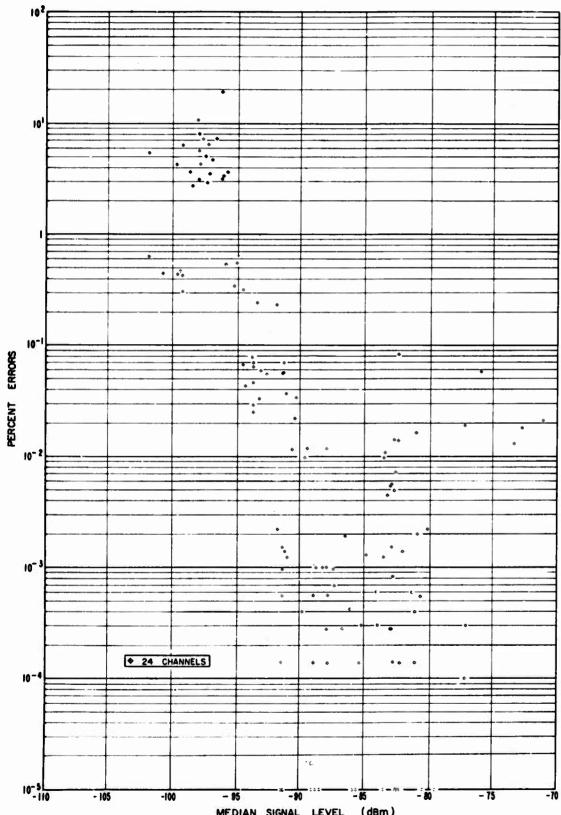


Figure 91. Frederick Δ modulated 2400 Bits/sec.



MEDIAN SIGNAL LEVEL (dBm)
Figure 92. GSC-4 Δ modulated 2400 Bits/sec.

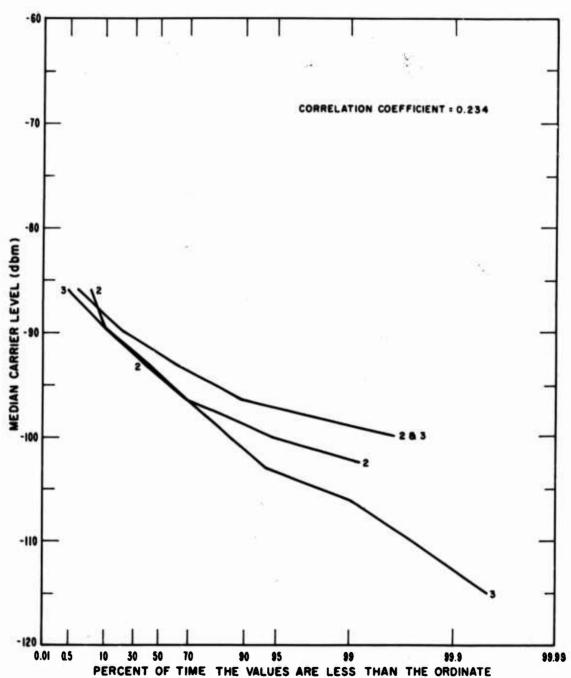


Figure 93. Sample distributions and combined distributions, Run 36, Time 1425-1430, FDM.

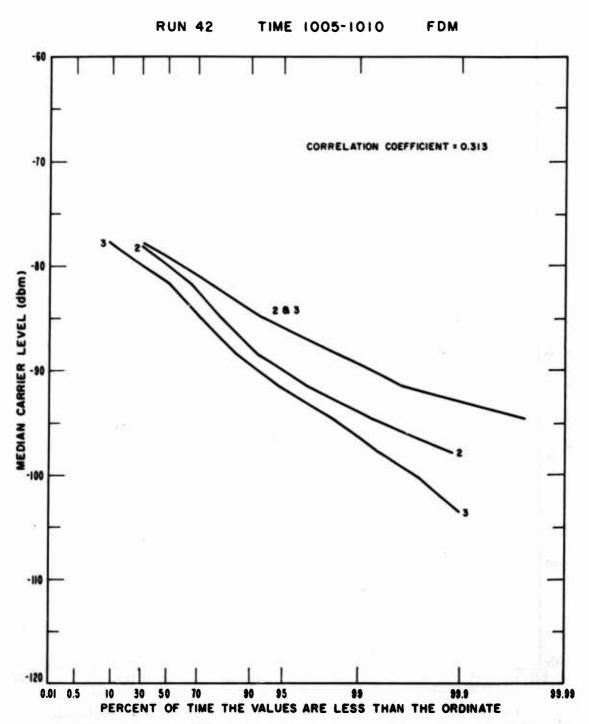


Figure 94. Sample distributions and combined distributions, Run 42, Time 1005-1010, FDM.

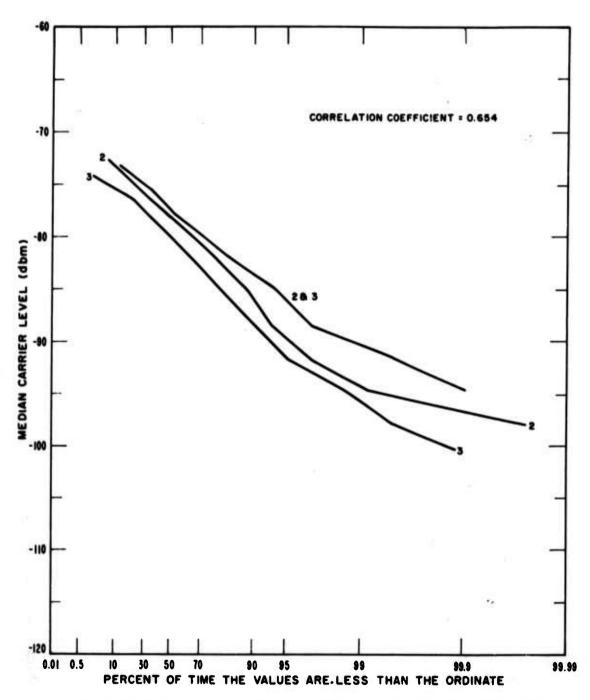


Figure 95. Sample distributions and combined distributions, Run 42, Time 1025-1030, FDM.

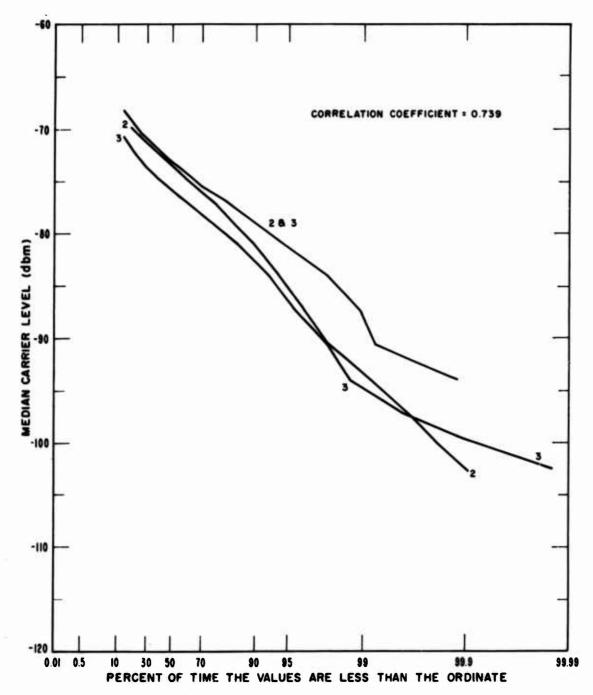


Figure 96. Sample distributions and combined distributions, Run 44, Time 1205-1210, FDM.

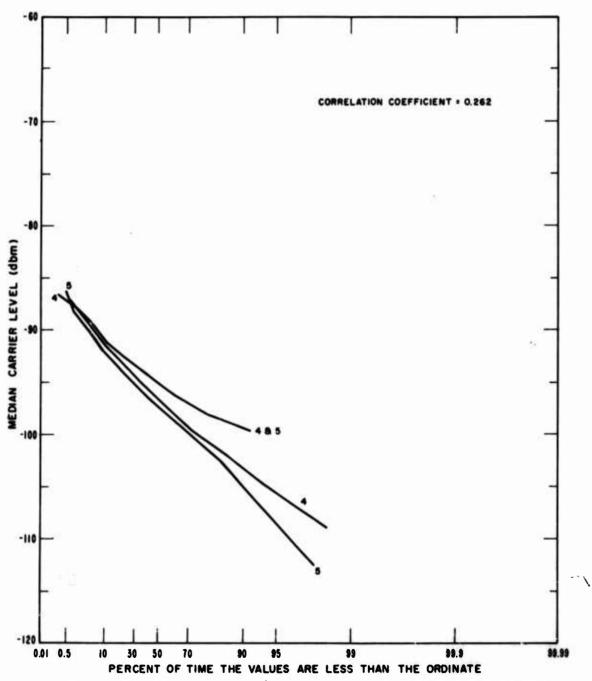


Figure 97. Sample distributions and combined distributions, Run 127, Time 1645-1650, FDM.

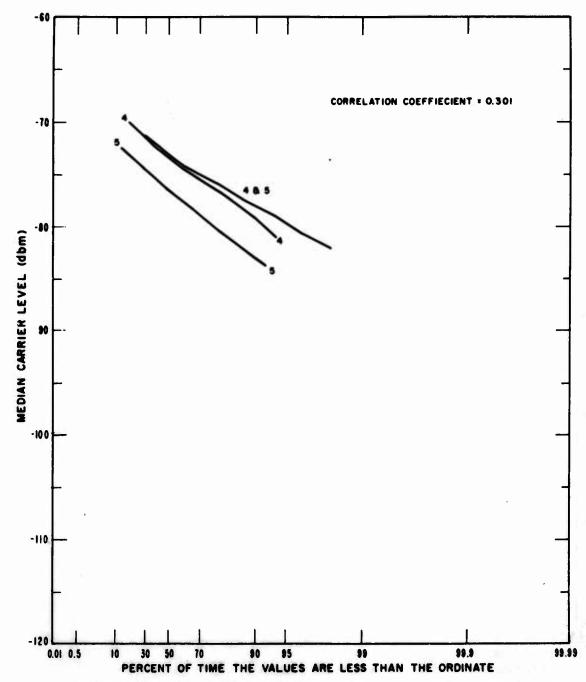


Figure 98. Sample distributions and combined distributions, Run 134, Time 1645-1650, FDM.

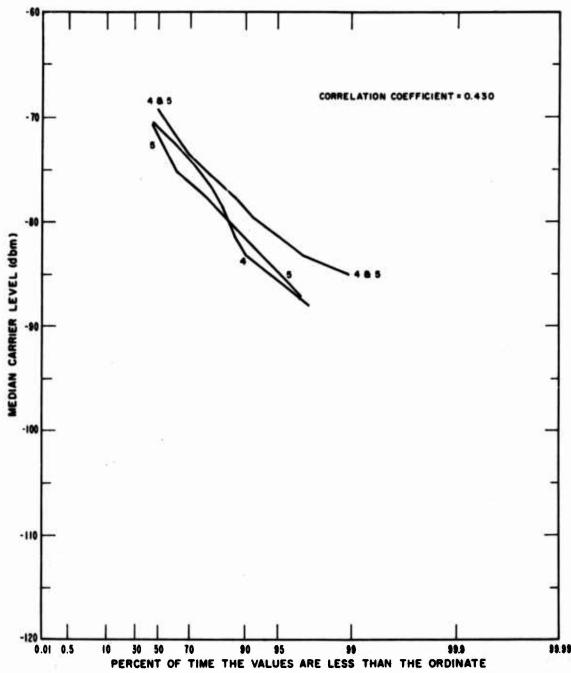


Figure 99. Sample distributions and combined distributions, Run 142, Time 1300-1305, FDM.

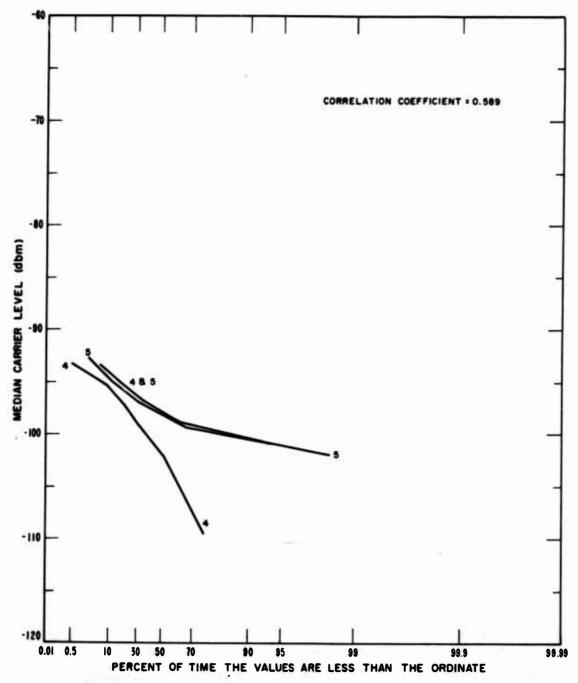


Figure 100. Sample distributions and combined distributions, Run 164, Time 1305-1310, FDM.

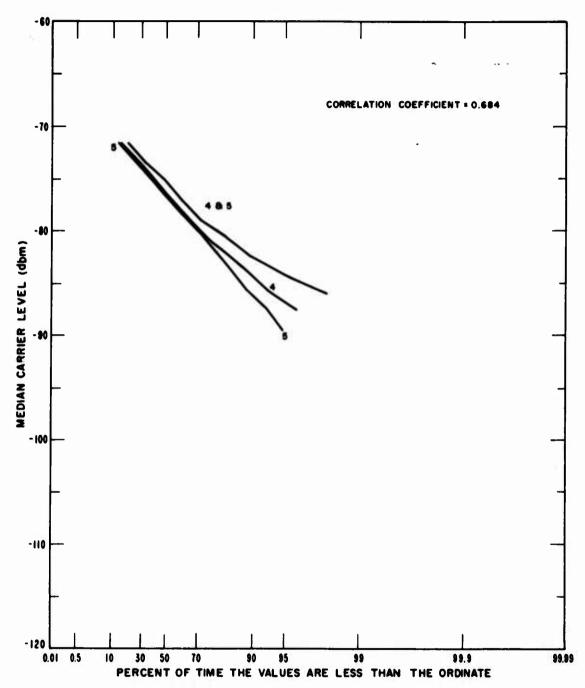


Figure 101. Sample distributions and combined distributions,
Run 215, Time 1320-1325, FDM.

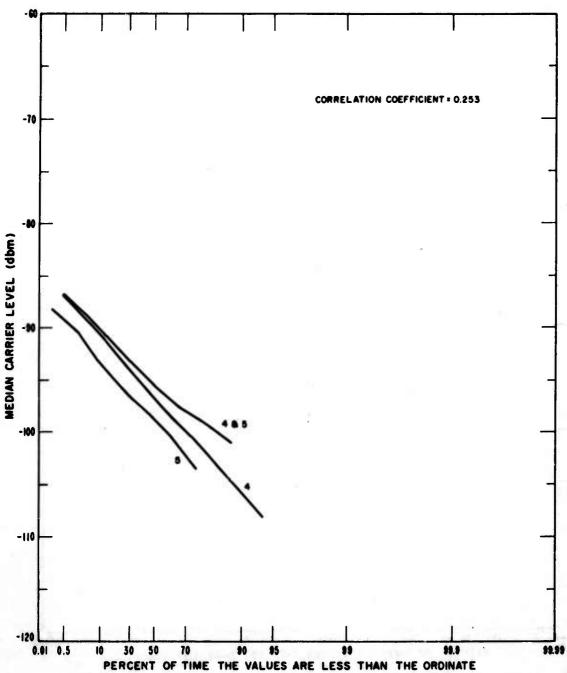


Figure 102. Sample distributions and combined distributions, Run 233, Time 1540-1545, FDM.

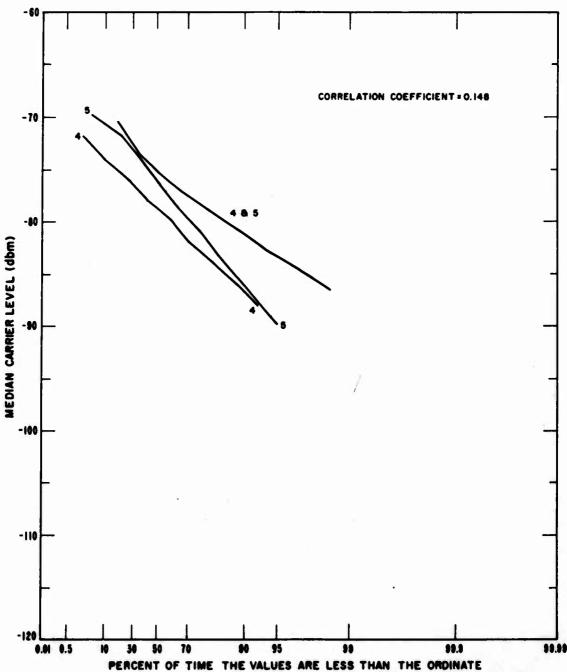


Figure 103. Sample distributions and combined distributions, Run 256, Time 1310-1315, FDM

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